



**STRUCTURAL CALCULATIONS**  
for  
**NM01-148 SPIKE**

at  
**221 NEW MEXICO 165**  
**PLACITAS, NM 87043**  
for  
**PINNACLE CONSULTING, INC.**  
&  
**RAYCAP (SS24-01302H-00R1)**



**BY: JACOB PROCTOR, P.E.**  
**PROFESSIONAL ENGINEER**

**PROJECT #: U0142.2054.242**

**DATE: October 24, 2024**

**DESIGNED BY MAR; CHECKED BY KJG**

**Note:**

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JOB NO.: UD142.2054.242

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PROJECT: NM01-148 SPIKE

**Design Criteria:**

**Code:** Structural design is based on the 2021 New Mexico Commercial Building Codes (2021-IBC) and the TIA-222-II standard.

**Wind:** Basic wind speed = 124 mph (3-second gust) per the TIA-222-II standard  
 Risk Category: II  
 Wind exposure: C  
 Topographic category: 1  
 Crest height: 0 ft

**Ice:** 0.25" radial ice @ 30 mph basic wind speed (3-second gust) per the TIA-222-II standard

**Seismic:** Seismic importance factor,  $I = 1$   
 Risk Category: II  
 Mapped spectral response accelerations:  $S_3 = 0.487g$   $S_4 = 0.16g$   
 Site class: C  
 Spectral response coefficients:  $S_{L18} = 0.422g$   $S_{D1} = 0.16g$   
 Seismic design category: C  
 Basic seismic force-resisting system: Telecomm. Steel Pole  
 Seismic base shear,  $V = 5.17$  k  
 Seismic response coefficient,  $C_s = 0.252$   
 Response modification factor,  $R = 1.5$   
 Analysis procedure: Equivalent Lateral Force

**General Notes:**

1. The contractor shall verify dimensions, conditions and elevations before starting work. The engineer shall be notified immediately if any discrepancies are found.
2. The typical notes and details shall apply in all cases unless specifically detailed elsewhere. Where no detail is shown, the construction shall be as shown for other similar work and as required by the building code.
3. These calculations are limited to the structural members shown in these calculations only.
4. The contractor shall be responsible for compliance with local construction safety orders. Approval of shop drawings by the architect or structural engineer shall not be construed as accepting this responsibility.
5. All structural framing members shall be adequately shored and braced during erection and until full lateral and vertical support is provided by adjoining members.



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PROJECT: NW01-146 SPIKE

**Structural Steel:**

- 1 All structural steel code checks based on the AISC, 15th Edition per the TIA-222-H standard
- 2 All 18-sided, tapered shaft steel to be per ASTM A572 GR. 65, U.N.O.
- 3 The design length of slip splices is equal to 1.67 times the inside width of the base of the upper section. Slip splice length tolerance is equal to  $\pm 1.0\%$  of the design slip splice length.
- 4 All steel pipe to be per ASTM A600 GR. B (72 KSI), U.N.O.
- 4 All steel round tubes (HSS) to be per , U.N.O.
- 5 All steel rectangular tubes (HSS) to be per ASTM A500 GR. B (46 KSI), U.N.O.
- 5 All steel wide flange shapes to be per , U.N.O.
- 6 All other structural steel shapes & plates shall be per ASTM A36, U.N.O.
- 7 All anchor bolts shall be per ASTM A615 GR. 75, U.N.O.
- 8 All bolts for steel-to-steel connections shall be per ASTM F3125 GR. A325 U.N.O.
- 9 All bolted connections shall be tightened per the "turn-of-nut" method as defined by AISC.
- 10 All welding shall be performed by certified welders in accordance with the latest edition of the American Welding Society (AWS) D1.1. Utilize minimum E70XX low-hydrogen electrode U.N.O. or where higher strength electrode is required by AWS D1.1
- 11 All steel surfaces shall be galvanized in accordance with ASTM A123 and ASTM F2329 standards, thoroughly coated with a zinc-rich primer, or otherwise protected as noted on the structural drawings.

**Fiberglass Reinforced Plastic (FRP):**

- 1 All structural shapes shall be Bedford Reinforced Plastics produced using the pultrusion process.
- 2 The fabricator and contractor shall exercise precautions necessary to protect the fiberglass pultruded structural shapes from abuse to prevent breakage, nicks, gouges, etc. during fabrication, handling, and installation.
- 3 Structural shapes shall be fabricated and assembled as indicated on the design drawings.
- 4 FRP threaded rods and nuts shall be tightened to snug tight and turned an additional 1/2 turn and locked with epoxy.

**Foundation / Concrete:**

- 1 All concrete mixing, placement, forming, and reinforcing installation shall be performed in accordance with the requirements of "Building Code Requirements for Reinforced Concrete", ACI 318-19. Foundation installation shall be in accordance with the requirements of "Standard Specifications for the Construction of Drilled Piers", ACI 355, latest edition.
- 2 All concrete shall have a minimum compressive strength of 4000 psi at 28 days.
- 3 Cement for all concrete shall be II with 8% ( $\pm 1.5\%$ ) entrained air. Maximum aggregate size shall be 3/4".
- 4 Reinforcing steel shall be per ASTM A615 Gr. 60, U.N.O.
- 5 Foundation design is based upon the project soils report prepared by:

Geotech: Tower Engineering Professionals, Inc.  
 Report No: 341545  
 Date: 31-Jul-24



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PROJECT: NM01-148 Spike

**DESIGN WIND LOADS ON LARGE RADOME CONCEALMENTS:**  
 (Screenwalls/Concealments on Monopoles)

Round Concealment Calculations  
 Supported on a Pole structure  
 Design per TIA-222-H

Label: Concealment tower

**INPUT DATA:**

Basic Wind Speed, V (mph) 104  
 Exposure Category C  
 Elevation Above Sea Level (ft) 5520

Structure:

Supporting Structure: Pole  
 Concealment Shape: Round  
 Tower Top of Steel (ft): 75  
 # of Concealments: 3

	Top	2nd	Bottom
Elevation Centerline (ft):	70	80	50
Concealment Height (ft):	10.0	10.0	10.0
Concealment Diameter (ft):	18.0	18.0	18.0
Open Area Top (%):	100%	0%	0%
Open Area Bottom (%):	0%	0%	100%

**WIND DESIGN SUMMARY:**

	70 ft.	60 ft.	50 ft.
Full Wind Pressure, 1.0W [psf]:	17.5	18.9	18.3
Full Ice Wind Pressure, 1.0W [psf]:	2.9	2.8	2.7
Full Service Wind Pressure, 1.0W [psf]:	5.8	5.6	5.4
Inside Wind Pressure, 1.0W [psf]:	21.0	20.3	19.6
Inside Ice Wind Pressure, 1.0W [psf]:	3.5	3.4	3.3
Inside Service Wind Pressure, 1.0W [psf]:	7.0	6.8	6.5
Wind Force, Outside Face (lbs):	3151	3051	2936
Wind Force, Inside Face (lbs):	2228	0	2075
Total Wind Force (lbs):	5379	3051	5011



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PROJECT: NM01-148 Spk

**WEIGHT DESIGN SUMMARY:**

**Self Weight Only:**

	Component:	Densities		Length, Area, Quantity		Self Weight (lb)	Total + 10% (lb)
Top @ 70' Elevation	ESSV Panel:	2.00	pcf	Area = ft <sup>2</sup>	585	1131	2084
	Framing w/o Grating	3.0	pcf	Area = ft <sup>2</sup>	254	763	
2nd @ 60' Elevation	ESSV Panel:	2.00	pcf	Area = ft <sup>2</sup>	585	1131	2084
	Framing w/o Grating	3.0	pcf	Area = ft <sup>2</sup>	254	763	
Bottom @ 50' Elevation	ESSV Panel:	2.00	pcf	Area = ft <sup>2</sup>	585	1131	2084
	Framing w/o Grating	3.0	pcf	Area = ft <sup>2</sup>	254	763	
						<b>W<sub>s</sub> =</b>	<b>621.1</b>

**Ice Weight Only:**

	Component:	Ice Density		Length, Area		Ice Weight (lb)	Total Weight (lb)
Top @ 70' Elevation	ESSV Panel:	1.3	pcf	Area = ft <sup>2</sup>	585	711	1031
	Framing w/o Grating	1.3	pcf	Area = ft <sup>2</sup>	254	320	
2nd @ 60' Elevation	ESSV Panel:	1.3	pcf	Area = ft <sup>2</sup>	585	711	1031
	Framing w/o Grating	1.3	pcf	Area = ft <sup>2</sup>	254	320	
Bottom @ 50' Elevation	ESSV Panel:	1.3	pcf	Area = ft <sup>2</sup>	585	711	711
	Framing w/o Grating	1.3	pcf	Area = ft <sup>2</sup>	0	0	
						<b>W<sub>i</sub> =</b>	<b>2774</b>

**Total W<sub>i</sub> = 8025**



JOB NO.: UD-42,0054,040

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PROJECT: NV01-143 SP KE

ASCE 7-16

**Seismic Base Shear Calculations:**

**Seismic Parameters:**

Risk Category	II
Seismic Design Category	D
Importance Factor	1.00
Site Class	S
R	5
$T_L$	6

$S_{D1}$	0.317	g
$S_1$	0.163	g
$S_{D2}$	0.215	g
$S_{M1}$	0.249	g

$S_{D3}$	0.422	g
$S_{M3}$	0.180	g
$\nu$	1.00	
$F_v$	1.50	

**Seismic Base Shear:**

Struct. Type	Tubular Steel Pole	
Detail Type	Worst Case C5	
h	74.0	ft
l	29400	lbs

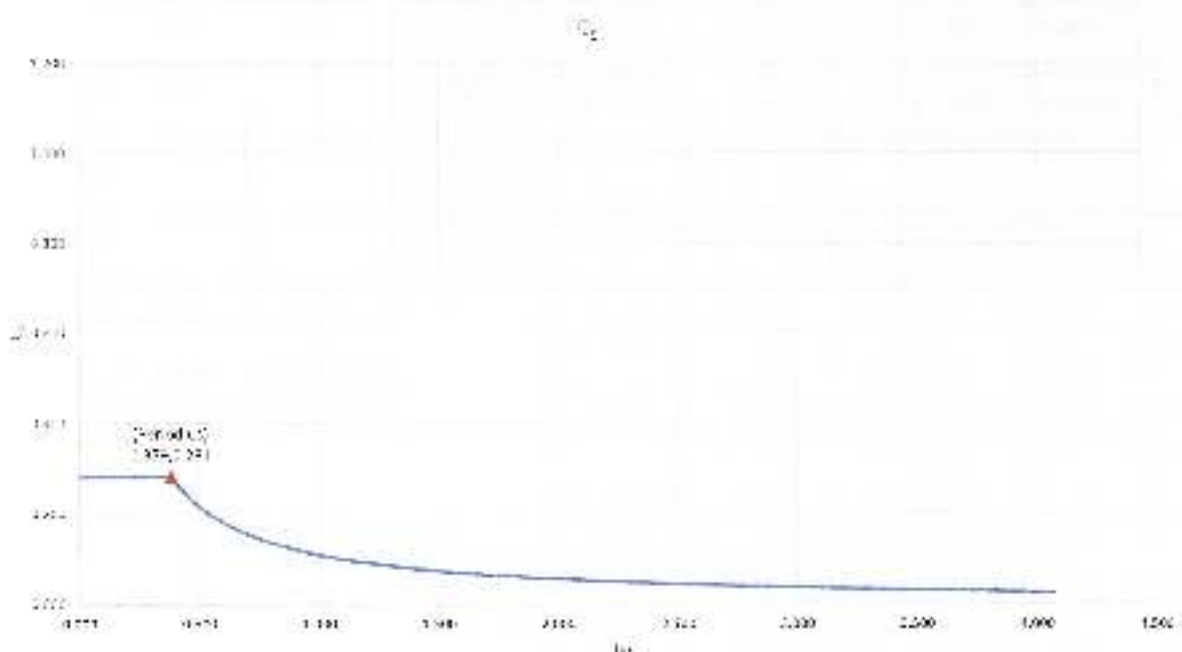
W	15.0	k
$W_1$	18.0	k

$t_d$	1.04	sec
T	0.98	sec
$\chi$	1.00	

$C_d$	0.282	
Seismic Shear $V_{base}$	3.0	k
Wind Shear	16.5	k

ratio	0.24
-------	------

**Wind Controls, No Seismic Analysis Required**



DESIGNED APPURTENANCE LOADING

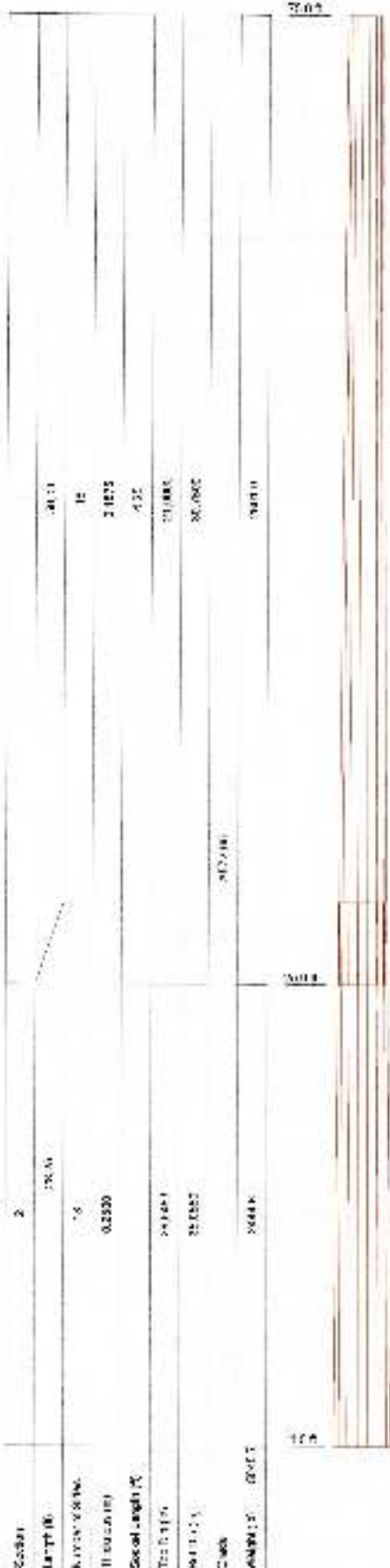
TYPE	ELEVATION	TYPE	ELEVATION
Concrete Load @ 50 PSF	75	40 Concrete Wall (Thickness 24 in)	88
10' Concrete Panel (Thickness 12 in)	72	20 Concrete Wall (Thickness 24 in)	85
10' Concrete Panel (Thickness 12 in)	70	10' Concrete Wall (Thickness 24 in)	82
10' Concrete Panel (Thickness 12 in)	68	10' Concrete Wall (Thickness 24 in)	79
10' Concrete Panel (Thickness 12 in)	66	10' Concrete Wall (Thickness 24 in)	76
10' Concrete Panel (Thickness 12 in)	64	10' Concrete Wall (Thickness 24 in)	73
10' Concrete Panel (Thickness 12 in)	62	10' Concrete Wall (Thickness 24 in)	70
10' Concrete Panel (Thickness 12 in)	60	10' Concrete Wall (Thickness 24 in)	67
10' Concrete Panel (Thickness 12 in)	58	10' Concrete Wall (Thickness 24 in)	64
10' Concrete Panel (Thickness 12 in)	56	10' Concrete Wall (Thickness 24 in)	61
10' Concrete Panel (Thickness 12 in)	54	10' Concrete Wall (Thickness 24 in)	58
10' Concrete Panel (Thickness 12 in)	52	10' Concrete Wall (Thickness 24 in)	55
10' Concrete Panel (Thickness 12 in)	50	10' Concrete Wall (Thickness 24 in)	52
10' Concrete Panel (Thickness 12 in)	48	10' Concrete Wall (Thickness 24 in)	49
10' Concrete Panel (Thickness 12 in)	46	10' Concrete Wall (Thickness 24 in)	46

MATERIAL STRENGTH

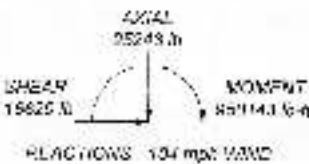
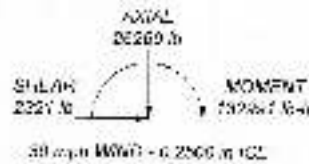
GRADE	Fy	Fu	GRADE	Fy	Fu
ASTM A36	36 ksi	58 ksi			

TOWER DESIGN NOTES


1. Tower is located in Bernalillo County, New Mexico.
2. Tower designed for Exposure C to the TIA-222-I Standard.
3. Tower designed for 114 mph basic wind in accordance with the TIA-222-I Standard.
4. Tower is also designed for 470 mph basic wind with 0.25 in. local ice accumulation, or increase in thickness with height.
5. Deflections are based upon 470 mph wind.
6. Tower Risk Category II.
7. Topography Category 1 with Crest Height of 0.00 ft.
8. TOWER RATING: 74.8%



ALL RELATIONS ASSUMED



<b>Vector Structural Engineering</b>		<b>** Spike</b>	
651 W Galena Park Blvd Draper, UT 84020 Phone: (801) 980-1775 Fax: (801) 980-1775		PLA 00142.2054.242	DATE 10/27/24
DRN 10/27/24	CHK 10/27/24	APP 10/27/24	REV 10/27/24

 <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd Denver, CO 80220 Phone: (303) 980-1775 Fax: (303) 980-1776	Job	Spike	Page 8 of 131
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	Client	Raycap	17:04:43 10/24/24
			Designed by
			mirie

## Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

- Tower is located in Sandoval County, New Mexico.
- Tower base elevation above sea level: 5521.00 ft.
- Basic wind speed of 101 mph.
- Risk Category II.
- Exposure Category C.
- Simplified Topographic Factor Procedure for wind speed-up calculations is used
- Topographic Category: 1.
- Crest Height: 0.00 ft.
- Nominal ice thickness of 0.2500 in.
- Ice thickness is considered to increase with height.
- Ice density of 56 pcf.
- A wind speed of 30 mph is used in combination with ice.
- Deflections calculated using a wind speed of 60 mph.
- Non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in pole design is 1.
- Local bending stresses due to climbing loads, lean line supports, and appearance mounts are not considered.

## Options

- |   |  |   |
|---|--|---|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontal</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>Use Code Stress Ratios</li> <li>Use Code Safety Factors - Girts</li> <li>Fasten to Ice</li> <li>Always Use Max Kz</li> <li>Kz In Exposure D Hurricane Region</li> <li>Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Girts Use</li> <li>Use Diagonal Inner Bracing (1 Side)</li> <li>SR Members Have Cur. Ends</li> <li>SR Members Are Concentric</li> <li>Distribute Leg Loads As Uniform</li> <li>Use Special Wind Profile</li> </ul> | <ul style="list-style-type: none"> <li>Assume Legs Pinned</li> <li>Assume Rig. 4 Inces. Plate</li> <li>Use Clean Splice For Wind Area</li> <li>Use Clean Splice For Kz</li> <li>Retention Girts In Initial Tension</li> <li>Bypass Mast Stability Checks</li> <li>Use Approx. Dish Coefficients</li> <li>Project Wind Area of Appendages</li> <li>Alternative Approx. EPA Calculation</li> <li>Adjust In-Tension Arm Area</li> <li>Add BC, GD+W Combination</li> <li>Soil Capacity Reports By Component</li> <li>Truing Into Diamond Tower Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> <li>Ignore Kz For 10 Deg. Angle Legs</li> <li>Use ASCE 10 X Drace Ly Rules</li> </ul> | <ul style="list-style-type: none"> <li>Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable Offset Girt At Foundation</li> <li>Consider Feed Line Torque</li> <li>Include Angle Deck Shear Checks</li> <li>Use TIA-222-H Bracing Report Exception</li> <li>Use TIA-222-H Tension Splice Exception</li> <li>Include Shear-Tension Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> <li>Pole Without Linear Attachments</li> <li>Pole With Stroud Or No Appendages</li> <li>Outside and Inside Corner Radii Are Known</li> </ul> |
|---|--|---|

## Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Dead Radius in	Pole Grade
L1	75.00 - 25.00	50.00	4.25	4	21.0000	30.7500	0.1875	0.7500	A572-55 (65 ksi)
L2	27.00 - 0.00	28.25		4	20.5664	45.0550	0.2500	1.0000	A572-55 (65 ksi)

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 621 W. Carlton Park Blvd Tampa, FL 33629 Phone: (813) 980-1775 FAX: (813) 999-1776	Job	Page 8 of 131
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	Client	Designed by
	Spike	
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	Raycap	mririe

### Tapered Pole Properties

Section	Top Dia in	Area in <sup>2</sup>	$I$ in <sup>4</sup>	$r$ in	$Z$ in	$S_x$ in <sup>3</sup>	$S_y$ in <sup>3</sup>	$J$ in <sup>4</sup>	$w$ lb	$w/L$
1.1	31.2950	12.3850	577.8251	7.4884	10.6580	52.5383	1356.6444	6.7042	3.2660	17.952
	31.1954	13.1855	2146.5191	10.8497	12.6210	129.4051	4295.6404	9.0060	5.0820	27.064
1.2	40.8000	31.7466	2920.5490	10.4004	13.0197	167.9101	5044.7089	11.6295	4.7901	19.041
	35.5572	27.6174	4276.7766	12.3555	11.8017	217.3557	8155.1149	13.8115	5.7297	23.019

Tower Elevation	Gusset Area per face	Gusset Thickness	Gusset Grade	Adjust Factor $A_f$	Adjust Factor $A_s$	Weight Mult.	Double Angle Spacing Diagonals in	Double Angle Spacing Horizontal in	Double Angle Spacing Vertical in
$H$	$A_f$	$t$					$s$	$s$	$s$
U. 75.00-22.00				1	1	1			
L. 75.00-1.00				1	1	1			

### User Defined Loads

Description	Elevation	Offset From Centroid	Windward Angle	Weight	$F_x$	$F_y$	Howl Factor	$C_{df}$
	$H$	$A$	$\theta$	$W$	$F_x$	$F_y$	$H_f$	$C_{df}$
Concealment Loading @ 75 ft	75.00	0.00	0.0000	No Ice	0.00	0.00	0.00	90.54
				Ice	316.00	0.00	0.00	143.59
				Service	1042.00	0.00	0.00	106.48
Concealment Loading @ 65 ft	65.00	0.00	0.0000	No Ice	0.00	0.00	0.00	93.31
				Ice	316.00	0.00	0.00	147.99
				Service	1042.00	0.00	0.00	109.75
Concealment Loading @ 65 ft	65.00	0.00	0.0000	No Ice	0.00	0.00	0.00	53.90
				Ice	316.00	0.00	0.00	105.85
				Service	1042.00	0.00	0.00	62.28
Concealment Loading @ 55 ft	55.00	0.00	0.0000	No Ice	0.00	0.00	0.00	54.79
				Ice	316.00	0.00	0.00	109.67
				Service	1042.00	0.00	0.00	61.51
Concealment Loading @ 55 ft	55.00	0.00	0.0000	No Ice	0.00	0.00	0.00	91.04
				Ice	356.00	0.00	0.00	142.92
				Service	1042.00	0.00	0.00	105.91
Concealment Loading @ 45 ft	45.00	0.00	0.0000	No Ice	0.00	0.00	0.00	149.09
				Ice	356.00	0.00	0.00	191.00
				Service	1042.00	0.00	0.00	130.48

### Discrete Tower Loads

<b>InxTower</b>  <b>Vector Structural Engineering</b> 631 W. Collins Park Blvd Denver, UT 84296 Phone: (801) 999-1775 FAX: (801) 956-1776	<b>Job</b>		Spike		<b>Page</b> 10 of 131	
	<b>Project</b>		U0142.2054.242		<b>Date</b> 17:04:43 10/24/24	
	<b>Client</b>		Raycap		<b>Designed by</b> mrrrie	

Description	Face or Leg	Offset Type	Offset Dim. Lateral Top # # #	Adjustment	Placement	Cut From	Cut To	Weight
				"	#	#	#	#
(4) Generic Panel (Enclosed, 115 lbs)	A	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	115.00 115.00
(4) Generic Panel (Enclosed, 115 lbs)	B	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	115.00 115.00
(4) Generic Panel (Enclosed, 115 lbs)	C	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	115.00 115.00
(2) 10'-0" T-arm EPA = 5.7 372 (61 lbs)	A	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	161.00 161.26
(2) 10'-0" T-arm EPA = 5.7 372 (61 lbs)	B	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	161.00 161.26
(2) 10'-0" T-arm EPA = 5.7 372 (61 lbs)	C	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	161.00 161.26
(4) Generic RRU (Enclosed, 75 lbs)	A	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	D	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	C	From Face	3.00 3.00 3.00	0.0000	70.00	No Ice .25" Ice	0.00 0.00	75.00 75.00
***								
(4) Generic Panel (Enclosed, 115 lbs)	A	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	115.00 115.00
(4) Generic Panel (Enclosed, 115 lbs)	H	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	115.00 115.00
(4) Generic Panel (Enclosed, 115 lbs)	C	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	115.00 115.00
(2) 10'-0" T-arm EPA = 5.7 372 (61 lbs)	A	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	161.00 161.26
(2) 10'-0" T-arm EPA = 5.7 372 (61 lbs)	B	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	161.00 161.26
(2) 10'-0" T-arm EPA = 5.7 372 (61 lbs)	C	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	161.00 161.26
(4) Generic RRU (Enclosed, 75 lbs)	A	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	B	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	C	From Face	3.00 3.00 3.00	0.0000	60.00	No Ice .25" Ice	0.00 0.00	75.00 75.00
***								
(4) Generic Panel (Enclosed, 115 lbs)	A	From Face	3.00	0.0000	30.00	No Ice	0.00	115.00

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 681 W. Galena Park Blvd Jasper, UT 84920 Phone: (801) 290-1775 FAX: (801) 290-1776	Job	Spike	Page 11 of 31
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	Client	Raycap	Designed by
			mnie

Description	Face or Leg	Offset Type	Offset Face Lateral Force	Adjustment	Placement	C.F. Front	C.F. Side	Weight
			$\frac{F}{h}$	$\frac{F}{h}$	$\frac{F}{h}$	$\frac{F}{h}$	$\frac{F}{h}$	$\frac{F}{h}$
115 lbs)			0.00		12" Ice	0.00	0.00	115.00
(4) Generic Panel (Enclosed, 115 lbs)	D	Front Face	3.00	0.0000	50.00	No Ice	0.00	115.00
			0.00		12" Ice	0.00	0.00	115.00
			0.00					
(4) Generic Panel (Enclosed, 115 lbs)	C	Front Face	3.00	0.0000	50.00	No Ice	0.00	115.00
			0.00		12" Ice	0.00	0.00	115.00
			0.00					
(2) 10'0" Tall BPA - 5.7 (59 (61 lbs)	A	Front Face	3.00	0.0000	50.00	No Ice	0.00	151.00
			0.00		12" Ice	0.00	0.00	59.25
			0.00					
(2) 10'0" Tall BPA - 5.7 (72 (61 lbs)	B	Front Face	3.00	0.0000	50.00	No Ice	0.00	151.00
			0.00		12" Ice	0.00	0.00	59.25
			0.00					
(2) 10'0" Tall BPA - 5.7 (72 (61 lbs)	C	Front Face	3.00	0.0000	50.00	No Ice	0.00	151.00
			0.00		12" Ice	0.00	0.00	59.25
			0.00					
(4) Generic BRC (Enclosed, 75 lbs)	A	Front Face	3.00	0.0000	50.00	No Ice	0.00	75.00
			0.00		12" Ice	0.00	0.00	75.00
			0.00					
(4) Generic BRC (Enclosed, 75 lbs)	B	Front Face	3.00	0.0000	50.00	No Ice	0.00	75.00
			0.00		12" Ice	0.00	0.00	75.00
			0.00					
(4) Generic BRC (Enclosed, 75 lbs)	C	Front Face	3.00	0.0000	50.00	No Ice	0.00	75.00
			0.00		12" Ice	0.00	0.00	75.00
			0.00					

### Tower Pressures - No Ice

$$G_U = 1.00$$

Section Elevation	$z$	$K_z$	$n$	$A_g$	$F$	$A_p$	$A_s$	$A_{se}$	Leg %	$C_{d1}$ on Face	$C_{d1}$ on Face
$\frac{z}{h}$	$\frac{z}{h}$		$\frac{z}{h}$	$\frac{z}{h}$	$\frac{z}{h}$	$\frac{z}{h}$	$\frac{z}{h}$	$\frac{z}{h}$		$\frac{z}{h}$	$\frac{z}{h}$
L1 15.00-25.00	49.10	1.000	74	176.355	A	0.000	106.355	136.355	100.00	0.000	0.000
					B	0.000	106.355		100.00	0.000	0.000
					C	0.000	106.355		100.00	0.000	0.000
L2 25.00-1.00	12.71	0.850	78	66.362	A	0.000	66.362	66.362	100.00	0.000	0.000
					B	0.000	66.362		100.00	0.000	0.000
					C	0.000	66.362		100.00	0.000	0.000

### Tower Pressure - With Ice

$$G_U = 1.00$$

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W Galena Park Blvd Denver, CO 80229 Phone: (303) 996-1775 Fax: (303) 996-1776	Job	Spire	Page 12 of 13	
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	Client	Raycap	Designed by	mirrie

Section Elevations	z	$K_z$	$g_f$	$Z_e$	$Z_{e,0}$	$\beta$	$Z_{e,0}$	$Z_{e,0}$	$Z_{e,0}$	Leg	$C_{d,0}$	$C_{d,0}$
ft	m		psf	ft	ft	e	ft	ft	ft	ft	Face	Face
L1 75.00-25.00	43.10	1.000	5	0.5601	111.523	A	0.000	111.523	111.523	100.00	0.000	0.000
						B	0.000	111.523	111.523	100.00	0.000	0.000
						C	0.000	111.523	111.523	100.00	0.000	0.000
L2 25.00-1.00	12.91	0.850	2	0.2273	67.403	A	0.000	67.403	67.403	100.00	0.000	0.000
						B	0.000	67.403	67.403	100.00	0.000	0.000
						C	0.000	67.403	67.403	100.00	0.000	0.000

### Tower Pressure - Service

$$G_e = 1.000$$

Section Elevations	z	$K_z$	$g_f$	$Z_e$	$Z_{e,0}$	$\beta$	$Z_{e,0}$	$Z_{e,0}$	$Z_{e,0}$	Leg	$C_{d,0}$	$C_{d,0}$
ft	m		psf	ft	ft	e	ft	ft	ft	ft	Face	Face
L1 75.00-25.00	43.10	1.000	7	109.355		A	0.000	109.355	109.355	100.00	0.000	0.000
						B	0.000	109.355	109.355	100.00	0.000	0.000
						C	0.000	109.355	109.355	100.00	0.000	0.000
L2 25.00-1.00	12.91	0.850	5	65.362		A	0.000	65.362	65.362	100.00	0.000	0.000
						B	0.000	65.362	65.362	100.00	0.000	0.000
						C	0.000	65.362	65.362	100.00	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevations	Add Weight	Self Weight	P	a	$Z_{e,0}$	$g_f$	$D_{e,0}$	$D_{e,0}$	$D_{e,0}$	F	v	Corr. Factor
ft	lb	lb	e	e	psf		ft	ft	ft	lb	psf	
L1 75.00-25.00	0.00	2600.97	A	1	0.73	24	1	1	109.355	2151.37	43.03	C
			B	1	0.73		1	1	109.355			
			C	1	0.73		1	1	109.355			
L2 25.00-1.00	0.00	2444.77	A	1	0.73	19	1	1	65.362	1027.02	42.79	C
			B	1	0.73		1	1	65.362			
			C	1	0.73		1	1	65.362			
Sum Weight	0.00	5045.74							OTM 1' 5538.47 lb-ft	3178.39		

### Tower Forces - No Ice - Wind 45 To Face

Section Elevations	Add Weight	Self Weight	P	a	$Z_{e,0}$	$g_f$	$D_{e,0}$	$D_{e,0}$	$D_{e,0}$	F	v	Corr. Factor
ft	lb	lb	e	e	psf		ft	ft	ft	lb	psf	
L1 75.00-25.00	0.00	2600.97	A	1	0.73	24	1	1	109.355	2151.37	43.03	C
			B	1	0.73		1	1	109.355			
			C	1	0.73		1	1	109.355			
L2 25.00-1.00	0.00	2444.77	A	1	0.73	19	1	1	65.362	1027.02	42.79	C

<b>tnxTower</b> <i>Vector Structural Engineering</i> 651 W. Galena Park Blvd Denver, CO 80229 Phone: (303) 950-1771 FAX: (303) 950-1776	Job	Spiko	Page	13 of 131
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Section Elevation	Add Weight	Self Weight	F <sub>u</sub> F <sub>c</sub> F <sub>e</sub>	e	C <sub>s</sub>	q <sub>s</sub> psf	D <sub>r</sub>	D <sub>s</sub>	A <sub>s</sub> ft <sup>2</sup>	F	w	Ctrl. Floor
ft	lb	lb								lb	psf	
Sum Weight:	0.00	3045.74	B C	1 1	0.75 0.75		1	1	66.362 66.362 115508.37 lb-ft	3178.39		

**Tower Forces - No Ice - Wind 60 To Face**

Section Elevation	Add Weight	Self Weight	F <sub>u</sub> F <sub>c</sub> F <sub>e</sub>	e	C <sub>s</sub>	q <sub>s</sub> psf	D <sub>r</sub>	D <sub>s</sub>	A <sub>s</sub> ft <sup>2</sup>	F	w	Ctrl. Floor
ft	lb	lb								lb	psf	
L 75.00-25.00	0.00	2600.97	A B C	1 1 1	0.75 0.75 0.75	24	1	1	109.355 109.355 109.355	2151.37	43.03	C
L2 25.00-1.00	0.00	2445.77	A B C	1 1 1	0.75 0.75 0.75	19	1	1	66.362 66.362 66.362	1027.01	42.79	C
Sum Weight:	0.00	3045.74						OTM	115508.37 lb-ft	3178.39		

**Tower Forces - No Ice - Wind 90 To Face**

Section Elevation	Add Weight	Self Weight	F <sub>u</sub> F <sub>c</sub> F <sub>e</sub>	e	C <sub>s</sub>	q <sub>s</sub> psf	D <sub>r</sub>	D <sub>s</sub>	A <sub>s</sub> ft <sup>2</sup>	F	w	Ctrl. Floor
ft	lb	lb								lb	psf	
L 75.00-25.00	0.00	2600.97	A B C	1 1 1	0.75 0.75 0.75	24	1	1	109.355 109.355 109.355	2151.37	43.03	C
L2 25.00-1.00	0.00	2445.77	A B C	1 1 1	0.75 0.75 0.75	19	1	1	66.362 66.362 66.362	1027.02	42.79	C
Sum Weight:	0.00	3045.74						OTM	115508.37 lb-ft	3178.39		

**Tower Forces - With Ice - Wind Normal To Face**

Section Elevation	Add Weight	Self Weight	e <sub>u</sub> e <sub>c</sub> e <sub>e</sub>	e	C <sub>s</sub>	q <sub>s</sub> psf	D <sub>r</sub>	D <sub>s</sub>	A <sub>s</sub> ft <sup>2</sup>	F	w	Ctrl. Floor
ft	lb	lb								lb	psf	
L1 75.00-35.00	0.00	3020.56	A B C	1 1 1	1.2 1.2 1.2	2	1	1	111.325 111.325 111.325	500.11	5.00	C

<b>inxTower</b> <b>Vector Structural Engineering</b> 651 W Gibson Park Blvd Denver, CO 80239 Phone: (303) 990-1775 Fax: (303) 990-0776	Job	Spike	Page 14 of 101
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	Client	Raycap	Designed by
			mirrie

Section Elevation	Add Weight	Self Weight	F a c t o r	e	C <sub>r</sub>	g <sub>r</sub>	D <sub>r</sub>	D <sub>s</sub>	A <sub>r</sub>	F	w	Ctrl Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	psf	
1.2 75 00-1.00	0.00	2466.54	A	1	1.2	2	1	1	67.271	142.40	5.93	C
			B	1	1.2		1	1	67.271			
			C	1	1.2		1	1	67.271			
Sum Weight	0.00	5687.10						OTM	16192.78 lb-ft	442.51		

### Tower Forces - With Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c t o r	e	C <sub>r</sub>	g <sub>r</sub>	D <sub>r</sub>	D <sub>s</sub>	A <sub>r</sub>	F	w	Ctrl Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	psf	
1.1 75 00-75.00	0.00	3091.99	A	1	1.2	1	1	-	111.523	300.11	6.00	C
			B	1	1.2		1	-	111.523			
			C	1	1.2		1	-	111.523			
1.2 25 00-1.00	0.00	2866.51	A	1	1.2	2	1	1	67.271	142.40	5.93	C
			D	1	1.2		1	1	67.271			
			E	1	1.2		1	1	67.271			
Sum Weight	0.00	5587.10						OTM	6192.78 lb-ft	442.51		

### Tower Forces - With Ice - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c t o r	e	C <sub>r</sub>	g <sub>r</sub>	D <sub>r</sub>	D <sub>s</sub>	A <sub>r</sub>	F	w	Ctrl Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	psf	
1.1 75 00 25.00	0.00	3020.96	A	1	1.2	2	-	1	111.523	300.11	6.00	C
			B	1	1.2		-	1	111.523			
			C	1	1.2		-	1	111.523			
1.2 25 00-1.00	0.00	2666.24	A	1	1.2	2	-	1	67.271	142.40	5.93	C
			B	1	1.2		-	1	67.271			
			C	1	1.2		-	1	67.271			
Sum Weight	0.00	5687.10						OTM	16192.78 lb-ft	442.51		

### Tower Forces - With Ice - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	F a c t o r	e	C <sub>r</sub>	g <sub>r</sub>	D <sub>r</sub>	D <sub>s</sub>	A <sub>r</sub>	F	w	Ctrl Face
ft	lb	lb				psf			ft <sup>2</sup>	lb	psf	
1.1 75 00-25.00	0.00	3020.96	A	1	1.2	2	1	1	111.523	300.11	6.00	C
			B	1	1.2		1	1	111.523			

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 631 W. Indiana Park Blvd Denver, CO 80206 Phone: (303) 999-1775 FAX: (303) 990-1775	Job	Page 15 of 131
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	Spike	
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	Raycap	mrrle

Section Elevation	Add Weight	Self Weight	F a c e	e	Lx	g	Dx	Cx	Fx	F	w	Ctrl Face
#	lb	lb	e			pcf			lb	lb	pcf	
L1 75.00-100.00	0.00	2669.54	A	1	1.2		1	1	111.324			
			B	1	1.2		1	1	67.271	142.40	5.94	C
			C	1	1.2		1	1	67.271			
			C	1	1.2		1	1	67.271			
Sum Weight	0.00	3687.00						DTM	16102.78	142.51		
									lb			

### Tower Forces - Service - Wind Normal To Face


Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	g	Dx	Cx	Fx	F	w	Ctrl Face
#	lb	lb	e			pcf			lb	lb	pcf	
L1 75.00-100.00	0.00	2600.90	A	1	0.75		7	1	109.355	508.65	12.17	C
			B	1	0.75		7	1	109.355			
			C	1	0.75		7	1	109.355			
L2 25.00-100.00	0.00	2444.77	A	1	0.75		5	1	66.362	200.56	13.11	C
			B	1	0.75		5	1	66.362			
			C	1	0.75		5	1	66.362			
Sum Weight	0.00	5045.67						DTM	32678.95	509.21		
									lb			

### Tower Forces - Service - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	g	Dx	Cx	Fx	F	w	Ctrl Face
#	lb	lb	e			pcf			lb	lb	pcf	
L1 75.00-100.00	0.00	2600.90	A	1	0.75		7	1	109.355	508.65	12.17	C
			B	1	0.75		7	1	109.355			
			C	1	0.75		7	1	109.355			
L2 25.00-100.00	0.00	2444.77	A	1	0.75		5	1	66.362	200.56	13.11	C
			B	1	0.75		5	1	66.362			
			C	1	0.75		5	1	66.362			
Sum Weight	0.00	5045.67						DTM	32678.95	509.21		
									lb			

### Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	g	Dx	Cx	Fx	F	w	Ctrl Face
#	lb	lb	e			pcf			lb	lb	pcf	
L1	0.00	2600.90	A	1	0.75		7	1	109.355	508.65	12.17	C

 <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd Draper, UT 84076 Phone: (801) 999-1775 FAX: (801) 956-1776	Job	Spike	Page 16 of 181	
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	Client	Raycap	Designed by	mmic

Section Elevation	Auto Weight	Self Weight	P a s	a	Cx	qx	My	Dy	Ay	P	q	Cor. Face
ft	lb	lb	s			psf			ft <sup>2</sup>	lb	psf	
75.00-25.00			H	1	0.73		1	1	109.353			
			C	1	0.73		1	1	109.353			
L2 25.00-1.00	0.00	2444.77	A	1	0.73	S	1	1	66.563	340.56	12.17	C
			D	1	0.73		1	1	66.563			
			C	1	0.73		1	1	66.563			
Sum Weight	0.00	5345.74						OTM	43678.96 lb-ft	459.2		

**Tower Forces - Service - Wind 90 To Face**

Section Elevation	Auto Weight	Self Weight	P a s	a	Cx	qx	My	Dy	Ay	P	q	Cor. Face
ft	lb	lb	s			psf			ft <sup>2</sup>	lb	psf	
L1 75.00-25.00	0.00	2600.97	A	1	0.73	T	1	1	109.353	608.36	12.17	C
			D	1	0.73		1	1	109.353			
			C	1	0.73		1	1	109.353			
L2 25.00-1.00	0.00	2444.77	A	1	0.73	S	1	1	66.563	340.56	12.17	C
			H	1	0.73		1	1	66.563			
			C	1	0.73		1	1	66.563			
Sum Weight	0.00	5045.74						OTM	32678.96 lb-ft	359.2		

**Discrete Appurtenance Pressures - No Ice  $G_o = 1.100$**

Description	Area ft <sup>2</sup>	Height ft	Offset ft	Offset ft	z ft	K <sub>z</sub>	q <sub>z</sub> psf	C <sub>pe</sub> Frame ft <sup>2</sup>	C <sub>pe</sub> Side ft <sup>2</sup>
Generic Panel (Enclosed, 115 lbs)	200.0000	160.00	-3.25	-1.96	70.00	1.174	27	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	160.00	3.46	-1.96	70.00	1.174	27	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	160.00	0.00	3.46	70.00	1.174	27	0.00	0.00
10'-0" Trans EPA = 5.7 275 (161 lbs)	200.0000	322.00	-3.25	-1.96	70.00	1.174	27	0.00	0.00
10'-0" Trans EPA = 5.7 275 (161 lbs)	60.0000	322.00	3.46	-1.96	70.00	1.174	27	0.00	0.00
10'-0" Trans EPA = 5.7 275 (161 lbs)	180.0000	322.00	0.00	3.46	70.00	1.174	27	0.00	0.00
Generic R31 (Enclosed, 75 lbs)	100.0000	300.00	-3.25	-1.96	70.00	1.174	27	0.00	0.00
Generic R31 (Enclosed, 75 lbs)	60.0000	300.00	3.25	-1.96	70.00	1.174	27	0.00	0.00
Generic R31 (Enclosed, 75 lbs)	180.0000	300.00	0.00	3.02	70.00	1.174	27	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	200.0000	160.00	3.46	-2.00	60.00	1.137	26	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	160.00	3.46	-2.00	60.00	1.137	26	0.00	0.00

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd Draper, UT 84020 Phone: (801) 990-1723 FAX: (801) 990-1726	Job	Page 17 of 131
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	Client	Designed by
	Spike	
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	Raycap	mrnie

Description	Area (ft <sup>2</sup> )	Weight #	Offset ft	Offset ft	x ft	K <sub>x</sub>	q <sub>x</sub> psf	C.F. From ft <sup>2</sup>	C.F. Side ft <sup>2</sup>
115 (6)									
Generic Panel (Enclosed, 115 lbs)	180.0000	150.00	0.00	4.00	60.00	1.137	25	0.00	0.00
10'-0" Team EPA = 3.7 (72 (61 lbs)	300.0000	322.00	-3.46	-2.00	60.00	1.137	25	0.00	0.00
10'-0" Team EPA = 3.7 (72 (61 lbs)	300.0000	322.00	3.46	-2.00	60.00	1.137	25	0.00	0.00
10'-0" Team EPA = 3.7 (72 (61 lbs)	180.0000	322.00	0.00	4.00	60.00	1.137	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.46	-2.00	60.00	1.137	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	3.46	-2.00	60.00	1.137	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	4.00	60.00	1.137	25	0.00	0.00
Generic Plate (Enclosed, 1.5 lbs)	300.0000	400.00	3.53	-2.00	50.00	1.094	25	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	40.0000	400.00	3.53	2.00	50.00	1.094	25	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	4.98	50.00	1.094	25	0.00	0.00
10'-0" Team EPA = 3.7 (72 (15 lbs)	300.0000	322.00	-3.53	-2.00	50.00	1.094	25	0.00	0.00
10'-0" Team EPA = 3.7 (72 (15 lbs)	60.0000	322.00	3.53	-2.00	50.00	1.094	25	0.00	0.00
10'-0" Team EPA = 3.7 (72 (15 lbs)	30.0000	322.00	0.00	-1.38	50.00	1.094	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.53	-2.00	50.00	1.094	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.53	-2.00	50.00	1.094	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	-1.38	50.00	1.094	25	0.00	0.00
Sum Weight:		9738.00							

**Discrete Appurtenance Pressures - With Ice** *G<sub>H</sub> = 1.10*

Description	Area (ft <sup>2</sup> )	Weight #	Offset ft	Offset ft	x ft	K <sub>x</sub>	q <sub>x</sub> psf	C.F. From ft <sup>2</sup>	C.F. Side ft <sup>2</sup>	Z m
Generic Panel (Enclosed, 115 lbs)	300.0000	450.00	-3.40	-1.00	70.00	1.174	2	0.00	0.00	0.2593
Generic Panel (Enclosed, 115 lbs)	50.0000	450.00	3.40	-1.00	70.00	1.174	2	0.00	0.00	0.2593
Generic Panel (Enclosed, 115 lbs)	180.0000	150.00	0.00	3.00	70.00	1.174	2	0.00	0.00	0.2593
10'-0" Team EPA = 3.7 (72 (61 lbs)	300.0000	751.32	-3.40	-1.00	70.00	1.174	2	0.00	0.00	0.2593
10'-0" Team EPA = 3.7 (72 (61 lbs)	50.0000	751.32	3.35	-1.00	70.00	1.174	2	0.00	0.00	0.2593
10'-0" Team EPA = 3.7 (72 (61 lbs)	180.0000	751.32	0.00	3.00	70.00	1.174	2	0.00	0.00	0.2593
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.40	-1.00	70.00	1.174	2	0.00	0.00	0.2593
Generic RRU (Enclosed, 75 lbs)	50.0000	300.00	3.35	-1.00	70.00	1.174	2	0.00	0.00	0.2593
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	3.00	70.00	1.174	2	0.00	0.00	0.2593

<b><i>inxTower</i></b> <b>Vector Structural Engineering</b> 501 W. Collins Park Blvd Opaoka, PA 17020 Phone: (717) 928-1775 FAX: (717) 928-1776	Job	Spoke	Page 16 of 151
	Project	U0142.7054.242	Date
	Client	Raycap	17:04:43 10/24/24
			Designed by
			mrfie

Description	Amount Adjoint *	Weight lb	Offset ft	Offset ft	x ft	K <sub>x</sub>	q <sub>x</sub> psf	C.A. Front ft <sup>2</sup>	C.A. Side ft <sup>2</sup>	L <sub>x</sub> ft
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-3.45	-2.00	90.00	1.127	2	0.00	0.00	0.2654
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.45	-2.00	90.00	1.127	2	0.00	0.00	0.2654
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	-4.00	90.00	1.127	2	0.00	0.00	0.2654
10'-0" T-arm EPA = 5.7 0'-2" (161 lbs)	300.0000	746.92	-1.45	-2.00	90.00	1.127	2	0.00	0.00	0.2654
10'-0" T-arm EPA = 5.7 0'-2" (161 lbs)	60.0000	746.92	3.45	-2.00	90.00	1.127	2	0.00	0.00	0.2654
10'-0" T-arm EPA = 5.7 ft 2 (161 lbs)	180.0000	746.92	0.00	-4.00	90.00	1.127	2	0.00	0.00	0.2654
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-1.45	-3.00	90.00	1.125	2	0.00	0.00	0.2654
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.45	-3.00	90.00	1.125	2	0.00	0.00	0.2654
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	-4.00	90.00	1.125	2	0.00	0.00	0.2654
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-1.35	-2.04	90.00	1.094	2	0.00	0.00	0.2605
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	2.35	-2.04	90.00	1.094	2	0.00	0.00	0.2605
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	-4.08	90.00	1.094	2	0.00	0.00	0.2605
10'-0" T-arm EPA = 5.7 0'-2" (161 lbs)	300.0000	750.24	-1.35	-2.04	90.00	1.094	2	0.00	0.00	0.2605
10'-0" T-arm EPA = 5.7 ft 2 (161 lbs)	60.0000	750.24	2.35	-2.04	90.00	1.094	2	0.00	0.00	0.2605
10'-0" T-arm EPA = 5.7 0'-2" (161 lbs)	180.0000	750.24	0.00	-4.08	90.00	1.094	2	0.00	0.00	0.2605
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-1.34	-2.04	90.00	1.094	2	0.00	0.00	0.2605
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.34	-2.04	90.00	1.094	2	0.00	0.00	0.2605
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	-4.08	90.00	1.094	2	0.00	0.00	0.2605
Sum Weight:		14559.01								

### Discrete Appurtenance Pressures - Service $G_{FR} = 1.100$

Description	Amount Adjoint *	Weight lb	Offset ft	Offset ft	x ft	K <sub>x</sub>	q <sub>x</sub> psf	C.A. Front ft <sup>2</sup>	C.A. Side ft <sup>2</sup>
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-3.30	-1.95	90.00	1.124	8	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.30	-1.95	90.00	1.124	8	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	-3.90	90.00	1.124	8	0.00	0.00
10'-0" T-arm EPA = 5.7 0'-2" (15 lbs)	60.0000	322.00	-3.30	-1.95	90.00	1.124	8	0.00	0.00
10'-0" T-arm EPA = 5.7 0'-2" (15 lbs)	60.0000	322.00	3.30	-1.95	90.00	1.124	8	0.00	0.00
10'-0" T-arm EPA = 5.7 0'-2" (15 lbs)	180.0000	322.00	0.00	-3.90	90.00	1.124	8	0.00	0.00
Generic RRU (Enclosed, 90 lbs)	300.0000	300.00	-3.30	-1.95	90.00	1.124	8	0.00	0.00

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W Calena Park Blvd Draper, UT 84020 Phone: (801) 996-1776 FAX: (801) 996-1776	Job	Page 19 of 131
	Project	Date
	Client	Designed by
	Spike	
	U0142.2054.242	17:04:43 10/24/24
	Raycop	marine

Description	Allowing Demand s	Weight lb	Offset ft	Offset ft	x ft	z ft	ax gpf	C <sub>pe</sub> lb/ft <sup>2</sup>	C <sub>pe</sub> ft <sup>2</sup>
75 lbs)									
Generic RRU (Enclosed, 75 lbs)	40.0000	300.00	3.59	-1.58	70.00	1.174	5	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	19.0000	100.00	0.00	3.92	70.00	1.171	5	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-3.15	2.00	50.00	1.137	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	40.0000	160.00	3.46	-2.00	60.00	1.137	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	136.0000	460.00	0.00	1.00	60.00	1.137	7	0.00	0.00
10'-0" Team EPA = 5.7 ft <sup>2</sup> (161 lbs)	300.0000	322.00	-3.46	-2.00	60.00	1.137	7	0.00	0.00
10'-0" Team EPA = 5.7 ft <sup>2</sup> (161 lbs)	60.0000	322.00	3.46	-2.00	60.00	1.137	7	0.00	0.00
10'-0" Team EPA = 5.7 ft <sup>2</sup> (161 lbs)	180.0000	322.00	0.00	1.00	60.00	1.137	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	500.00	-3.46	-2.00	60.00	1.137	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	50.0000	500.00	3.46	-2.00	60.00	1.137	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	500.00	0.00	1.00	60.00	1.137	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	300.0000	440.00	-3.33	-2.00	50.00	1.094	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	50.0000	440.00	3.33	-2.00	50.00	1.094	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	440.00	0.00	1.00	50.00	1.094	7	0.00	0.00
10'-0" Team EPA = 5.7 ft <sup>2</sup> (161 lbs)	300.0000	322.00	-3.33	-2.00	50.00	1.094	7	0.00	0.00
10'-0" Team EPA = 5.7 ft <sup>2</sup> (161 lbs)	60.0000	322.00	3.33	-2.00	50.00	1.094	7	0.00	0.00
10'-0" Team EPA = 5.7 ft <sup>2</sup> (161 lbs)	180.0000	322.00	0.00	1.00	50.00	1.094	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	50.0000	300.00	-3.33	-2.00	50.00	1.051	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.33	-2.00	50.00	1.051	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	190.0000	300.00	0.00	-1.00	50.00	1.051	7	0.00	0.00
Span Weight		9738.00							

**Force Totals**

Load Case	Vertical Force lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments M <sub>x</sub> lb-ft	Sum of Overturning Moments M <sub>y</sub> lb-ft	Sum of Torques lb-ft
Dead Weight	5043.74					
Decking Weight	0.00					
Total Member Self-Weight	5043.74			0.00	0.00	
Total Weight	21035.74			0.00	0.00	
Wind 0 deg - No Ice		0.00	-16620.39	-910766.37	0.00	0.00
Wind 30 deg - No Ice		8310.20	-14394.68	-790045.87	-476133.15	0.00
Wind 45 deg - No Ice		11792.19	-11792.19	-649069.74	-649069.74	0.00
Wind 60 deg - No Ice		14293.68	8310.20	-486733.19	-790045.87	0.00

Job	Spike	Page 28 of 131
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Client	Raycap	Designed by mirie

Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Y lb	Sum of Overturning Moments, Mx lb-ft	Sum of Overturning Moments, My lb-ft	Sum of Torques lb-ft
Wind 90 deg - No Ice		16591.99	0.00	0.00	-412596.57	0.00
Wind 120 deg - No Ice		14591.68	8310.20	476195.74	-290046.85	0.00
Wind 150 deg - No Ice		11752.39	11752.39	643069.74	-643069.74	0.00
Wind 180 deg - No Ice		8310.20	16791.68	780645.85	-455123.19	0.00
Wind 180 deg - No Ice		0.00	16791.68	912268.20	0.00	0.00
Wind 210 deg - No Ice		8310.20	-1353.68	790645.85	456134.19	0.00
Wind 225 deg - No Ice		-1752.39	11752.39	643069.74	-643069.74	0.00
Wind 240 deg - No Ice		-4393.68	8310.20	456133.19	750313.85	0.00
Wind 270 deg - No Ice		-46620.49	0.00	0.00	912268.20	0.00
Wind 300 deg - No Ice		-4393.68	-8310.20	456133.19	750313.85	0.00
Wind 315 deg - No Ice		-1752.39	-11752.39	-643069.74	-643069.74	0.00
Wind 330 deg - No Ice		8310.20	-1353.68	-790645.85	-456133.19	0.00
Member Ice	641.30					
Total Weight Ice	22022.1			0.00	0.00	
Wind 0 deg - Ice		0.00	-2537.31	-127902.78	0.00	0.00
Wind 30 deg - Ice		1161.73	-2017.35	-110420.66	63751.29	0.00
Wind 45 deg - Ice		1642.26	-1642.26	-90358.38	50158.08	0.00
Wind 60 deg - Ice		2011.25	-1151.25	-65751.39	-10420.66	0.00
Wind 90 deg - Ice		2322.51	0.00	0.00	-37502.78	0.00
Wind 120 deg - Ice		2011.25	1161.73	5921.58	-10420.66	0.00
Wind 135 deg - Ice		1642.26	1642.26	90358.38	-50158.08	0.00
Wind 150 deg - Ice		1161.73	2017.35	110420.66	-63751.29	0.00
Wind 180 deg - Ice		0.00	2322.51	127902.78	0.00	0.00
Wind 210 deg - Ice		-1161.73	2017.35	110420.66	63751.29	0.00
Wind 225 deg - Ice		-1642.26	1642.26	90358.38	50158.08	0.00
Wind 240 deg - Ice		-2011.25	1161.73	5921.58	110420.66	0.00
Wind 270 deg - Ice		-2322.51	0.00	0.00	127902.78	0.00
Wind 300 deg - Ice		2011.25	-1151.25	-65751.39	110420.66	0.00
Wind 315 deg - Ice		-1642.26	-1642.26	-90358.38	50158.08	0.00
Wind 330 deg - Ice		-1161.73	-2017.35	-110420.66	63751.29	0.00
Total Weight	21913.74			0.00	0.00	
Wind 0 deg - Service		0.00	-6575.21	297864.96	0.00	0.00
Wind 30 deg - Service		2586.61	-4653.34	-257958.62	-148932.48	0.00
Wind 45 deg - Service		3799.43	-3799.43	-210622.33	-210622.33	0.00
Wind 60 deg - Service		4552.34	-2686.81	-148932.48	-257958.62	0.00
Wind 90 deg - Service		5373.21	0.00	0.00	-297864.96	0.00
Wind 120 deg - Service		4653.34	2686.81	148932.48	-257958.62	0.00
Wind 135 deg - Service		3799.43	3799.43	210622.33	-210622.33	0.00
Wind 150 deg - Service		2586.61	4653.34	257958.62	-148932.48	0.00
Wind 180 deg - Service		0.00	5373.21	297864.96	0.00	0.00
Wind 210 deg - Service		-2586.61	4653.34	257958.62	148932.48	0.00
Wind 225 deg - Service		-3799.43	3799.43	210622.33	210622.33	0.00
Wind 240 deg - Service		-4552.34	2686.81	148932.48	257958.62	0.00
Wind 270 deg - Service		-5373.21	0.00	0.00	297864.96	0.00
Wind 300 deg - Service		-4653.34	-2686.81	-148932.48	257958.62	0.00
Wind 315 deg - Service		-3799.43	-3799.43	-210622.33	210622.33	0.00
Wind 330 deg - Service		-2586.61	-4653.34	-257958.62	148932.48	0.00

**Load Combinations**

Comb	Description
1	Dead Only
2	1.2 Dead + 1.0 Wind 0 deg - No Ice
3	0.9 Dead + 1.0 Wind 0 deg - No Ice
4	1.2 Dead + 1.0 Wind 90 deg - No Ice

<b>inxTower</b>  <b>Vector Structural Engineering</b> 671 W Galena Park, #102 Denver, CO 80229 Phone: (303) 956-1773 FAX: (303) 990-1776	Job	Spike	Page 21 of 131
	Project	U0142.2054.242	Date
	Client	Raycap	Designed by
			mrie

Comp. No.	Description
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 45 deg - No Ice
7	0.9 Dead+1.0 Wind 45 deg - No Ice
8	1.2 Dead+1.0 Wind 60 deg - No Ice
9	0.9 Dead+1.0 Wind 60 deg - No Ice
10	1.2 Dead+1.0 Wind 90 deg - No Ice
11	0.9 Dead+1.0 Wind 90 deg - No Ice
12	1.2 Dead+1.0 Wind 120 deg - No Ice
13	0.9 Dead+1.0 Wind 120 deg - No Ice
14	1.2 Dead+1.0 Wind 135 deg - No Ice
15	0.9 Dead+1.0 Wind 135 deg - No Ice
16	1.2 Dead+1.0 Wind 150 deg - No Ice
17	0.9 Dead+1.0 Wind 150 deg - No Ice
18	1.2 Dead+1.0 Wind 180 deg - No Ice
19	0.9 Dead+1.0 Wind 180 deg - No Ice
20	1.2 Dead+1.0 Wind 210 deg - No Ice
21	0.9 Dead+1.0 Wind 210 deg - No Ice
22	1.2 Dead+1.0 Wind 225 deg - No Ice
23	0.9 Dead+1.0 Wind 225 deg - No Ice
24	1.2 Dead+1.0 Wind 240 deg - No Ice
25	0.9 Dead+1.0 Wind 240 deg - No Ice
26	1.2 Dead+1.0 Wind 270 deg - No Ice
27	0.9 Dead+1.0 Wind 270 deg - No Ice
28	1.2 Dead+1.0 Wind 300 deg - No Ice
29	0.9 Dead+1.0 Wind 300 deg - No Ice
30	1.2 Dead+1.0 Wind 315 deg - No Ice
31	0.9 Dead+1.0 Wind 315 deg - No Ice
32	1.2 Dead+1.0 Wind 330 deg - No Ice
33	0.9 Dead+1.0 Wind 330 deg - No Ice
34	1.2 Dead+1.0 Ice
35	1.2 Dead+1.0 Wind 0 deg+1.0 Ice
36	1.2 Dead+1.0 Wind 30 deg+1.0 Ice
37	1.2 Dead+1.0 Wind 45 deg+1.0 Ice
38	1.2 Dead+1.0 Wind 60 deg+1.0 Ice
39	1.2 Dead+1.0 Wind 90 deg+1.0 Ice
40	1.2 Dead+1.0 Wind 120 deg+1.0 Ice
41	1.2 Dead+1.0 Wind 135 deg+1.0 Ice
42	1.2 Dead+1.0 Wind 150 deg+1.0 Ice
43	1.2 Dead+1.0 Wind 180 deg+1.0 Ice
44	1.2 Dead+1.0 Wind 210 deg+1.0 Ice
45	1.2 Dead+1.0 Wind 225 deg+1.0 Ice
46	1.2 Dead+1.0 Wind 240 deg+1.0 Ice
47	1.2 Dead+1.0 Wind 270 deg+1.0 Ice
48	1.2 Dead+1.0 Wind 300 deg+1.0 Ice
49	1.2 Dead+1.0 Wind 315 deg+1.0 Ice
50	1.2 Dead+1.0 Wind 330 deg+1.0 Ice
51	Dead+Wind 0 deg - Service
52	Dead+Wind 30 deg - Service
53	Dead+Wind 45 deg - Service
54	Dead+Wind 60 deg - Service
55	Dead+Wind 90 deg - Service
56	Dead+Wind 120 deg - Service
57	Dead+Wind 135 deg - Service
58	Dead+Wind 150 deg - Service
59	Dead+Wind 180 deg - Service
60	Dead+Wind 210 deg - Service
61	Dead+Wind 225 deg - Service
62	Dead+Wind 240 deg - Service
63	Dead+Wind 270 deg - Service
64	Dead+Wind 300 deg - Service
65	Dead+Wind 315 deg - Service
66	Dead+Wind 330 deg - Service

<b>inxTower</b>  <b>Vector Structural Engineering</b> 551 W Cabana Park Blvd Denver, CO 80202 Phone: (303) 950-1777 FAX: (303) 930-1776	<b>Job</b> Spike	<b>Page</b> 22 of 131
	<b>Project</b> U0142.2054.242	<b>Date</b> 17:04:43 10/24/24
	<b>Client</b> Raycap	<b>Designed by</b> mrrie

### Maximum Member Forces

Section No.	Direction #	Component Type	Condition	Gen. Load Comb.	Area lb	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
1.1	75-25	Pole	Max. Tension	33	0.00	0.00	-0.00
			Max. Compression	34	22726.73	0.00	0.00
			Max. Mx	10	-21330.45	-438073.86	0.00
			Max. My	1	-21330.45	0.00	488073.86
			Max. Vx	10	16039.32	-488073.86	0.00
			Max. Vy	2	-16039.32	0.00	-488073.86
			Max. Torque	16	0.00	0.00	0.00
1.2	25-1	Pole	Max. Tension	7	0.00	0.00	0.00
			Max. Compression	74	-26268.73	0.00	0.00
			Max. Mx	10	-25241.11	-496122.99	0.00
			Max. My	15	-25241.11	0.00	-496122.99
			Max. Vx	10	16657.49	-496122.99	0.00
			Max. Vy	15	16657.49	0.00	-496122.99
			Max. Torque	16	0.00	0.00	0.00

### Maximum Reactions

Location	Condition	Gen. Load Comb.	Vertical lb	Horizontal X lb	Horizontal Y lb
Pole	Max. Vert	74	26268.73	0.00	0.00
	Max. Hx	27	18932.16	16620.17	0.00
	Max. Hy	3	18932.16	0.00	16620.17
	Max. Mx	7	95022.99	0.00	16620.16
	Max. My	10	95022.99	-16620.16	0.00
	Max. Tension	16	0.00	8310.17	-14495.64
	Min. Vx	3	18932.16	0.00	16620.17
	Min. Hx	11	18932.16	-16620.17	0.00
	Min. Hy	19	18932.16	0.00	-16620.17
	Min. Mx	18	-55022.99	0.00	-16620.16
	Min. My	26	-55022.99	16620.16	0.00
	M = Tension	20	0.00	8310.17	-14393.63

### Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear X lb	Shear Y lb	Overswing Moment X lb-ft	Overswing Moment Y lb-ft	Torque lb-ft
Dead Only	21025.91	0.00	0.00	0.00	0.00	0.00
1.2 Dead+1.0 Wind 0 deg - No Ice	15742.87	0.00	-16620.16	-55022.99	0.00	0.00
0.9 Dead+1.0 Wind 0 deg - No Ice	4952.16	0.00	-16620.17	-430156.89	0.00	0.00
1.5 Dead+1.0 Wind 30 deg - No Ice	25242.88	8310.17	-14495.64	-822848.76	-79071.71	0.00
0.9 Dead+1.0 Wind 30 deg - No Ice	18932.16	8310.18	-14393.63	814200.56	-423684.71	0.00

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W. Granger Park Blvd Granger, UT 84629 Phone: (801) 996-1777 FAX: (801) 996-1776	Job	Page 23 of 131
	Project	Date
	Client	Designed by
	Spike	
	U0142.2054.242	17:04:48 10/24/24
	Raycap	mrrile

Load Combination	Vertical lb	Shear lb	Wear lb	Overturning Moment, M <sub>o</sub> lb-ft	Overturning Moment, M <sub>o</sub> lb-ft	Torque lb-ft
1.1 Dead-1.0 Wind 45 deg - No Ice	25242.88	11752.35	-11752.35	-671851.82	-671352.82	0.00
1.0 Dead-1.0 Wind 45 deg - No Ice	18951.16	11752.37	-11752.37	-664800.16	-664800.16	0.00
1.2 Dead+1.0 Wind 60 deg - No Ice	25242.88	14393.53	-4310.17	-475371.71	-822448.26	-0.00
0.9 Dead+1.0 Wind 60 deg - No Ice	18952.15	14393.57	-8310.18	-470064.71	-814210.56	-0.00
1.2 Dead+1.0 Wind 90 deg - No Ice	25242.87	16620.07	0.00	0.00	-990122.95	0.00
0.9 Dead+1.0 Wind 90 deg - No Ice	18952.16	16620.17	0.00	0.00	-940155.89	0.00
1.2 Dead+1.0 Wind 120 deg - No Ice	25242.88	-14393.53	8310.17	-75071.71	-822848.26	0.00
0.9 Dead+1.0 Wind 120 deg - No Ice	18952.16	-14393.55	8310.18	-75081.71	-814210.56	0.00
1.2 Dead+1.0 Wind 135 deg - No Ice	25242.88	11752.35	11752.35	671852.82	-671852.82	0.00
0.9 Dead+1.0 Wind 135 deg - No Ice	18952.16	11752.37	11752.37	664800.16	-664800.16	0.00
1.2 Dead+1.0 Wind 150 deg - No Ice	25242.88	8310.17	14393.53	822818.26	-475371.71	-0.00
0.9 Dead+1.0 Wind 150 deg - No Ice	18952.16	8310.18	14393.55	814210.56	-470064.71	-0.00
1.2 Dead+1.0 Wind 180 deg - No Ice	25242.87	0.00	16620.07	990122.95	0.00	0.00
0.9 Dead+1.0 Wind 180 deg - No Ice	18952.16	0.00	16620.17	940155.89	0.00	0.00
1.2 Dead+1.0 Wind 210 deg - No Ice	25242.88	-8310.17	14393.53	822848.26	-475371.71	0.00
0.9 Dead+1.0 Wind 210 deg - No Ice	18952.16	-8310.18	14393.57	814210.56	-470064.71	0.00
1.2 Dead+1.0 Wind 225 deg - No Ice	25242.88	-11752.35	11752.35	-671851.82	671352.82	0.00
0.9 Dead+1.0 Wind 225 deg - No Ice	18952.16	-11752.37	11752.37	-664800.16	664800.16	0.00
1.2 Dead+1.0 Wind 240 deg - No Ice	25242.88	-14393.53	-8310.17	-475371.71	-822448.26	-0.00
0.9 Dead+1.0 Wind 240 deg - No Ice	18952.15	-14393.57	-8310.18	-470064.71	-814210.56	-0.00
1.2 Dead+1.0 Wind 270 deg - No Ice	25242.87	-16620.07	0.00	0.00	990122.95	0.00
0.9 Dead+1.0 Wind 270 deg - No Ice	18952.15	-16620.17	-0.00	0.00	940155.89	0.00
1.2 Dead+1.0 Wind 300 deg - No Ice	25242.88	-14393.53	-8310.17	-475371.71	-822818.26	0.00
0.9 Dead+1.0 Wind 300 deg - No Ice	18952.15	-14393.57	-8310.18	-470064.71	-814210.56	0.00
1.2 Dead+1.0 Wind 315 deg - No Ice	25242.88	-11752.35	-11752.35	-671852.82	671852.82	0.00
0.9 Dead+1.0 Wind 315 deg - No Ice	18952.15	-11752.37	-11752.37	-664800.16	664800.16	0.00
1.2 Dead+1.0 Wind 330 deg - No Ice	25242.88	-4310.17	-14393.53	-822848.26	-475371.71	-0.00
0.9 Dead+1.0 Wind 330 deg - No Ice	18952.15	-4310.18	-14393.55	-814210.56	-470064.71	-0.00
1.2 Dead+1.0 Ice	26268.55	0.00	0.00	0.00	0.00	0.00
1.2 Dead+1.0 Wind 0 deg-1.0 Ice	26268.51	0.00	-7321.18	-132960.58	0.00	0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice	26268.51	-1660.64	-2010.79	-115173.25	-66465.30	0.00

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 3 <sup>rd</sup> Calumet Park Blvd Chicago, IL 60620 Phone: (815) 496-1775 FAX: (815) 990-1776	Job	Spike	Page 24 of 131
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Load Combination	Vertical k	Major k	Minor k	Overturning Moment M <sub>x</sub> k-ft	Overturning Moment M <sub>y</sub> k-ft	Torque k-ft
1.2 Dead+1.0 Wind 45 deg+1.0 Ice	26268.51	1641.39	-1641.39	94038.55	-94038.55	0.00
1.2 Dead+1.0 Wind 50 deg+1.0 Ice	26268.51	2010.29	-160.64	-66495.30	-113175.34	-0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice	26268.51	2321.28	0.00	0.00	-152990.98	0.00
1.2 Dead+1.0 Wind 140 deg+1.0 Ice	26268.51	2010.29	160.64	66495.30	-113175.34	0.00
1.2 Dead+1.0 Wind 135 deg+1.0 Ice	26268.51	1641.39	1641.39	94038.55	94038.55	0.00
1.2 Dead+1.0 Wind 150 deg+1.0 Ice	26268.51	1160.64	2010.29	-15173.25	-66495.30	-0.00
1.2 Dead+1.0 Wind 180 deg+1.0 Ice	26268.51	0.00	2321.28	122990.98	0.00	0.00
1.2 Dead+1.0 Wind 210 deg+1.0 Ice	26268.51	1160.64	2010.29	113175.34	66495.30	0.00
1.2 Dead+1.0 Wind 225 deg+1.0 Ice	26268.51	-1641.39	1641.39	94038.55	94038.55	0.00
1.2 Dead+1.0 Wind 270 deg+1.0 Ice	26268.51	-2010.29	1160.64	66495.30	-15173.25	-0.00
1.2 Dead+1.0 Wind 270 deg+1.0 Ice	26268.51	2321.28	0.00	0.00	-122990.98	0.00
1.2 Dead+1.0 Wind 300 deg+1.0 Ice	26268.51	-2010.29	-1160.64	-66495.30	-15173.25	0.00
1.2 Dead+1.0 Wind 315 deg+1.0 Ice	26268.51	-1641.39	-1641.39	-94038.55	94038.55	0.00
1.2 Dead+1.0 Wind 330 deg+1.0 Ice	26268.51	-1160.64	-2010.29	-113175.34	66495.30	-0.00
Dead+Wind 0 deg - Service	21035.75	0.00	-5492.91	-308215.42	0.00	0.00
Dead+Wind 45 deg - Service	21035.75	2680.37	-1552.93	-256932.40	-517941.24	0.00
Dead+Wind 45 deg - Service	21035.75	3799.11	-3799.11	-3799.11	-517941.24	0.00
Dead+Wind 60 deg - Service	21035.75	4652.93	-2680.37	-154107.24	-308215.42	-0.00
Dead+Wind 90 deg - Service	21035.75	5492.91	0.00	0.00	-308215.42	0.00
Dead+Wind 120 deg - Service	21035.75	4652.93	2680.37	154107.24	-308215.42	0.00
Dead+Wind 135 deg - Service	21035.75	3799.11	3799.11	217941.24	-517941.24	0.00
Dead+Wind 150 deg - Service	21035.75	2680.37	4652.93	268922.40	-517941.24	0.00
Dead+Wind 180 deg - Service	21035.75	0.00	5492.91	308215.42	0.00	0.00
Dead+Wind 210 deg - Service	21035.75	-2680.37	4652.93	268932.40	154107.24	0.00
Dead+Wind 225 deg - Service	21035.75	-3799.11	3799.11	217941.24	217941.24	0.00
Dead+Wind 240 deg - Service	21035.75	-4652.91	2680.37	154107.24	268922.40	0.00
Dead+Wind 270 deg - Service	21035.75	-5492.91	0.00	0.00	308215.42	0.00
Dead+Wind 300 deg - Service	21035.75	-4652.91	-2680.37	-154107.24	268932.40	0.00
Dead+Wind 315 deg - Service	21035.75	-3799.11	-3799.11	-217941.24	217941.24	0.00
Dead+Wind 330 deg - Service	21035.75	-2680.37	-4652.91	-268932.40	154107.24	-0.00

## Solution Summary

Load Comb.	FX k	Sum of Applied Forces			FY k	Sum of Reactions			% Drift
		F1 k	F2 k	F3 k		R1 k	R2 k	R3 k	
1	0.00	-21035.74	0.00	0.00	21035.74	0.00	0.00	0.00%	
2	0.00	-25242.88	-4992.91	0.00	25242.87	6620.65	0.00	0.00%	
3	0.00	18932.16	-1620.39	0.00	18932.16	6620.17	0.00%	0.00%	
4	8310.20	-25242.88	-14353.58	-8310.17	25242.88	14393.63	0.00%	0.00%	
5	8310.20	-18712.18	-14353.58	-8310.18	18712.16	14393.63	0.00%	0.00%	
6	11752.99	-25242.88	-11752.99	-11752.99	25242.88	11752.99	0.00%	0.00%	
7	11752.99	-18942.16	-11752.99	-11752.99	18942.16	11752.99	0.00%	0.00%	
8	14393.63	-25242.88	-8310.20	-4992.63	25242.88	8310.17	0.00%	0.00%	

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Load Comb.	Sum of Applied Forces				Sum of Reactions		% Error
	PX lb	PY lb	PZ lb	RY lb	RF lb	RZ lb	
9	-14393.68	-18932.16	-8310.20	-14393.68	18932.16	8310.18	0.001%
10	16620.99	-1752.38	0.00	-16620.99	25242.87	0.00	0.001%
11	16620.99	-18932.16	0.00	-16620.99	18932.15	0.00	0.001%
12	14393.68	-25242.88	5310.20	-14393.68	7572.88	5310.17	0.000%
13	14393.68	-18932.16	8310.20	-14393.68	18932.15	-8310.18	0.000%
14	11752.39	-25242.88	11752.39	-11752.39	25242.88	-11752.38	0.000%
15	11752.39	-18932.16	11752.39	-11752.39	18932.16	-11752.37	0.000%
16	8310.20	-25242.88	-14393.68	-8310.20	25242.88	-14393.64	0.000%
17	8310.20	-18932.16	-14393.68	-8310.20	18932.16	-14393.63	0.000%
18	0.00	-25242.88	16620.99	0.00	25242.87	-16620.98	0.001%
19	0.00	18932.16	16620.99	0.00	18932.16	-16620.99	0.001%
20	-8310.20	-25242.88	14393.68	8310.17	7572.88	-14393.63	0.000%
21	-8310.20	-18932.16	14393.68	8310.15	8310.17	-14393.63	0.000%
22	-11752.39	-25242.88	11752.39	11752.37	25242.88	-11752.35	0.000%
23	-11752.39	-18932.16	11752.39	11752.37	18932.16	-11752.37	0.000%
24	-14393.68	-25242.88	8310.20	-14393.68	7572.88	8310.17	0.000%
25	-14393.68	-18932.16	8310.20	-14393.68	18932.16	-8310.18	0.000%
26	-16620.99	25242.88	0.00	16620.99	25242.87	0.00	0.001%
27	-16620.99	-18932.16	0.00	16620.99	18932.15	0.00	0.001%
28	-14393.68	-1752.38	-8310.20	-14393.68	25242.88	8310.17	0.000%
29	-14393.68	-18932.16	-8310.20	-14393.68	18932.15	8310.15	0.000%
30	-11752.39	-25242.88	-11752.39	-11752.39	25242.88	11752.38	0.000%
31	-11752.39	-18932.16	-11752.39	-11752.39	18932.15	11752.39	0.000%
32	8310.20	-25242.88	8310.20	8310.17	7572.88	-14393.64	0.000%
33	8310.20	-18932.16	-14393.68	8310.18	18932.16	-14393.63	0.000%
34	0.00	-26268.51	0.00	0.00	26268.51	0.00	0.000%
35	0.00	-26268.51	-2111.35	0.00	26268.51	2111.34	0.000%
36	1161.25	-26268.51	-2111.35	-1161.25	26268.51	2111.29	0.000%
37	1542.26	-26268.51	-1642.26	-1641.99	26268.51	1641.99	0.000%
38	2010.29	-26268.51	-1161.25	-2010.29	26268.51	1161.64	0.000%
39	2321.28	-26268.51	0.00	2321.28	26268.51	0.00	0.000%
40	2710.35	-26268.51	1161.25	-2710.29	26268.51	-1161.54	0.000%
41	1642.26	-26268.51	1642.26	-1641.99	26268.51	-1641.99	0.000%
42	1161.25	-26268.51	2010.29	1161.64	26268.51	-2010.29	0.000%
43	0.00	-26268.51	2321.28	0.00	26268.51	-2321.28	0.000%
44	-1161.25	26268.51	2010.29	-1161.64	26268.51	-2010.29	0.000%
45	-1542.26	26268.51	1642.26	-1641.99	26268.51	-1641.99	0.000%
46	-2010.29	26268.51	1161.25	-2010.29	26268.51	-1161.64	0.000%
47	-2321.28	26268.51	0.00	2321.28	26268.51	0.00	0.000%
48	-2710.35	26268.51	-1161.25	2710.29	26268.51	1161.64	0.000%
49	-1642.26	26268.51	-1642.26	1641.99	26268.51	1641.99	0.000%
50	-1161.25	26268.51	-2010.29	1161.64	26268.51	2010.29	0.000%
51	0.00	-21035.73	3799.41	0.00	21035.73	3799.41	0.000%
52	2686.57	-21035.73	-4652.37	-2686.57	21035.73	-4652.37	0.000%
53	3799.41	-21035.73	-3799.41	-3799.41	21035.73	3799.41	0.000%
54	4652.37	-21035.73	-2686.57	-4652.37	21035.73	-2686.57	0.000%
55	5372.75	-21035.73	0.00	-5372.75	21035.73	0.00	0.000%
56	6084.13	-21035.73	2556.61	-6084.13	21035.73	-2556.61	0.000%
57	7999.41	-21035.73	3799.41	-7999.41	21035.73	-3799.41	0.000%
58	7685.61	-21035.73	4652.37	-7685.61	21035.73	-4652.37	0.000%
59	0.00	-21035.73	5372.75	0.00	21035.73	-5372.75	0.000%
60	2686.57	-21035.73	1521.34	2686.57	21035.73	-1521.34	0.000%
61	3799.41	-21035.73	3799.41	3799.41	21035.73	-3799.41	0.000%
62	-6084.13	-21035.73	2556.61	-6084.13	21035.73	-2556.61	0.000%
63	-3799.41	-21035.73	0.00	-3799.41	21035.73	0.00	0.000%
64	-4652.37	-21035.73	-2686.57	-4652.37	21035.73	2686.57	0.000%
65	-1799.41	-21035.73	-3799.41	-1799.41	21035.73	3799.41	0.000%
66	-2686.57	-21035.73	-4652.37	-2686.57	21035.73	-4652.37	0.000%

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 231 W. Galena, Park Place Chicago, IL 60606 Phone: (861) 599-1775 FAX: (861) 856-1776	Job	Spike	Page 26 of 131
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			mmic

### Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.0000001	0.0000001
2	Yes	10	0.0000001	0.0000397
3	Yes	10	0.0000001	0.0003526
4	Yes	11	0.0000001	0.0006147
5	Yes	11	0.0000001	0.0004761
6	Yes	11	0.0000001	0.0005055
7	Yes	11	0.0000001	0.0005254
8	Yes	11	0.0000001	0.0006177
9	Yes	17	0.0000001	0.0004591
10	Yes	10	0.0000001	0.0003955
11	Yes	10	0.0000001	0.0004396
12	Yes	12	0.0000001	0.0006177
13	Yes	12	0.0000001	0.0004591
14	Yes	17	0.0000001	0.0005055
15	Yes	17	0.0000001	0.0005761
16	Yes	17	0.0000001	0.0006147
17	Yes	11	0.0000001	0.0004761
18	Yes	10	0.0000001	0.0004762
19	Yes	10	0.0000001	0.0004766
20	Yes	11	0.0000001	0.0005177
21	Yes	11	0.0000001	0.0004761
22	Yes	11	0.0000001	0.0003706
23	Yes	11	0.0000001	0.0004594
24	Yes	11	0.0000001	0.0005149
25	Yes	11	0.0000001	0.0004591
26	Yes	10	0.0000001	0.0004592
27	Yes	10	0.0000001	0.0005766
28	Yes	11	0.0000001	0.0006147
29	Yes	11	0.0000001	0.0004591
30	Yes	11	0.0000001	0.0003056
31	Yes	11	0.0000001	0.0005254
32	Yes	11	0.0000001	0.0006147
33	Yes	11	0.0000001	0.0004591
34	Yes	6	0.0000001	0.0000001
35	Yes	8	0.0000001	0.0007999
36	Yes	8	0.0000001	0.0007527
37	Yes	8	0.0000001	0.0007596
38	Yes	8	0.0000001	0.0007527
39	Yes	5	0.0000001	0.0002999
40	Yes	5	0.0000001	0.0002527
41	Yes	5	0.0000001	0.0003366
42	Yes	5	0.0000001	0.0002527
43	Yes	5	0.0000001	0.0002999
44	Yes	5	0.0000001	0.0002527
45	Yes	5	0.0000001	0.0003366
46	Yes	5	0.0000001	0.0003377
47	Yes	5	0.0000001	0.0002999
48	Yes	5	0.0000001	0.0002527
49	Yes	5	0.0000001	0.0002366
50	Yes	5	0.0000001	0.0002527
51	Yes	9	0.0000001	0.0003156
52	Yes	9	0.0000001	0.0003507
53	Yes	9	0.0000001	0.0002527
54	Yes	9	0.0000001	0.0003507
55	Yes	9	0.0000001	0.0003507
56	Yes	9	0.0000001	0.0003507
57	Yes	9	0.0000001	0.0003507

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58	Yes	9	0.0000001	0.00005807
59	Yes	9	0.0000001	0.00007196
60	Yes	9	0.0000001	0.00005807
61	Yes	9	0.0000001	0.00005262
62	Yes	9	0.0000001	0.00005807
63	Yes	9	0.0000001	0.00007196
64	Yes	9	0.0000001	0.00005807
65	Yes	9	0.0000001	0.00005262
66	Yes	9	0.0000001	0.00005807

**Maximum Tower Deflections - Service Wind**

Section No.	Elevation ft	Max. Deflection in	Gen. Load Comb.	Tilt °	Torsion °
L1	75 - 25	10.110	59	1.6418	0.0000
L2	29.25 - 1	1.580	59	0.6258	0.0000

**Critical Deflections and Radius of Curvature - Service Wind**

Elevation ft	Appearance	Gen. Load Comb.	Deflection in	Tilt °	Torsion °	Radius of Curvature ft
75.00	Concealment Leading @ 25 ft	59	10.110	1.6418	0.0000	217.3
90.00	(4) Generic Panel (Enclosed, 115 lbs)	59	3.999	0.9965	0.0000	217.3
61.00	Concealment Leading @ 95 ft	59	7.905	0.9906	0.0000	108.7
60.00	(4) Generic Panel (Enclosed, 115 lbs)	59	6.850	0.6400	0.0000	92.6
33.00	Concealment Leading @ 95 ft	59	3.801	0.8579	0.0000	5428
30.00	(4) Generic Panel (Enclosed, 115 lbs)	59	4.827	0.7906	0.0000	494.2
45.00	Concealment Leading @ 95 ft	59	1.922	0.7432	0.0000	4618

**Maximum Tower Deflections - Design Wind**

Section No.	Elevation ft	Max. Deflection in	Gen. Load Comb.	Tilt °	Torsion °
L1	75 - 25	31.197	18	3.9647	0.0000
L2	29.75 - 1	3.175	18	1.6194	0.0000

**Critical Deflections and Radius of Curvature - Design Wind**

Elevation ft	Appearance	Gen. Load Comb.	Deflection in	Tilt °	Torsion °	Radius of Curvature ft
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<b>tnxTower</b>  <b>Vector Structural Engineering</b> 651 W. Ganssow Park Blvd Cooper, UT 84629 Phone: (907) 956-1775 FAX: (907) 992-1776	Job	Spike	Page 28 of 131
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Elevation ft	Appearance	Conc. Load Cush	Deflection in	Job "	Dist "	Radius of Curvature ft
75.00	Concealment Loading @ 75 ft	18	21.67	1.2917	0.0000	7914
73.00	(4) Generic Panel (Enclosed, 115 lbs)	18	27.687	1.6680	0.0000	7914
65.00	Concealment Loading @ 65 ft	18	24.410	1.9249	0.0000	1516
63.00	(4) Generic Panel (Enclosed, 115 lbs)	18	21.617	1.7787	0.0000	2264
55.00	Concealment Loading @ 55 ft	18	17.352	2.6251	0.0000	1772
53.00	(4) Generic Panel (Enclosed, 115 lbs)	18	14.357	2.5612	0.0000	1417
15.00	Concealment Loading @ 45 ft	18	13.025	1.7890	0.0000	1130

### Compression Checks

### Pole Design Data

Section No	Elevation ft	WxH	I <sub>x</sub> ft <sup>4</sup>	I <sub>y</sub> ft <sup>4</sup>	K <sub>1</sub>	d <sub>1</sub> in <sup>2</sup>	P <sub>1</sub> lb	e <sub>1</sub> in	Ratio			
									$\frac{P_1}{e_1}$			
1.1	75 - 73.5921	TP30.75x2.50.1875	80.00	0.00	0.0	12.6615	-1215.91	7.0930.00	0.002			
	72.5921 - 70.1942								12.9449	-1355.66	757075.00	0.002
	70.1942 - 67.7963								13.2273	-1499.62	723424.00	0.007
	67.7963 - 65.3981								13.5098	-1647.77	789971.00	0.007
	65.3981 - 62.9995								13.7922	-1799.19	85681.00	0.010
	62.9995 - 60.6005								14.0745	-1953.80	823661.00	0.010
	60.6005 - 58.2015								14.3567	-2111.53	839012.00	0.014
	58.2015 - 55.8025								14.6389	-2272.40	853867.00	0.014
	55.8025 - 53.4035								14.9210	-2436.43	868220.00	0.017
	53.4035 - 51.0045								15.2031	-2603.63	882075.00	0.017
	51.0045 - 48.6055								15.4852	-2773.99	895434.00	0.021
	48.6055 - 46.2065								15.7673	-2947.50	908299.00	0.021
	46.2065 - 43.8075								16.0494	-3124.17	920671.00	0.022
	43.8075 - 41.4085								16.3315	-3303.99	932551.00	0.022
	41.4085 - 39.0095								16.6136	-3486.97	943940.00	0.021
	39.0095 - 36.6105								16.8957	-3673.10	954840.00	0.021
	36.6105 - 34.2115								17.1778	-3862.39	965251.00	0.021
	34.2115 - 31.8125								17.4599	-4054.83	975174.00	0.021
	31.8125 - 29.4135								17.7420	-4250.42	984610.00	0.021

<b>inxTower</b>  <b>Vector Structural Engineering</b> 611 W. Collins Park Blvd Draper, UT 84020 Phone: (801) 990-1170 FAX: (801) 990-1770	<b>Job</b> Spike	Page 29 of 137
	<b>Project</b> U0142.2054.242	<b>Date</b> 17:04:43 10/24/24
	<b>Client</b> Raycap	<b>Designed by</b> mrfife

Section No.	Dimension $\beta$	Size	$I$ $\beta^4$	$I_c$ $\beta^4$	$R_{I\beta}$	$Z$ $in^3$	$P_c$ $\beta^3$	$\#P_c$ $\beta^3$	Ratio $\frac{P_c}{\#P_c}$				
L1	29.25												
	29.25 - 25	TP35 (Covered) 6464 at 25	78.77	0.00	0.0	18.7885	-7629.76	1051030.00	0.009				
	29.25 - 25					25.4642	-72657.30	1395400.00	0.009				
	25 - 25.7368					25.0996	-72459.40	1402810.00	0.016				
	25.7368 -					24.2991	-72581.80	1421260.00	0.016				
	22.4777												
	22.4777 -					24.4605	-72729.60	1432700.00	0.016				
	21.2105												
	21.2105 -					24.0850	-72876.60	1444130.00	0.016				
	19.9474												
	19.9474 -					24.5814	-73025.00	1455560.00	0.016				
	18.6842												
	18.6842 -					25.0759	-73174.60	1467000.00	0.016				
	17.4211												
	17.4211 -					25.2723	-73325.50	1478430.00	0.016				
	16.1579												
	16.1579 -					25.4678	-73477.70	1489870.00	0.016				
	14.8947												
	14.8947 -					25.6633	-73631.10	1501300.00	0.016				
	13.6315												
13.6315 -	25.8587					-73785.70	1512730.00	0.016					
12.3684													
12.3684 -	26.0542	-73941.30	1524170.00	0.016									
11.1053													
11.1053 -	26.2496	-74098.60	1535600.00	0.016									
9.8421													
9.8421 -	26.4451	-74256.90	1547040.00	0.016									
8.57895													
8.57895 -	26.6405	-74416.30	1558470.00	0.016									
7.31579													
7.31579 -	26.8359	-74576.90	1569900.00	0.016									
6.05263													
6.05263 -	27.0314	-74738.70	1581330.00	0.016									
4.78947													
4.78947 -	27.2259	-74901.70	1592760.00	0.016									
3.52632													
3.52632 -	27.4225	-75065.90	1604190.00	0.016									
2.26316													
2.26316 - 1	27.6178	-75231.10	1615640.00	0.016									

### Pole Bending Design Data

Section No.	Dimension $\beta$	Size	$AC_c$ $\beta^3$	$AC_c$ $\beta^3$	Ratio $\frac{AC_c}{\beta^3}$	$AC_c$ $\beta^3$	$u_{d\beta}$ $\beta^3$	Ratio $\frac{AC_c}{\beta^3}$	
L1	75 - 72.5921	(P50) 75x75 at 1573	6755.77	197586.67	0.017	0.00	392385.67	0.000	
	72.5921		13752.08	407269.17	0.034	0.00	477969.17	0.000	
	70.1842		51475.33	477531.67	3.651	0.00	122301.67	0.000	
	67.7763								
	67.7763 -		29477.67	477475.00	1.067	0.00	477475.00	0.000	
	65.3684								
	65.3684 -		15388.12	152781.60	0.003	0.00	152781.60	0.000	
	62.9605								
	62.9605 -		55743.25	158214.13	0.140	0.00	158214.13	0.000	
	60.5526								

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Member No.	Direction	Dist	$M_x$	$M_y$	End $M_x$	$M_y$	$M_z$	End $M_z$
	$\theta$		$\theta$	$\theta$	$\theta$	$\theta$	$\theta$	$\theta$
	60.5526 -		57125.90	-433755.00	0.776	0.00	494265.00	0.000
	58.1447 -							
	58.1447 -		106051.00	496125.00	0.210	0.00	496125.00	0.000
	55.7504 -							
	55.7504 -		120115.60	513191.60	0.337	0.00	513191.60	0.000
	53.3289 -							
	53.3289 -		163520.80	531050.60	0.406	0.00	531050.60	0.000
	50.9211 -							
	50.9211 -		193385.80	547000.00	0.337	0.00	547000.00	0.000
	48.5132 -							
	48.5132 -		224613.20	563078.30	0.259	0.00	563078.30	0.000
	46.1053 -							
	46.1053 -		253356.60	579129.10	0.448	0.00	579129.10	0.000
	43.6974 -							
	43.6974 -		285091.00	595295.00	0.459	0.00	595295.00	0.000
	41.2892 -							
	41.2892 -		333000.00	611516.30	0.348	0.00	611516.30	0.000
	38.8816 -							
	38.8816 -		378056.00	627791.00	0.254	0.00	627791.00	0.000
	36.4739 -							
	36.4739 -		411260.00	644107.50	0.628	0.00	644107.50	0.000
	34.0658 -							
	34.0658 -		445604.10	660457.50	0.681	0.00	660457.50	0.000
	31.6579 -							
	31.6579 -		480084.10	676854.10	0.721	0.00	676854.10	0.000
	29.25 -							
	29.25 -	11945.051x29.3465x0.25	244523.30	703782.50	0.346	0.00	703782.50	0.000
	26.8427 -		311957.80	720953.00	0.305	0.00	720953.00	0.000
	24.4348 -		379929.10	738174.60	0.335	0.00	738174.60	0.000
	22.0269 -		447910.00	755500.00	0.365	0.00	755500.00	0.000
	19.6190 -							
	19.6190 -		515921.60	772948.50	0.376	0.00	772948.50	0.000
	17.2111 -							
	17.2111 -		583954.10	790556.60	0.386	0.00	790556.60	0.000
	14.8032 -							
	14.8032 -		651986.60	808306.60	0.359	0.00	808306.60	0.000
	12.3953 -							
	12.3953 -		720000.00	826208.30	0.609	0.00	826208.30	0.000
	10.0000 -							
	10.0000 -		788000.00	844350.00	0.620	0.00	844350.00	0.000
	7.6051 -							
	7.6051 -		856000.00	862700.00	0.630	0.00	862700.00	0.000
	5.2102 -							
	5.2102 -		924000.00	881350.00	0.630	0.00	881350.00	0.000
	2.8153 -							
	2.8153 -		992000.00	900300.00	0.677	0.00	900300.00	0.000
	0.4204 -							
	0.4204 -		1060000.00	920000.00	0.686	0.00	920000.00	0.000
	0.0000 -							
	0.0000 -		1128000.00	940000.00	0.695	0.00	940000.00	0.000
	0.0000 -							
	0.0000 -		1196000.00	960000.00	0.703	0.00	960000.00	0.000
	0.0000 -							
	0.0000 -		1264000.00	980000.00	0.711	0.00	980000.00	0.000

<b>inxTower</b>  <b>Vector Structural Engineering</b> 671 W. Collins Road, Suite Denver, CO 80221 Phone: (303) 996-1775 Fax: (303) 999-8736	Job	Page 31 of 131
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	Client	Designed by
	Spike	
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	Raycap	mirrie

Section No.	Elevation $\bar{y}$	Size	$M_x$ $\bar{y}-\bar{y}_c$	$\sigma_{M_x}$ $\bar{y}-\bar{y}_c$	Ratio $\frac{M_x}{\phi M_n}$ $\bar{y}-\bar{y}_c$	$M_y$ $\bar{y}-\bar{y}_c$	$\sigma_{M_y}$ $\bar{y}-\bar{y}_c$	Ratio $\frac{M_y}{\phi M_n}$ $\bar{y}-\bar{y}_c$
	1.52042							
	1.52042 -		929166.67	1561875.00	0.719	0.00	1561875.00	0.000
	2.263.6							
	2.263.6 -		950141.67	1566791.67	0.727	0.00	1566791.67	0.000

### Pole Shear Design Data

Section No.	Elevation $\bar{y}$	Size	Actual $V_x$ $\bar{y}$	$\phi V_x$ $\bar{y}$	Ratio $\frac{V_x}{\phi V_n}$ $\bar{y}-\bar{y}_c$	Actual $V_y$ $\bar{y}-\bar{y}_c$	$\phi V_y$ $\bar{y}-\bar{y}_c$	Ratio $\frac{V_y}{\phi V_n}$ $\bar{y}-\bar{y}_c$	
11	0.0 - 0.0941	IP50 150x210x18.75	2850.91	2222.95.00	0.015	0.00	414258.33	0.000	
	0.0941 -		2950.90	227183.00	0.015	0.00	432762.00	0.000	
	0.1882								
	0.1882 -		3274.97	332087.00	0.014	0.00	431643.00	0.000	
	0.2823								
	0.2823 -		3370.62	246991.00	0.014	0.00	430932.33	0.000	
	0.3764								
	0.3764 -		3821.63	241845.00	0.032	0.00	450625.00	0.000	
	0.4705								
	0.4705 -		3575.58	246799.00	0.032	0.00	516790.00	0.000	
	0.5646								
	0.5646 -		3394.33	257704.00	0.035	0.00	541218.33	0.000	
	0.6587								
	0.6587 -		3130.42	256608.00	0.032	0.00	557170.00	0.000	
	0.7528								
	0.7528 -		12579.60	267312.00	0.048	0.00	573425.00	0.000	
	0.8469								
	0.8469 -		12590.00	268415.00	0.048	0.00	591135.33	0.000	
	0.9410								
	0.9410 -		12946.70	271370.00	0.048	0.00	617245.00	0.000	
	0.9410 -								
	1.0351								
	1.0351 -		13007.30	276075.00	0.049	0.00	633460.00	0.000	
	1.1292								
	1.1292 -		13569.00	281788.00	0.050	0.00	660788.33	0.000	
	1.2233								
	1.2233 -		15751.00	286902.00	0.051	0.00	685900.00	0.000	
	1.3174								
	1.3174 -		17798.80	290996.00	0.054	0.00	709725.00	0.000	
	1.4115								
	1.4115 -		18853.00	295840.00	0.054	0.00	732852.33	0.000	
1.5056									
1.5056 -	19521.40	300744.00	0.055	0.00	758587.00	0.000			
1.6000									
1.6000 -	19885.90	305648.00	0.052	0.00	783319.33	0.000			
1.6941									
1.6941 -	19039.80	310552.00	0.037	0.00	808497.00	0.000			
1.7882									
1.7882 -	7775.53	317908.00	0.032	0.00	854366.00	0.000			
1.8823									
1.8823 -	9028.32	416618.00	0.022	0.00	1106775.00	0.000			
1.9764									
1.9764 -	19216.90	422549.00	0.038	0.00	1124511.67	0.000			
2.0705									
2.0705 -	16241.50	426279.00	0.038	0.00	1147966.67	0.000			
2.1646									
2.1646 -	16566.70	429809.00	0.038	0.00	1167789.33	0.000			
2.2587									
2.2587 -	16240.50	433239.00	0.034	0.00	1182250.00	0.000			

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 611 W. Collins Park Blvd Chicago, IL 60620 Phone: (603) 999-1775 Fax: (603) 999-1776	Job	Page 32 of 31
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	Client	Designed by
	Spike	
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	Raycap	mrrine

Section No.	Location	Size	Actual $P_u$	$oF_u$	Ratio $P_u$	Actual $T_u$	$oT_u$	Ratio $T_u$
	$\beta$		$P_u$	$\beta$	$\frac{P_u}{\phi T_u}$	$T_u$	$\beta$	$\frac{T_u}{\phi P_u}$
	19.577 - 18.687		16414.90	476669.00	0.037	0.00	1.59115.67	0.000
	18.687 - 18.842		16338.90	460100.00	0.037	0.00	1218034.99	0.000
	17.4211 - 17.4211		16462.90	449550.00	0.037	0.00	1037091.67	0.000
	16.1379 - 16.1379		16388.00	446490.00	0.037	0.00	1336590.00	0.000
	14.8947 - 14.8947		16409.40	430500.00	0.036	0.00	1220064.44	0.000
	13.6315 - 13.6315		16430.40	415500.00	0.036	0.00	1296104.66	0.000
	12.3684 - 12.3684		16450.00	407250.00	0.036	0.00	1314816.67	0.000
	11.1053 - 11.1053		16472.10	397681.00	0.036	0.00	1346161.07	0.000
	9.8421 - 9.8421		16502.10	384110.00	0.036	0.00	1354566.67	0.000
	8.5795 - 8.5795		16523.00	367541.00	0.035	0.00	1374638.73	0.000
	7.3179 - 7.3179		16547.80	347671.00	0.035	0.00	1394908.44	0.000
	6.0526 - 6.0526		16570.50	324401.00	0.035	0.00	1415300.00	0.000
	4.7897 - 4.7897		16593.10	297931.00	0.035	0.00	1435811.67	0.000
	3.5263 - 3.5263		16615.70	269261.00	0.035	0.00	1456525.00	0.000
	2.2615 - 2.2615		16638.20	237992.00	0.034	0.00	1477366.67	0.000

### Pole Interaction Design Data

Section No.	Location	Ratio $P_u$	Ratio $T_u$	Ratio $M_y$	Ratio $P_u$	Ratio $T_u$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
	$\beta$	$\frac{P_u}{\phi T_u}$	$\frac{T_u}{\phi P_u}$	$\frac{M_y}{\phi P_u}$	$\frac{P_u}{\phi T_u}$	$\frac{T_u}{\phi P_u}$			
1.1	75 - 72.592	0.032	0.017	0.000	0.017	0.000	0.019	1.000	✓
	72.592 - 70.181	0.000	0.034	0.000	0.017	0.000	0.030	1.000	✓
	70.181 - 67.769	0.007	0.051	0.000	0.014	0.000	0.054	1.000	✓
	67.769 - 65.358	0.007	0.067	0.000	0.014	0.000	0.077	1.000	✓
	65.358 - 62.946	0.010	0.103	0.000	0.017	0.000	0.114	1.000	✓
	62.946 - 60.535	0.010	0.140	0.000	0.022	0.000	0.151	1.000	✓
	60.535 - 58.124	0.014	0.176	0.000	0.023	0.000	0.191	1.000	✓
	58.124 - 55.713	0.014	0.210	0.000	0.022	0.000	0.226	1.000	✓
	55.713 - 53.302	0.017	0.257	0.000	0.028	0.000	0.276	1.000	✓

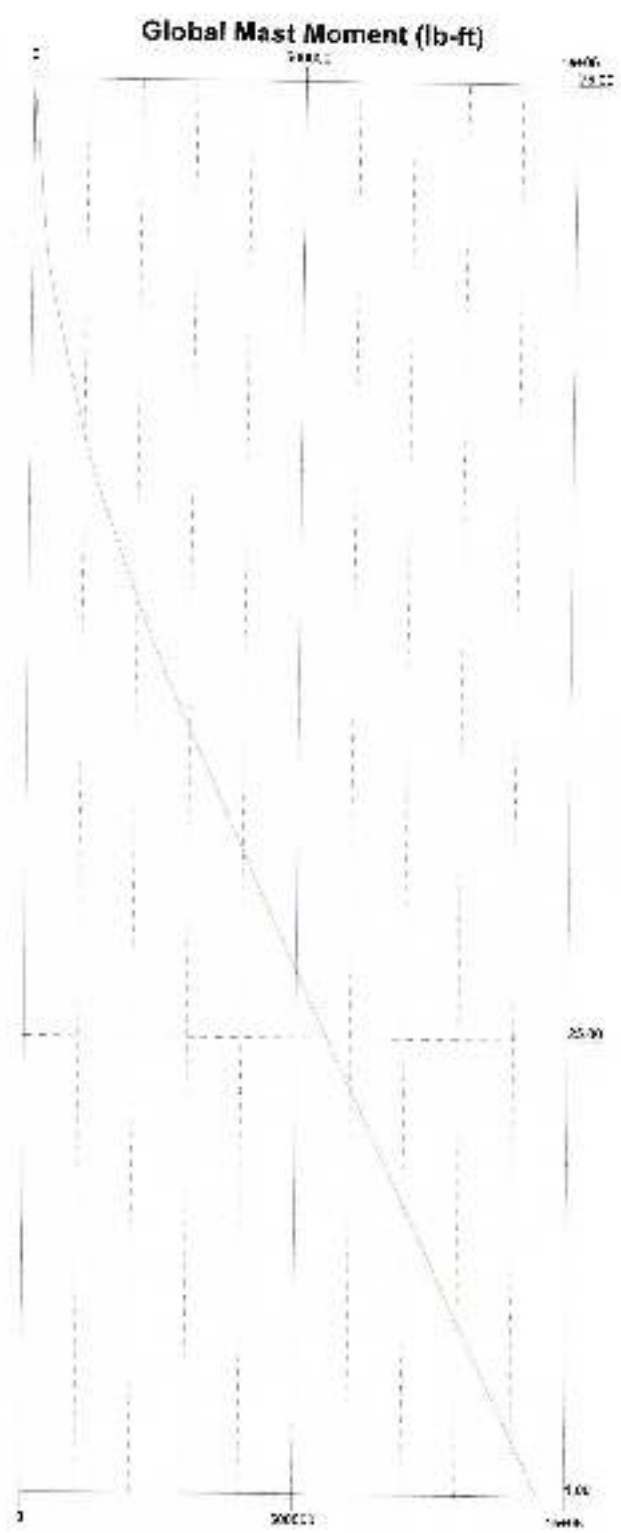
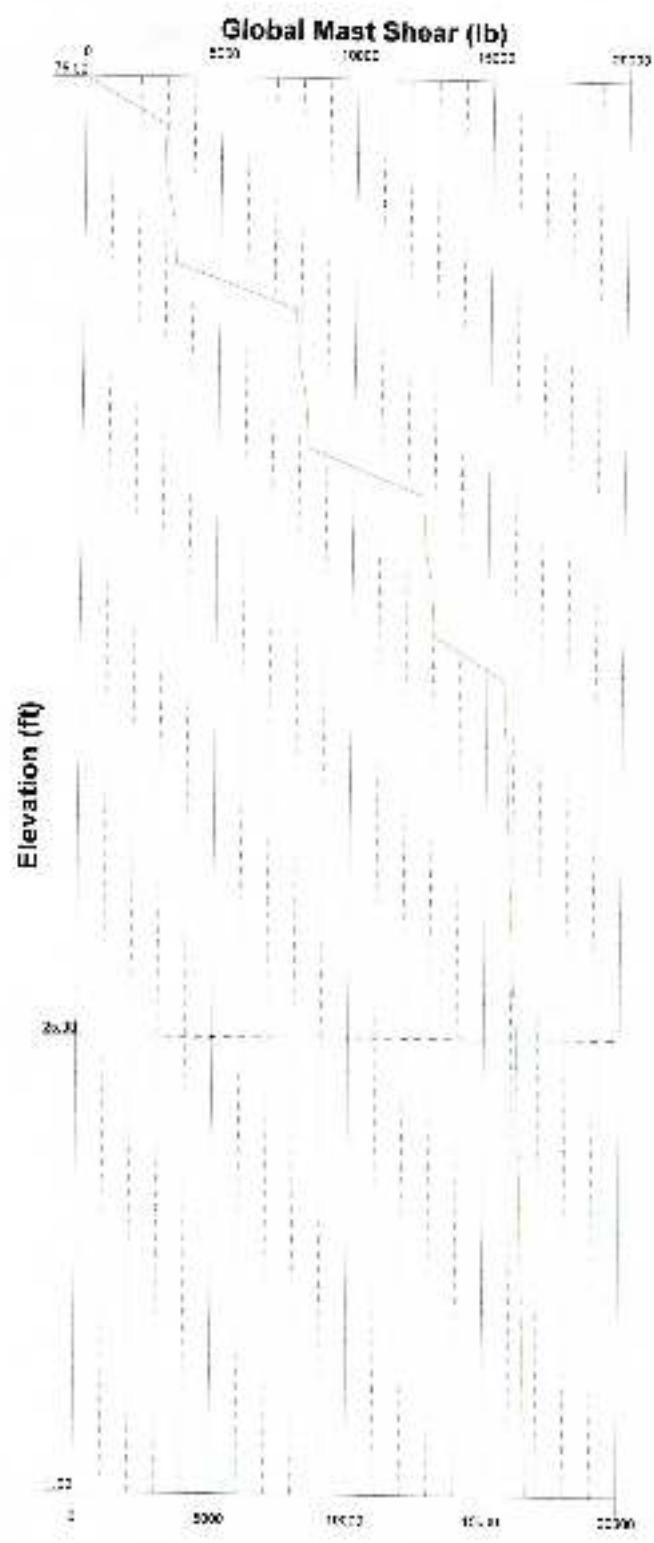
Section No.	Element R	Ratio	Ratio	Ratio	Ratio	Ratio	Comb. Member Ratio	Allow. Member Ratio	Critical
		P <sub>x</sub>	M <sub>x</sub>	M <sub>y</sub>	P <sub>y</sub>	T <sub>x</sub>			
	53-536								
	53-2289	0.00	0.00	0.00	0.04	0.00	0.02	1.00	
	53-211								
	50-92	0.02	0.04	0.00	0.04	0.00	0.07	1.00	
	48-512								
	48-532	0.00	0.05	0.00	0.04	0.00	0.07	1.00	
	46-1053								
	46-1185	0.02	0.04	0.00	0.06	0.00	0.09	1.00	
	42-6974								
	43-5974	0.00	0.09	0.00	0.05	0.00	0.04	1.00	
	41-2915								
	41-2895	0.02	0.04	0.00	0.04	0.00	0.07	1.00	
	38-5516								
	38-8816	0.02	0.04	0.00	0.04	0.00	0.06	1.00	
	26-1717								
	36-4737	0.02	0.05	0.00	0.05	0.00	0.08	1.00	
	34-1658								
	34-6598	0.02	0.04	0.00	0.02	0.00	0.04	1.00	
	31-6579								
	31-6575	0.02	0.02	0.00	0.02	0.00	0.05	1.00	
	30-25								
	29-21-35	0.06	0.04	0.00	0.00	0.00	0.06	1.00	
13	29-21-35	0.00	0.04	0.00	0.02	0.00	0.03	1.00	
	27-22-2368	0.01	0.03	0.00	0.03	0.00	0.07	1.00	
	23-2368	0.01	0.05	0.00	0.05	0.00	0.08	1.00	
	22-4737								
	22-4747	0.06	0.07	0.00	0.04	0.00	0.09	1.00	
	21-2105								
	21-2105	0.01	0.03	0.00	0.03	0.00	0.05	1.00	
	19-9474								
	18-5842	0.01	0.09	0.00	0.03	0.00	0.01	1.00	
	18-6312	0.01	0.07	0.00	0.03	0.00	0.05	1.00	
	17-4711								
	17-4211	0.01	0.00	0.00	0.07	0.00	0.03	1.00	
	15-1579								
	16-1579	0.01	0.03	0.00	0.03	0.00	0.07	1.00	
	14-8947								
	13-5816	0.01	0.04	0.00	0.03	0.00	0.07	1.00	
	13-6216	0.01	0.09	0.00	0.03	0.00	0.07	1.00	
	12-3687								
	12-3584	0.01	0.09	0.00	0.06	0.00	0.06	1.00	
	11-1051								
	11-1051	0.01	0.05	0.00	0.03	0.00	0.08	1.00	
	9-8421								
	9-8431	0.01	0.07	0.00	0.03	0.00	0.04	1.00	
	8-5793								
	8-37895	0.01	0.06	0.00	0.03	0.00	0.03	1.00	

<b>inxTower</b> <b>Vector Structural Engineering</b> 621 W. Galena Park Blvd Denver, CO 80220 Phone: (303) 990-1773 FAX: (303) 990-1776	Job	Spike	Page 34 of 131
	Project	U0142.2054.242	Date 17:04:43 10/24/24
	Client	Raycap	Designed by mrmie

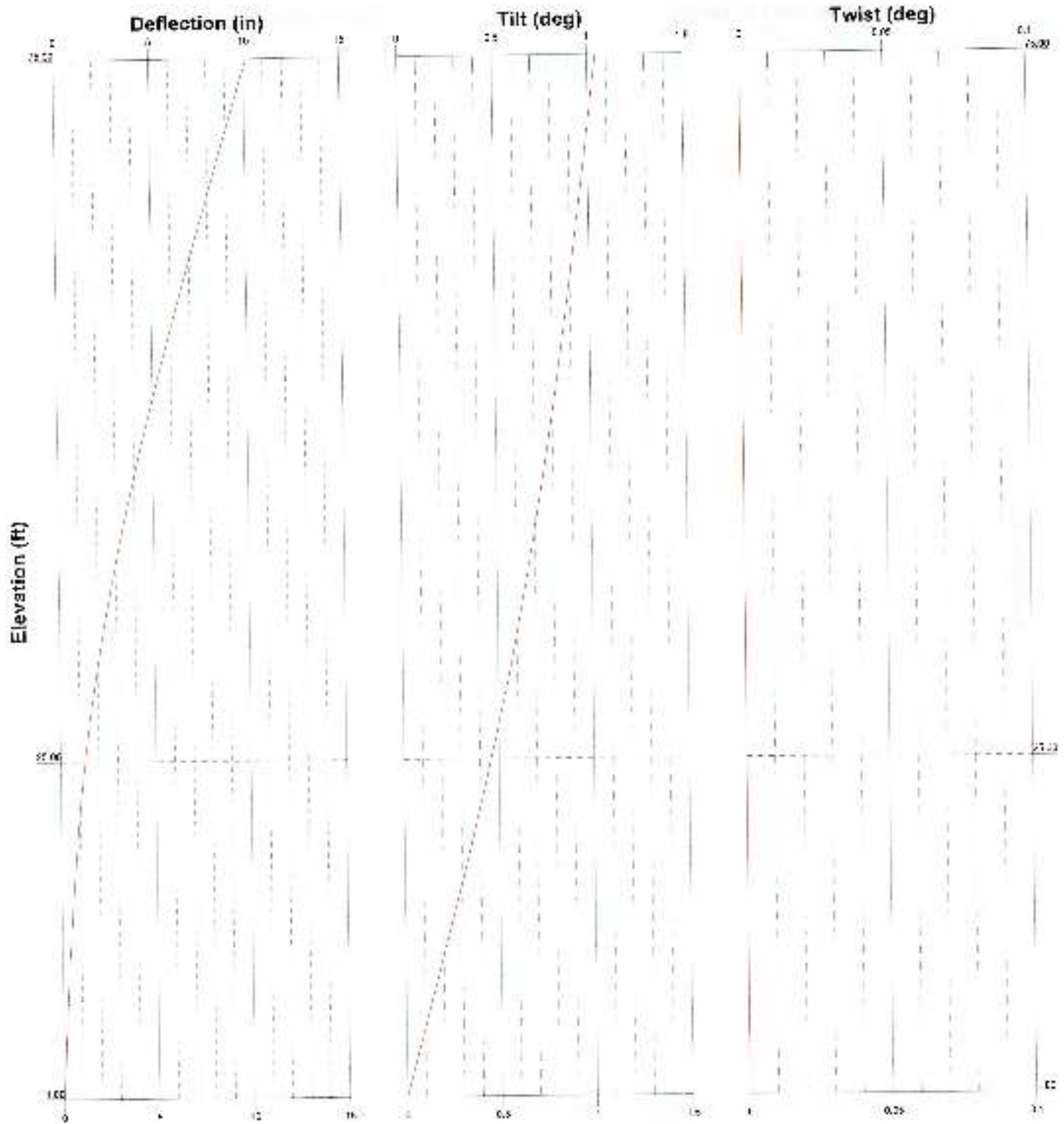
Section No.	Elevation <i>P</i>	Ratio <i>P<sub>u</sub></i>	Ratio <i>M<sub>u</sub></i>	Ratio <i>M<sub>c</sub></i>	Ratio <i>V<sub>u</sub></i>	Ratio <i>V<sub>c</sub></i>	Contn. Stress Ratio	Allow. Stress Ratio	Criteria
	<i>P</i>	<i>P<sub>u</sub></i>	<i>M<sub>u</sub></i>	<i>M<sub>c</sub></i>	<i>V<sub>u</sub></i>	<i>V<sub>c</sub></i>			
	7.31575						0.711	1.000	✓
	7.31575 - 8.03253	0.016	0.695	0.000	0.035	0.000	0.720	1.000	✓
	8.03253 - 8.78917	0.018	0.709	0.000	0.035	0.000	0.724	1.000	✓
	8.78917 - 9.52509	0.016	0.711	0.000	0.035	0.000	0.735	1.000	✓
	9.52509 - 1.36915	0.018	0.719	0.000	0.035	0.000	0.741	1.000	✓
	1.36915 - 2.26315 - 1	0.018	0.727	0.000	0.034	0.000			✓

### Section Capacity Table

Section No.	Elevation <i>P</i>	Component Type	Size	Critical Element	<i>P</i> k	<i>M<sub>u</sub></i> k	95 Capacity	Pass/Fail	
11	75 - 75	Pole	TP30 75x2100.1875	1	-21330.40	1.0517000	74.5	Pass	
12	75 - 75	Pole	TP15 385x290.5463x0.75	2	-25341.10	15.567000	74.4	Pass	
Summary									
Pole (1...)								74.5	Pass
RATING =								74.5	Pass



<b>Vector Structural Engineering</b> 657 W Galena Park Blvd Draper, UT 84020 Phone: (801) 940-1775 FAX: (801) 968-776		<b>Spiko</b> No. 001022054.242 Dr. P. Taylor Date: 10/24/24 Title:	10/24/24 10/24/24 10/24/24
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<b>Vector Structural Engineering</b> 551 W Galena Park Blvd Draper, UT 84020 Phone: (801) 950-1775 FAX: (801) 950-1776	SEE Spike
	DRAWN: UB142 2004.249
	CHECKED: RAY/AD
	DATE: TIA-222-H
	DATE: 3/24/04
SCALE: NTS	
SHEET NO: E 5	



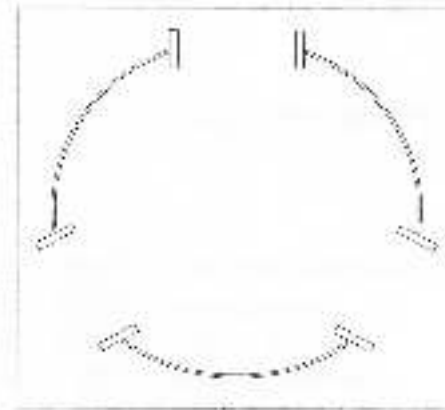
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PROJECT: NM01-148 SPIKE

## Port Design:

Label: Ports at 70 ft A.G.L.



### Geometry Input

Elevation of Port, AGL	70.00	ft
Pole Diameter	21.975	in
Pole Thickness	0.1875	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	11.0	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	3/8	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	3	

	Port 1	Port 2	Port 3
Azimuth (°)	0	120	240
Height (in)	12	12	12
Width (in)	8	8	8
Depth (in)	2.5	2.5	2.5
Thickness (in)	0.5	0.5	0.5
Projection (in)	0.5	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	2.5	2.5	2.5
Pole Area Removed (in <sup>2</sup> )	1.54	1.54	1.54
Dist. From Center to Reinf. (in)	10.7375	10.2375	10.2375
Area Check	79.9%	79.9%	79.9%
MOI Check	85.0%	85.0%	85.0%
Individual Port Weights (lbs)	14	14	14
Reduction in Pole Weigh. (lbs)	16		
Total Port Weight (lbs)	27		



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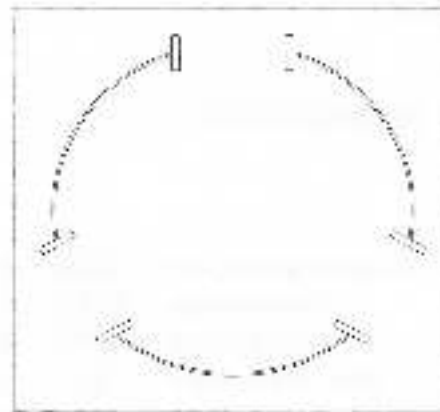
PROJECT: NM01-148 SPIKE

## Port Design:

Label: Ports at 60 ft A.G.L.

### Geometry Input

Elevation of Port, AGL	60.00	ft
Pole Diameter	23.925	in
Pole Thickness	0.1875	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	11.0	k/in
Weld Filler Strength	70	ksi
Required Fillet Weld	3/8	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	3	



	Port 1	Port 2	Port 3
Azimuth (°)	0	120	240
Height (in)	12	12	12
Width (in)	8	8	8
Depth (in)	2.5	2.5	2.5
Thickness (in)	0.5	0.5	0.5
Projection (in)	0.5	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	2.5	2.5	2.5
Pole Area Removed (in <sup>2</sup> )	1.53	1.53	1.53
Dist. From Center to Reinf. (in)	11.2125	11.2125	11.2125
Area Check	79.6%	79.6%	79.6%
MOI Check	84.2%	84.2%	84.2%
Individual Port Weights (lbs)	14	14	14
Reduction in Pole Weight (lbs)	16		
Total Port Weight (lbs)	27		



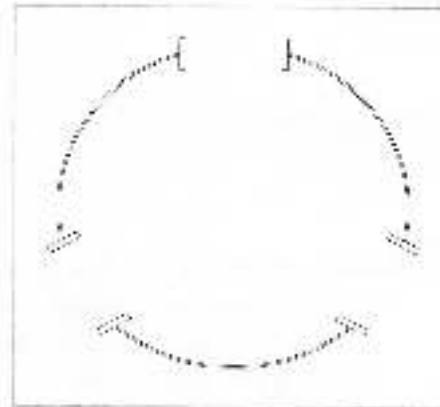
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PROJECT: NM01-148 SPIKE

### Port Design:

Label: Ports at 50 ft A.G.L.



#### Geometry Input

Elevation of Port, AGL	50.00	ft
Pole Diameter	25.875	in
Pole Thickness	0.1875	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	11.0	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	3/8	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	3	

	Port 1	Port 2	Port 3
Azimuth (°)	0	120	240
Height (in)	12	12	12
Width (in)	8	8	8
Depth (in)	2.5	2.5	2.5
Thickness (in)	0.5	0.5	0.5
Projection (in)	0.5	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	2.5	2.5	2.5
Pole Area Removed (in <sup>2</sup> )	1.53	1.53	1.53
Dist. From Center to Reinf. (in)	12.1875	12.1875	12.1875
Area Check	79.3%	79.3%	79.3%
MDI Check	83.6%	83.6%	83.6%
Individual Port Weights (lbs)	14	14	14
Reduction in Pole Weight (lbs)	16		
Total Port Weight (lbs)	27		



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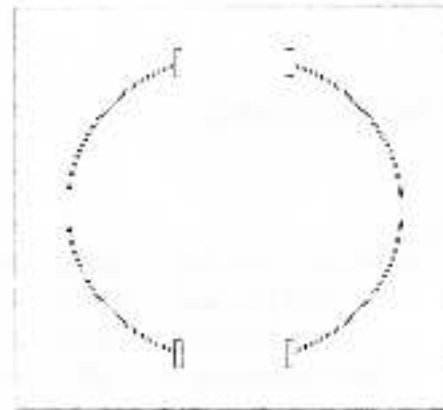
PROJECT: NM01-14R SPIKE

## Port Design:

Label: Ports at 7 ft A.G.L.

### Geometry Input

Elevation of Port, AGL	7.00	ft
Pole Diameter	33.885	in
Pole Thickness	0.25	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	14.6	k/in
Weld Filler Strength	70	ksi
Required Fillet Weld	1/2	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	2	



	Port 1	Port 2
Azimuth (°)	0	180
Height (in)	24	24
Width (in)	12	12
Depth (in)	3	3
Thickness (in)	0.75	0.75
Projection (in)	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	4.5	4.5
Pole Area Removed (in <sup>2</sup> )	3.07	3.07
Dist. From Center to Reinf. (in)	15.9425	15.9425
Area Check	88.6%	88.6%
MOI Check	93.5%	93.5%
Individual Port Weights (lbs)	46	46
Reduction in Pole Weight (lbs)	42	
Total Port Weight (lbs)	50	



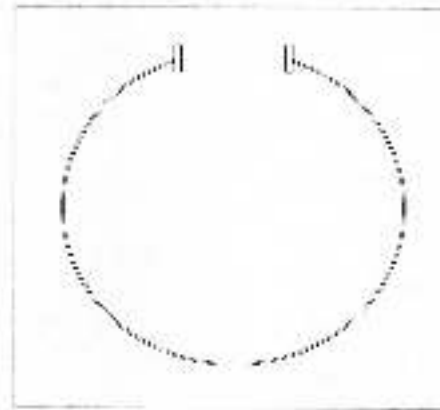
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PROJECT: NM01-148 SPIKE

## Port Design:

Label: Ports at 3 ft A.G.L.



### Geometry Input

Elevation of Port, AGI	3.00	ft
Pole Diameter	34.665	in
Pole Thickness	0.25	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	14.6	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	1/2	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	1	

	Part 1
Azimuth (°)	0
Height (in)	24
Width (in)	12
Depth (in)	3
Thickness (in)	0.75
Projection (in)	0.5
Reinforcing Area (in <sup>2</sup> )	4.5
Pole Area Removed (in <sup>2</sup> )	3.06
Dist. From Center to Reinf. (in)	16.3325
Area Check	88.5%
MOI Check	93.3%
Individual Port Weights (lbs)	46
Reduction in Pole Weight (lbs)	23
Total Port Weight (lbs)	23



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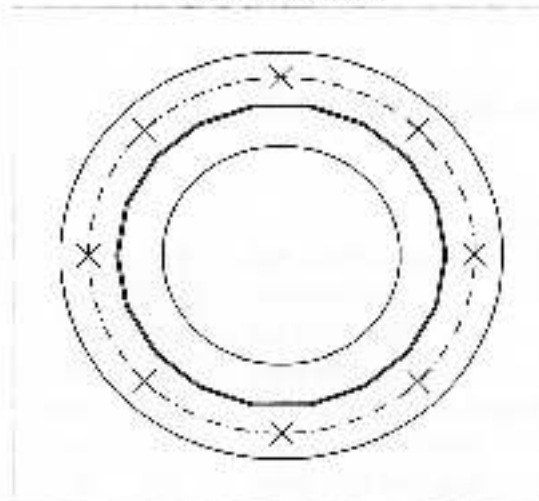
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PROJECT: NMU-1'8 SPIK

### Monopole Baseplate & Anchorage Design per TIA-222-H Annex D & TIA-222-H Section 4.9.9

Quantity	Symbol	Value	Units
Number of sides		18	
Hot U.D.	$D$	35.06	in
Pole wall thickness	$t$	0.25	in
Pole yield strength	$F_y$	65	ksi
Weld factor		7	in
base plate fillet weld size		0.35	in
Anchor diameter	$d$	2.25	in
Number of anchors	$n$	8	
Anchor grade		A518-75	
Base plate thickness	$t_p$	2.25	in
Base plate yield strength	$F_y$	50	ksi
Anchor hole diameter		2.625	in
Slotted to outside edge?		No	
Hot washer diameter		4	
Zinc drain hole diameter		2.625	
Zinc drain circle		30.5	in
Bolt circle diameter	$D_{bc}$	41.5	in
Para O.D.	$D_{po}$	47.8	in
Plate O.D.		25.5	in

Base Plate Illustration

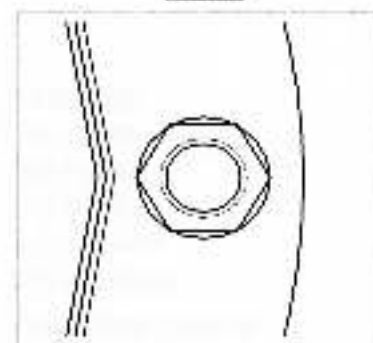


LRFD Loads	Symbol	Wind		Seismic	
		Value	Units	Value	Units
Axial down	$R_{ax}$	25.37	k	0.00	k
Axial up	$R_{ax}$	0	k	0.00	k
Shear	$V_u$	15.62	k	0.00	k
Moment	$M_u$	950.14	k-ft	0.00	k-ft
Member mom. capacity	$\phi M_p$	132	k-ft		

Checks	Wind		Seismic	
	Value	Limit	Value	Limit
Plate stress ratio	46.8%	OK		
Anchor unity check	55.0%	OK		
Min. number of sides	18	OK	6 minimum	
Min. number of anchors	8	OK	8 minimum	
Max. anchor rod to pole distance	3.1'	OK	13.5' maximum	
Min. anchor diameter	2.25"	OK	0.75' minimum	
Max. anchor rod spacing	26.3'	NG	13.5' maximum	
Min. anchor rod spacing	15.88'	OK	6.75' minimum	
Min. base plate thickness	1.95"	OK	2" minimum	
Min. inside diameter	25.5"	OK	10.52' minimum	
Max. inside diameter	25.5"	OK	21.125' maximum	

Note: when number of anchors is less than minimum and when maximum anchor rod spacing is exceeded, adjustments are made to the affected plate which calculations as if requirements of TIA-222-H Annex G were met.

Fit Check



Check	Dist.	Result
Washer vs weld	0.0339	OK
Washer vs DD	0.8125	OK
Washer covers hole	0.5	OK



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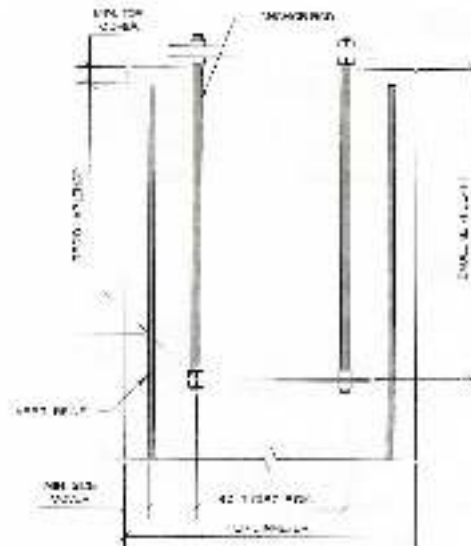
PROJECT: NM21-149 SHIKH

## Anchorage Embedment Design

(per ACI 318-19)

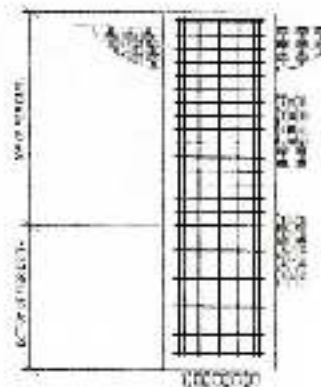
Vertical Bar Size	#6
N of Vertical Bars	22
Concrete Compressive Strength (psi)	4300
Pier Diameter (ft)	5.5
Pier Depth (ft)	20
Top of Pier Elevation (ft)	5
Concrete Volume (yd <sup>3</sup> )	13.0
Side Concrete Cover (in)	4
Top Concrete Cover (in)	2
Horizontal Tie Size	#4
Bolt Circle Diameter (in)	41.5
N of Anchor Rods	8
Anchor Rod Diameter (in)	2.25

$\psi_b$ (bar location factor)	1.0	Table 25.4.2.4
$\psi_s$ (sloppy coating factor)	1.0	Table 25.4.2.4
$\psi_g$ (bar size factor)	1.0	Table 25.4.2.4
$\lambda$ (concrete type factor)	1.0	Table 25.4.2.4
Vertical Bar Diameter (in)	1.0	
Horizontal Tie Diameter (in)	0.500	
$H_u$ (ft)	4.25	
Req'd Lap Length (in)	37.3	in (Section 25.4.2.2)
Min. Req'd Embedment Depth (in)	48.2	



## Transverse Reinforcement Design

Seismic Design Category	G
Apply Seismic Detailing?	No
Site Class	C
Type of Transverse Reinforcement	Spiral
Transverse $f_y$ (ksi)	50
Seismic Hooks Required?	No
Tie Size OK?	Yes
Spacing at Top of Pier (in)	12
Spacing at Bottom of Pier (in)	12
Total Pier Length (ft)	20.5
Top Pier Length (ft)	20.5
Bottom Pier Length (ft)	0





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Project: NM01-148 SPIKE

**Drilled Pier Design:****Applied Loads:**

Max. shear, V	22.2	k
Max. moment, M	1,266.9	k-ft
Max. down, P <sub>down</sub>	35.0	k
Max. uplift, P <sub>uplift</sub>	0.0	k

Design methodology:	LRFD
Maximum foundation rating:	100%

**Pier Properties:**

Pier shape	Round
Pier diameter, b:	5.5 ft
Min. pier diameter, b <sub>min</sub> (opt):	0.0 ft
b:	5.5
Top of pier elevation:	0.5 ft
Pier depth, d:	20 ft
Min. pier depth, d <sub>min</sub> (opt):	0.0 ft

Volume of concrete	487	ft <sup>3</sup>
Volume of concrete	18.0	yd <sup>3</sup>
Weight of concrete	73.1	k

**Soil Properties & Analysis:**

Allow. bearing pressure:	65,800	psf
Cross or net?	Net	
1/3 increase for short term loads?	No	
Skin friction (down):	0	psf
Skin friction (uplift):	0	psf
Top length to ignore:	2.75	ft
1/3 increase for short term loads?	No	
Combine skin friction w/ end bearing?	No	
Bearing capacity:	1,553.5	k
Uplift capacity:	65.8	k

F.S.: 1

F.S.: 1

F.S.: 1

**Results:**

Bearing capacity OK.  
 Uplift capacity OK.

Lateral analysis in LPIE



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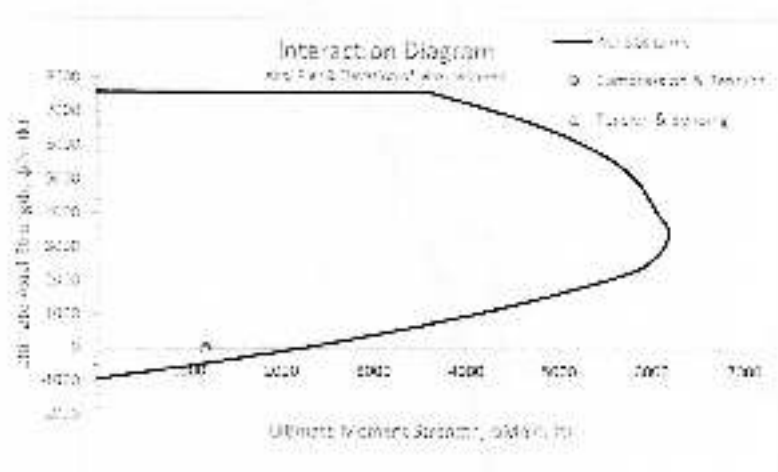
PROJECT: MM01 149 Soka

**Drilled Pier Reinforcement:****Design Requirements:**

Max. Moment, $M$ (k-ft)	800.1	Max. Down, $P_{max}$ (k)	23.0	Required Foundation UC (min)	100%
Max. Shear, $V$ (k)	16.6	Max. Uplift, $P_u$ (k)	0.0	Min. $M-V^2/P_{max}E$ (k-ft)	1100.1
Height of $V$ (ft)	15.855	Eccentricity for $P$ (in)	0	(Uplift is negative for compression w/ Interaction Diagram)	
		Concrete Self-weight (k)	47.7	(0.145 pcf)	

**Pier Properties:**

Code Reference	ACI 318-19
Pier Diameter (ft)	3.0
Top of Pier Elevation (ft)	0
Pier Depth (ft)	20
Vertical Bar Size	#8
Bar Diameter (in)	1.0
Bar Area (in <sup>2</sup> )	0.79
Reinforcement Design Category	C
# of Vertical Bars	22
Vert. Yield Strength (ksi)	60000
Horizontal Reinf. Type	Spiral
Horizontal Reinf. Size	#4
Horizontal Reinf. Diameter (in)	0.5
Side Concrete Cover (in)	4
Vert. Ledge Distance (in)	4.5
Conc. Comp. Strength, $f_c$ (ksi)	4000
Angle Between Bars, $\theta$ (radians)	0.785
Area of Steel (in <sup>2</sup> )	17.4
Gross Column Area (in <sup>2</sup> )	2421.2
Min. Reinforcement Ratio	0.51%
$\rho_f$	0.85
Concrete Yield Strain, $\epsilon_{sy}$ (in/in)	0.003
$P_u$ (k)	12515
$\alpha$	0.75
$\beta_1$ Factor	0.80
$\phi$ (pure compression, $\phi_c$ )	0.75
$E_s$ (ksi)	29000
Steel Yield Strain, $\epsilon_{sy}$ (in/in)	0.002055
Number of verticals in top row	1

**Axial & Bending Checks:**

Steel/Concrete Ratio: 0.51% &gt; Min. Reinf. Ratio

**Compression & Bending**

@ 1/4 Pier @ Max. M

$\phi P_u$ (k)	19.7	32.9
$\phi M_u$ (k-ft)	2222.9	2910.2
UC	53.1%	51.1%

OK, Adequate

$$:P_u^2 - \phi_c P_u^2 + \phi_c^2 P_u^2 + \phi_c^2 M_u^2$$

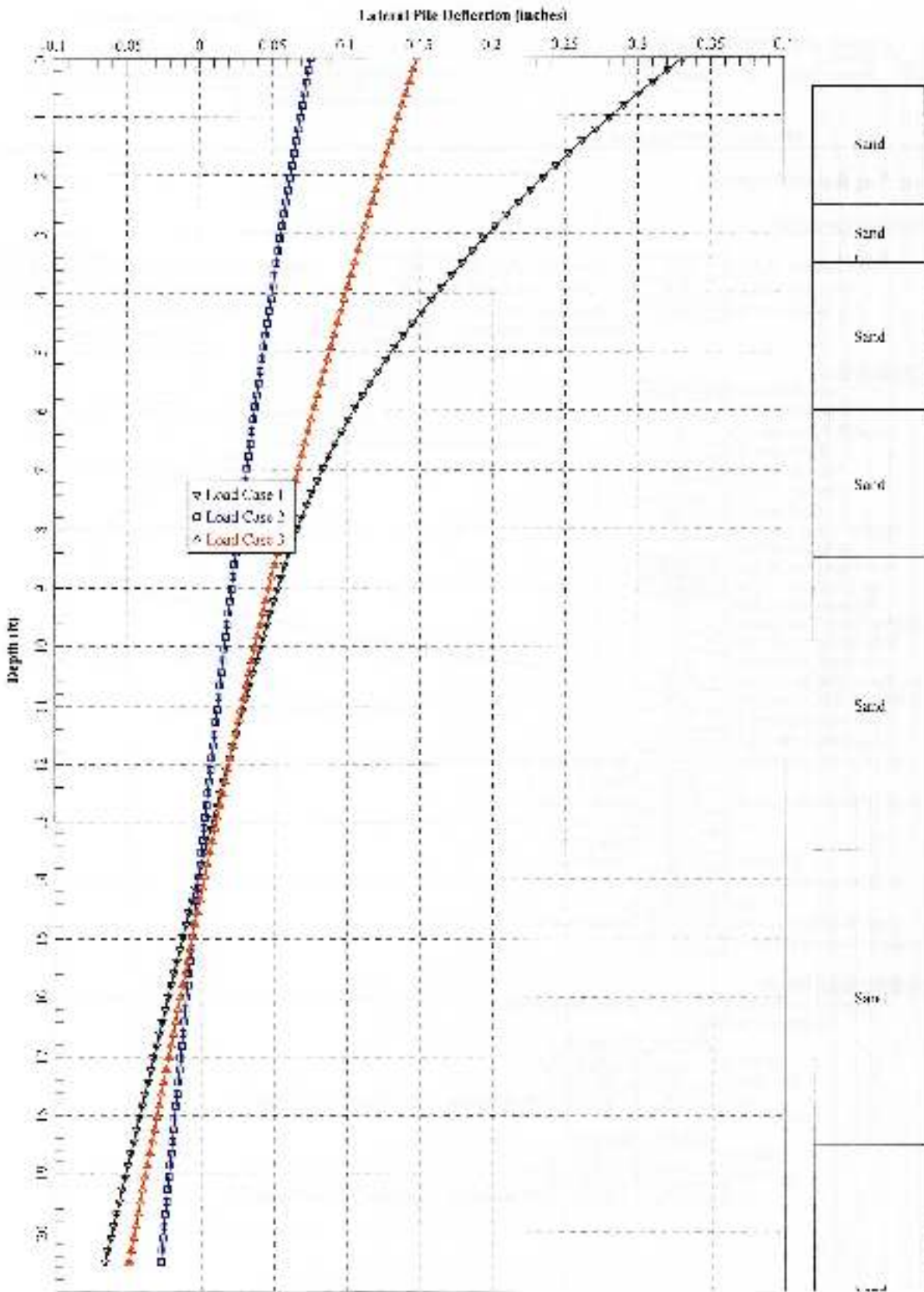
**Tension & Bending**

@ 3/4 Pier @ Max. M

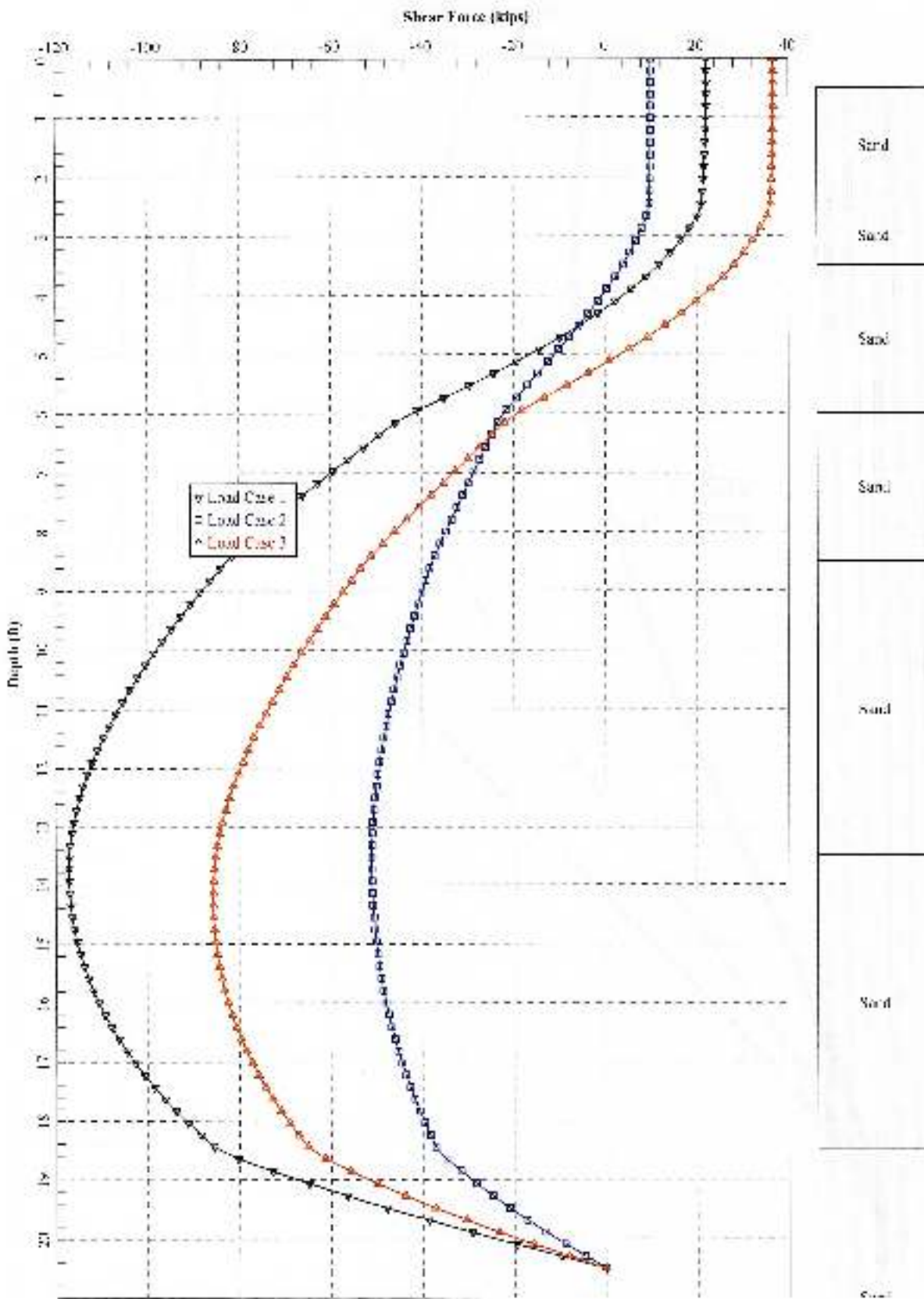
$\phi P_u$ (k)	0.0	42.9
$\phi M_u$ (k-ft)	2152.5	2270.1
UC	51.1%	52.0%

OK, Adequate

$$:P_u^2 - \phi_c P_u^2 + \phi_c^2 P_u^2 + \phi_c^2 M_u^2$$







LDIA for Miram, Volume 001-11.001

Analysis of Loads, Moments, and Deformed Shapes  
 Subjected to Lateral Loading Using the p-y Method  
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Number of Files to be Analyzed:

100  
 100

Number of Security Levels: 1000000

This type of LDIA is known as a "batch" analysis.

Water Structural Engineering, Inc.

Use of this program by any other than "Water Structural Engineering, Inc." is a violation of the software license agreement.

Files Used for Analysis

LDIA File Locations:  
 Case: C:\Program Files\Earth\Project\Case\001-11.001\Volume 001-11.001-001  
 Substructure: 001-11.001-001\Substructure\Substructure\11001

Batch Input Data File:  
 11001-001-001

Batch Output Report File:  
 11001-001-001

Batch Plot Output File:  
 11001-001-001

Batch Output Message File:  
 11001-001-001

Time and Date of Analysis

Date: October 04, 1979

Time: 11:21:37

File Name

11001-001-001-001-001

11001-001-001-001-001

11001-001-001

11001-001-001

11001-001-001

Program Options and Settings

General Options:  
 - Use Substructure Analysis Computations (Consistent) [Yes/No]  
 - Use Water, Inc.'s Batch for Data Input and Computation  
 - Use Substructure Analysis [Yes/No/Force/Post/Update]

Analysis Method Settings:  
 - Method Number of Iterations [1000]  
 - Iteration Tolerance for Convergence [1.000E-05]  
 - Plot as a Single Deflection [100.0000]  
 - Substructure Elements [100]

Utility Applied to Water of Order of Loading:  
 - None [None/Identified]

- Use of pile weight distribution factor (if any) as not selected
- Analyze load-carrying capacities (Method of Seegradle)
- Soil distribution lateral and vertical
- Loading by lateral and vertical acting on pile not selected
- Time of wave reflection at the pile tip not selected
- Time of wave reflection at the pile tip not selected
- Time of wave reflection at the pile tip not selected
- Time of wave reflection at the pile tip not selected
- Time of wave reflection at the pile tip not selected
- Time of wave reflection at the pile tip not selected

**Design Values**

- Allow pile cap to be selected to design design system.
- Allow pile cap to be selected, bearing capacity, shear force, etc.
- Allow pile cap to be selected for full length of pile.
- Allow pile cap to be selected for full length of pile.
- Allow pile cap to be selected for full length of pile.
- Allow pile cap to be selected for full length of pile.
- Allow pile cap to be selected for full length of pile.
- Allow pile cap to be selected for full length of pile.

**Pile Structural Properties (see Section)**

Number of pile sections selected	=	2
Total length of pile	=	22,500 ft
Depth of ground surface below water table	=	6,500 ft

Pile dimensions and properties are defined using a section. The values are computed using the following values interpolated with care over the length of the pile. A summary of the pile dimensions is as follows:

Code No.	Depth Value Pile feet	Pile Properties
1	0.000	25.22002 ft
2	22.500	25.22002 ft

**Load Structural Properties for Pile Section**

**Pile Section No. 1**

Section No. (see Section No. 1)	25.22002 ft
Length of section	25.22002 ft
Depth of section	25.22002 ft

Shear capacity of section = 2,902 lbs

**Soil Values and Pile Section Angles**

Grain Size (mm)	0.00 degrees
	0.00 radians
Pile Section Angle	0.00 degrees
	0.00 radians

**Soil and Pile Section Properties**

The soil is defined by the following properties:

**Layer 1: (see Section No. 1) (see Section No. 1)**

Number of pile sections selected	0.20000 ft
Total length of pile	2.00000 ft
Depth of ground surface below water table	0.20000 ft
Number of pile sections selected	0.20000 ft
Total length of pile	2.00000 ft
Depth of ground surface below water table	0.20000 ft
Number of pile sections selected	0.20000 ft
Total length of pile	2.00000 ft
Depth of ground surface below water table	0.20000 ft

The soil values for the design are defined for this layer.

**Layer 2: (see Section No. 2) (see Section No. 2)**

Number of pile sections selected	0.22002 ft
Total length of pile	2.20002 ft
Depth of ground surface below water table	0.22002 ft
Number of pile sections selected	0.22002 ft
Total length of pile	2.20002 ft
Depth of ground surface below water table	0.22002 ft
Number of pile sections selected	0.22002 ft
Total length of pile	2.20002 ft
Depth of ground surface below water table	0.22002 ft

The soil values for the design are defined for this layer.

**Layer 3: (see Section No. 3) (see Section No. 3)**



NOTE: The unit values for sagrada k will be computed for this layer.

Layer 10 is sand, dry unit weight by base of pile, 1074

Distance from top of pile to top of layer = 0.00000 ft  
 Distance from top of pile to bottom of layer = 7.00000 ft  
 Effective unit weight at top of layer = 110.00000 pcf  
 Effective unit weight at bottom of layer = 110.00000 pcf  
 Refraction angle at top of layer = 25.00000 deg.  
 Refraction angle at bottom of layer = 25.00000 deg.  
 Sagrada k at top of layer = 0.0000 pcf  
 Sagrada k at bottom of layer = 0.0000 pcf

NOTE: Default values for sagrada k will be computed for this layer.

Layer 11 is sand, dry unit weight by base of pile, 1074

Distance from top of pile to top of layer = 0.00000 ft  
 Distance from top of pile to bottom of layer = 0.00000 ft  
 Effective unit weight at top of layer = 110.00000 pcf  
 Effective unit weight at bottom of layer = 110.00000 pcf  
 Refraction angle at top of layer = 25.00000 deg.  
 Refraction angle at bottom of layer = 25.00000 deg.  
 Sagrada k at top of layer = 0.0000 pcf  
 Sagrada k at bottom of layer = 0.0000 pcf

NOTE: Default values for sagrada k will be computed for this layer.

Layer 12 is sand, dry unit weight by base of pile, 1074

Distance from top of pile to top of layer = 0.00000 ft  
 Distance from top of pile to bottom of layer = 0.00000 ft  
 Effective unit weight at top of layer = 110.00000 pcf  
 Effective unit weight at bottom of layer = 110.00000 pcf  
 Refraction angle at top of layer = 25.00000 deg.  
 Refraction angle at bottom of layer = 25.00000 deg.  
 Sagrada k at top of layer = 0.0000 pcf  
 Sagrada k at bottom of layer = 0.0000 pcf

NOTE: Default values for sagrada k will be computed for this layer.

Depth of the lower soil layer is used to define the pile point

#### Summary of Input Soil Properties

Layer	Soil Type	Layer	Thickness (ft)	Depth (ft)
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Layer No.	Soil Type	Depth (ft)	Unit Weight (pcf)	Refraction Ang (deg)	Sp. Mod.
1	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
2	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
3	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
4	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
5	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
6	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
7	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
8	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
9	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
10	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
11	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default
12	Sand	0.0000	110.0000	25.0000	default
	(Sand, dry unit w)	0.0000	110.0000	25.0000	default

#### Soil Loading Type

Static loading is used for all analyses.

#### Mid-way loading on pile is used by the driver

Number of load specifier = 7

Load No.	Load Type	Location	Soil Depth
1	Point	0	0.0000





3.000000	1000000	1000000000	10	1000000	1.000000	1.000000
3.000001	1000001	1000001000	10	1000001	1.000001	1.000001
3.000002	1000002	1000002000	10	1000002	1.000002	1.000002
3.000003	1000003	1000003000	10	1000003	1.000003	1.000003
3.000004	1000004	1000004000	10	1000004	1.000004	1.000004
3.000005	1000005	1000005000	10	1000005	1.000005	1.000005
3.000006	1000006	1000006000	10	1000006	1.000006	1.000006
3.000007	1000007	1000007000	10	1000007	1.000007	1.000007
3.000008	1000008	1000008000	10	1000008	1.000008	1.000008
3.000009	1000009	1000009000	10	1000009	1.000009	1.000009
3.000010	1000010	1000010000	10	1000010	1.000010	1.000010
3.000011	1000011	1000011000	10	1000011	1.000011	1.000011
3.000012	1000012	1000012000	10	1000012	1.000012	1.000012
3.000013	1000013	1000013000	10	1000013	1.000013	1.000013
3.000014	1000014	1000014000	10	1000014	1.000014	1.000014
3.000015	1000015	1000015000	10	1000015	1.000015	1.000015
3.000016	1000016	1000016000	10	1000016	1.000016	1.000016
3.000017	1000017	1000017000	10	1000017	1.000017	1.000017
3.000018	1000018	1000018000	10	1000018	1.000018	1.000018
3.000019	1000019	1000019000	10	1000019	1.000019	1.000019
3.000020	1000020	1000020000	10	1000020	1.000020	1.000020
3.000021	1000021	1000021000	10	1000021	1.000021	1.000021
3.000022	1000022	1000022000	10	1000022	1.000022	1.000022
3.000023	1000023	1000023000	10	1000023	1.000023	1.000023
3.000024	1000024	1000024000	10	1000024	1.000024	1.000024
3.000025	1000025	1000025000	10	1000025	1.000025	1.000025
3.000026	1000026	1000026000	10	1000026	1.000026	1.000026
3.000027	1000027	1000027000	10	1000027	1.000027	1.000027
3.000028	1000028	1000028000	10	1000028	1.000028	1.000028
3.000029	1000029	1000029000	10	1000029	1.000029	1.000029
3.000030	1000030	1000030000	10	1000030	1.000030	1.000030
3.000031	1000031	1000031000	10	1000031	1.000031	1.000031
3.000032	1000032	1000032000	10	1000032	1.000032	1.000032
3.000033	1000033	1000033000	10	1000033	1.000033	1.000033
3.000034	1000034	1000034000	10	1000034	1.000034	1.000034
3.000035	1000035	1000035000	10	1000035	1.000035	1.000035
3.000036	1000036	1000036000	10	1000036	1.000036	1.000036
3.000037	1000037	1000037000	10	1000037	1.000037	1.000037
3.000038	1000038	1000038000	10	1000038	1.000038	1.000038
3.000039	1000039	1000039000	10	1000039	1.000039	1.000039
3.000040	1000040	1000040000	10	1000040	1.000040	1.000040
3.000041	1000041	1000041000	10	1000041	1.000041	1.000041
3.000042	1000042	1000042000	10	1000042	1.000042	1.000042
3.000043	1000043	1000043000	10	1000043	1.000043	1.000043
3.000044	1000044	1000044000	10	1000044	1.000044	1.000044
3.000045	1000045	1000045000	10	1000045	1.000045	1.000045
3.000046	1000046	1000046000	10	1000046	1.000046	1.000046
3.000047	1000047	1000047000	10	1000047	1.000047	1.000047
3.000048	1000048	1000048000	10	1000048	1.000048	1.000048
3.000049	1000049	1000049000	10	1000049	1.000049	1.000049
3.000050	1000050	1000050000	10	1000050	1.000050	1.000050
3.000051	1000051	1000051000	10	1000051	1.000051	1.000051
3.000052	1000052	1000052000	10	1000052	1.000052	1.000052
3.000053	1000053	1000053000	10	1000053	1.000053	1.000053
3.000054	1000054	1000054000	10	1000054	1.000054	1.000054
3.000055	1000055	1000055000	10	1000055	1.000055	1.000055
3.000056	1000056	1000056000	10	1000056	1.000056	1.000056
3.000057	1000057	1000057000	10	1000057	1.000057	1.000057
3.000058	1000058	1000058000	10	1000058	1.000058	1.000058
3.000059	1000059	1000059000	10	1000059	1.000059	1.000059
3.000060	1000060	1000060000	10	1000060	1.000060	1.000060
3.000061	1000061	1000061000	10	1000061	1.000061	1.000061
3.000062	1000062	1000062000	10	1000062	1.000062	1.000062
3.000063	1000063	1000063000	10	1000063	1.000063	1.000063
3.000064	1000064	1000064000	10	1000064	1.000064	1.000064
3.000065	1000065	1000065000	10	1000065	1.000065	1.000065
3.000066	1000066	1000066000	10	1000066	1.000066	1.000066
3.000067	1000067	1000067000	10	1000067	1.000067	1.000067
3.000068	1000068	1000068000	10	1000068	1.000068	1.000068
3.000069	1000069	1000069000	10	1000069	1.000069	1.000069
3.000070	1000070	1000070000	10	1000070	1.000070	1.000070
3.000071	1000071	1000071000	10	1000071	1.000071	1.000071
3.000072	1000072	1000072000	10	1000072	1.000072	1.000072
3.000073	1000073	1000073000	10	1000073	1.000073	1.000073
3.000074	1000074	1000074000	10	1000074	1.000074	1.000074
3.000075	1000075	1000075000	10	1000075	1.000075	1.000075
3.000076	1000076	1000076000	10	1000076	1.000076	1.000076
3.000077	1000077	1000077000	10	1000077	1.000077	1.000077
3.000078	1000078	1000078000	10	1000078	1.000078	1.000078
3.000079	1000079	1000079000	10	1000079	1.000079	1.000079
3.000080	1000080	1000080000	10	1000080	1.000080	1.000080
3.000081	1000081	1000081000	10	1000081	1.000081	1.000081
3.000082	1000082	1000082000	10	1000082	1.000082	1.000082
3.000083	1000083	1000083000	10	1000083	1.000083	1.000083
3.000084	1000084	1000084000	10	1000084	1.000084	1.000084
3.000085	1000085	1000085000	10	1000085	1.000085	1.000085
3.000086	1000086	1000086000	10	1000086	1.000086	1.000086
3.000087	1000087	1000087000	10	1000087	1.000087	1.000087
3.000088	1000088	1000088000	10	1000088	1.000088	1.000088
3.000089	1000089	1000089000	10	1000089	1.000089	1.000089
3.000090	1000090	1000090000	10	1000090	1.000090	1.000090
3.000091	1000091	1000091000	10	1000091	1.000091	1.000091
3.000092	1000092	1000092000	10	1000092	1.000092	1.000092
3.000093	1000093	1000093000	10	1000093	1.000093	1.000093
3.000094	1000094	1000094000	10	1000094	1.000094	1.000094
3.000095	1000095	1000095000	10	1000095	1.000095	1.000095
3.000096	1000096	1000096000	10	1000096	1.000096	1.000096
3.000097	1000097	1000097000	10	1000097	1.000097	1.000097
3.000098	1000098	1000098000	10	1000098	1.000098	1.000098
3.000099	1000099	1000099000	10	1000099	1.000099	1.000099
3.000100	1000100	1000100000	10	1000100	1.000100	1.000100

3.000101	1000101	1000101000	10	1000101	1.000101	1.000101
3.000102	1000102	1000102000	10	1000102	1.000102	1.000102
3.000103	1000103	1000103000	10	1000103	1.000103	1.000103
3.000104	1000104	1000104000	10	1000104	1.000104	1.000104
3.000105	1000105	1000105000	10	1000105	1.000105	1.000105
3.000106	1000106	1000106000	10	1000106	1.000106	1.000106
3.000107	1000107	1000107000	10	1000107	1.000107	1.000107
3.000108	1000108	1000108000	10	1000108	1.000108	1.000108
3.000109	1000109	1000109000	10	1000109	1.000109	1.000109
3.000110	1000110	1000110000	10	1000110	1.000110	1.000110
3.000111	1000111	1000111000	10	1000111	1.000111	1.000111
3.000112	1000112	1000112000	10	1000112	1.000112	1.000112
3.000113	1000113	1000113000	10	1000113	1.000113	1.000113
3.000114	1000114	1000114000	10	1000114	1.000114	1.000114
3.000115	1000115	1000115000	10	1000115	1.000115	1.000115
3.000116	1000116	1000116000	10	1000116	1.000116	1.000116
3.000117	1000117	1000117000	10	1000117	1.000117	1.000117
3.000118	1000118	1000118000	10	1000118	1.000118	1.000118
3.000119	1000119	1000119000	10	1000119	1.000119	1.000119
3.000120	1000120	1000120000	10	1000120	1.000120	1.000120
3.000121	1000121	1000121000	10	1000121	1.000121	1.000121
3.000122	1000122	1000122000	10	1000122	1.000122	1.000122
3.000123	1000123	1000123000	10	1000123	1.000123	1.000123
3.000124	1000124	1000124000	10	1000124	1.000124	1.000124
3.000125	1000125	1000125000	10	1000125	1.000125	1.000125
3.000126	1000126	1000126000	10	1000126	1.000126	1.000126
3.000127	1000127	1000127000	10	1000127	1.000127	1.000127
3.000128	1000128	1000128000	10	1000128	1.000128	1.000128
3.000129	1000129	1000129000	10	1000129	1.000129	1.000129
3.000130	1000130	1000130000	10	1000130	1.000130	1.000130
3.000131	1000131	1000131000	10	1000131	1.000131	1.000131
3.000132	1000132	1000132000	10	1000132	1.000132	1.000132
3.000133	1000133	1000133000	10	1000133	1.000133	1.000133
3.000134	1000134	1000134000	10	1000134	1.000134	1.000134
3.000135	1000135	1000135000	10	1000135	1.000135	1.000135
3.000136						





8.340705	3415	1011284	23.423022	3.332217	8.339951
8.340740	3415	14796200	23.423722	3.332678	8.339951
8.340775	3415	12968170	23.423900	3.332776	8.339951
8.340810	3415	03401770	23.424197	3.332859	8.3401396
8.340845	3415	03102230	23.424377	3.332944	8.3401396
8.340880	3415	78514750	23.424557	3.333029	8.3401396
8.340915	3415	49369320	23.424737	3.333114	8.3401396
8.340950	3415	44684340	23.424917	3.333199	8.3401396
8.340985	3415	44319490	23.425097	3.333284	8.3401396
8.341020	3415	03323970	23.425277	3.333369	8.3401396
8.341055	3415	03266170	23.425457	3.333454	8.3401396
8.341090	3415	03208370	23.425637	3.333539	8.3401396
8.341125	3415	03150570	23.425817	3.333624	8.3401396
8.341160	3415	03092770	23.425997	3.333709	8.3401396
8.341195	3415	03034970	23.426177	3.333794	8.3401396
8.341230	3415	02977170	23.426357	3.333879	8.3401396
8.341265	3415	02919370	23.426537	3.333964	8.3401396
8.341300	3415	02861570	23.426717	3.334049	8.3401396
8.341335	3415	02803770	23.426897	3.334134	8.3401396
8.341370	3415	02745970	23.427077	3.334219	8.3401396
8.341405	3415	02688170	23.427257	3.334304	8.3401396
8.341440	3415	02630370	23.427437	3.334389	8.3401396
8.341475	3415	02572570	23.427617	3.334474	8.3401396
8.341510	3415	02514770	23.427797	3.334559	8.3401396
8.341545	3415	02456970	23.427977	3.334644	8.3401396
8.341580	3415	02399170	23.428157	3.334729	8.3401396
8.341615	3415	02341370	23.428337	3.334814	8.3401396
8.341650	3415	02283570	23.428517	3.334899	8.3401396
8.341685	3415	02225770	23.428697	3.334984	8.3401396
8.341720	3415	02167970	23.428877	3.335069	8.3401396
8.341755	3415	02110170	23.429057	3.335154	8.3401396
8.341790	3415	02052370	23.429237	3.335239	8.3401396
8.341825	3415	01994570	23.429417	3.335324	8.3401396
8.341860	3415	01936770	23.429597	3.335409	8.3401396
8.341895	3415	01878970	23.429777	3.335494	8.3401396
8.341930	3415	01821170	23.429957	3.335579	8.3401396
8.341965	3415	01763370	23.430137	3.335664	8.3401396
8.342000	3415	01705570	23.430317	3.335749	8.3401396
8.342035	3415	01647770	23.430497	3.335834	8.3401396
8.342070	3415	01589970	23.430677	3.335919	8.3401396
8.342105	3415	01532170	23.430857	3.336004	8.3401396
8.342140	3415	01474370	23.431037	3.336089	8.3401396
8.342175	3415	01416570	23.431217	3.336174	8.3401396
8.342210	3415	01358770	23.431397	3.336259	8.3401396
8.342245	3415	01300970	23.431577	3.336344	8.3401396
8.342280	3415	01243170	23.431757	3.336429	8.3401396
8.342315	3415	01185370	23.431937	3.336514	8.3401396
8.342350	3415	01127570	23.432117	3.336599	8.3401396
8.342385	3415	01069770	23.432297	3.336684	8.3401396
8.342420	3415	01011970	23.432477	3.336769	8.3401396
8.342455	3415	00954170	23.432657	3.336854	8.3401396
8.342490	3415	00896370	23.432837	3.336939	8.3401396
8.342525	3415	00838570	23.433017	3.337024	8.3401396
8.342560	3415	00780770	23.433197	3.337109	8.3401396
8.342595	3415	00722970	23.433377	3.337194	8.3401396
8.342630	3415	00665170	23.433557	3.337279	8.3401396
8.342665	3415	00607370	23.433737	3.337364	8.3401396
8.342700	3415	00549570	23.433917	3.337449	8.3401396
8.342735	3415	00491770	23.434097	3.337534	8.3401396
8.342770	3415	00433970	23.434277	3.337619	8.3401396
8.342805	3415	00376170	23.434457	3.337704	8.3401396
8.342840	3415	00318370	23.434637	3.337789	8.3401396
8.342875	3415	00260570	23.434817	3.337874	8.3401396
8.342910	3415	00202770	23.434997	3.337959	8.3401396
8.342945	3415	00144970	23.435177	3.338044	8.3401396
8.342980	3415	00087170	23.435357	3.338129	8.3401396
8.343015	3415	00029370	23.435537	3.338214	8.3401396
8.343050	3415	000000	23.435717	3.338299	8.3401396

8.343085	3415	000000	23.435897	3.338384	8.3401396
8.343120	3415	000000	23.436077	3.338469	8.3401396
8.343155	3415	000000	23.436257	3.338554	8.3401396
8.343190	3415	000000	23.436437	3.338639	8.3401396
8.343225	3415	000000	23.436617	3.338724	8.3401396
8.343260	3415	000000	23.436797	3.338809	8.3401396
8.343295	3415	000000	23.436977	3.338894	8.3401396
8.343330	3415	000000	23.437157	3.338979	8.3401396
8.343365	3415	000000	23.437337	3.339064	8.3401396
8.343400	3415	000000	23.437517	3.339149	8.3401396
8.343435	3415	000000	23.437697	3.339234	8.3401396
8.343470	3415	000000	23.437877	3.339319	8.3401396
8.343505	3415	000000	23.438057	3.339404	8.3401396
8.343540	3415	000000	23.438237	3.339489	8.3401396
8.343575	3415	000000	23.438417	3.339574	8.3401396
8.343610	3415	000000	23.438597	3.339659	8.3401396
8.343645	3415	000000	23.438777	3.339744	8.3401396
8.343680	3415	000000	23.438957	3.339829	8.3401396
8.343715	3415	000000	23.439137	3.339914	8.3401396
8.343750	3415	000000	23.439317	3.339999	8.3401396
8.343785	3415	000000	23.439497	3.340084	8.3401396
8.343820	3415	000000	23.439677	3.340169	8.3401396
8.343855	3415	000000	23.439857	3.340254	8.3401396
8.343890	3415	000000	23.440037	3.340339	8.3401396
8.343925	3415	000000	23.440217	3.340424	8.3401396
8.343960	3415	000000	23.440397	3.340509	8.3401396
8.344000	3415	000000	23.440577	3.340594	8.3401396
8.344040	3415	000000	23.440757	3.340679	8.3401396
8.344080	3415	000000	23.440937	3.340764	8.3401396
8.344120	3415	000000	23.441117	3.340849	8.3401396
8.344160	3415	000000	23.441297	3.340934	8.3401396
8.344200	3415	000000	23.441477	3.341019	8.3401396
8.344240	3415	000000	23.441657	3.341104	8.3401396
8.344280	3415	000000	23.441837	3.341189	8.3401396
8.344320	3415	000000	23.442017	3.341274	8.3401396
8.344360	3415	000000	23.442197	3.341359	8.3401396
8.344400	3415	000000	23.442377	3.341444	8.3401396
8.344440	3415	000000	23.442557	3.341529	8.3401396
8.344480	3415	000000	23.442737	3.341614	8.3401396
8.344520	3415	000000	23.442917	3.341699	8.3401396
8.344560	3415	000000	23.443097	3.341784	8.3401396
8.344600	3415	000000	23.443277	3.341869	8.3401396
8.344640	3415	000000	23.443457	3.341954	8.3401396
8.344680	3415	000000	23.443637	3.342039	8.3401396
8.344720	3415	000000	23.443817	3.342124	8.3401396
8.344760	3415	000000	23.443997	3.342209	8.3401396
8.344800	3415	000000	23.444177	3.342294	8.3401396
8.344840	3415	000000	23.444357	3.342379	8.3401396
8.344880	3415	000000	23.444537	3.342464	8.3401396
8.344920	3415	000000	23.444717	3.342549	8.3401396
8.344960	3415	000000	23.444897	3.342634	8.3401396
8.345000	3415	000000	23.445077	3.342719	8.3401396
8.345040	3415	000000	23.445257	3.342804	8.3401396
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8.345120	3415	000000	23.445617	3.342974	8.3401396
8.345160	3415	000000	23.445797	3.343059	8.3401396
8.345200	3415	000000	23.445977	3.343144	8.3401396
8.345240	3415	000000	23.446157	3.343229	8.3401396
8.345280	3415	000000	23.446337	3.343314	8.3401396
8.345320	3415	000000	23.446517	3.343399	8.3401396
8.345360	3415	000000	23.446697	3.343484	8.3401396
8.345400	3415	000000	23.446877	3.343569	8.3401396
8.345440	3415	000000	23.447057	3.343654	8.3401396
8.345480	3415	000000	23.447237	3.343739	8.3401396
8.345520	3415	000000	23.447417	3.343824	8.3401396
8.345560	3415	000000	23.447597	3.343909	8.3401396
8.345600	3415	000000	23.447777	3.343994	8.3401396
8.345640	3415	000000	23.447957	3.344079	8.3401396
8.345680	3415	000000	23.448137	3.344164	8.3401396
8.345720	3415	000000	23.448317	3.344249	8.3401396
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8.345920	3415	000000	23.449217	3.344674	8.3401396
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8.346040	3415	000000	23.449757	3.344929	8.3401396
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8.346120	3415	000000	23.450117	3.345099	8.3401396
8.346160	3415	000000	23.450297	3.345184	8.3401396
8.346200	3415	000000	23.450477	3.345269	8.3401396
8.346240	3415	000000	23.450657	3.345354	8.3401396
8.346280	3415	000000	23.450837	3.345439	8.3401396
8.346320	3415	000000	23.451017	3.345524	8.3401396
8.346360	3415	000000			





1.4977072	12622	9677128	17	507029	1.4977072	9.7674502
1.4977073	-22.727612	9677129	17	507030	1.4977073	9.7674503
1.4977074	7.714	9677130	17	507031	1.4977074	9.7674504
1.4977075	-22.624722	9677131	17	507032	1.4977075	9.7674505
1.4977076	7.714	9677132	17	507033	1.4977076	9.7674506
1.4977077	-29.724832	9677133	17	507034	1.4977077	9.7674507
1.4977078	12.614	9677134	17	507035	1.4977078	9.7674508
1.4977079	-22.624722	9677135	17	507036	1.4977079	9.7674509
1.4977080	12.614	9677136	17	507037	1.4977080	9.7674510
1.4977081	-29.724832	9677137	17	507038	1.4977081	9.7674511
1.4977082	7.714	9677138	17	507039	1.4977082	9.7674512
1.4977083	-22.624722	9677139	17	507040	1.4977083	9.7674513
1.4977084	12.614	9677140	17	507041	1.4977084	9.7674514
1.4977085	-29.724832	9677141	17	507042	1.4977085	9.7674515
1.4977086	7.714	9677142	17	507043	1.4977086	9.7674516
1.4977087	-22.624722	9677143	17	507044	1.4977087	9.7674517
1.4977088	12.614	9677144	17	507045	1.4977088	9.7674518
1.4977089	-29.724832	9677145	17	507046	1.4977089	9.7674519
1.4977090	7.714	9677146	17	507047	1.4977090	9.7674520
1.4977091	-22.624722	9677147	17	507048	1.4977091	9.7674521
1.4977092	12.614	9677148	17	507049	1.4977092	9.7674522
1.4977093	-29.724832	9677149	17	507050	1.4977093	9.7674523
1.4977094	7.714	9677150	17	507051	1.4977094	9.7674524
1.4977095	-22.624722	9677151	17	507052	1.4977095	9.7674525
1.4977096	12.614	9677152	17	507053	1.4977096	9.7674526
1.4977097	-29.724832	9677153	17	507054	1.4977097	9.7674527
1.4977098	7.714	9677154	17	507055	1.4977098	9.7674528
1.4977099	-22.624722	9677155	17	507056	1.4977099	9.7674529
1.4977100	12.614	9677156	17	507057	1.4977100	9.7674530
1.4977101	-29.724832	9677157	17	507058	1.4977101	9.7674531
1.4977102	7.714	9677158	17	507059	1.4977102	9.7674532
1.4977103	-22.624722	9677159	17	507060	1.4977103	9.7674533
1.4977104	12.614	9677160	17	507061	1.4977104	9.7674534
1.4977105	-29.724832	9677161	17	507062	1.4977105	9.7674535
1.4977106	7.714	9677162	17	507063	1.4977106	9.7674536
1.4977107	-22.624722	9677163	17	507064	1.4977107	9.7674537
1.4977108	12.614	9677164	17	507065	1.4977108	9.7674538
1.4977109	-29.724832	9677165	17	507066	1.4977109	9.7674539
1.4977110	7.714	9677166	17	507067	1.4977110	9.7674540
1.4977111	-22.624722	9677167	17	507068	1.4977111	9.7674541
1.4977112	12.614	9677168	17	507069	1.4977112	9.7674542
1.4977113	-29.724832	9677169	17	507070	1.4977113	9.7674543
1.4977114	7.714	9677170	17	507071	1.4977114	9.7674544
1.4977115	-22.624722	9677171	17	507072	1.4977115	9.7674545
1.4977116	12.614	9677172	17	507073	1.4977116	9.7674546
1.4977117	-29.724832	9677173	17	507074	1.4977117	9.7674547
1.4977118	7.714	9677174	17	507075	1.4977118	9.7674548
1.4977119	-22.624722	9677175	17	507076	1.4977119	9.7674549
1.4977120	12.614	9677176	17	507077	1.4977120	9.7674550
1.4977121	-29.724832	9677177	17	507078	1.4977121	9.7674551
1.4977122	7.714	9677178	17	507079	1.4977122	9.7674552
1.4977123	-22.624722	9677179	17	507080	1.4977123	9.7674553
1.4977124	12.614	9677180	17	507081	1.4977124	9.7674554
1.4977125	-29.724832	9677181	17	507082	1.4977125	9.7674555
1.4977126	7.714	9677182	17	507083	1.4977126	9.7674556
1.4977127	-22.624722	9677183	17	507084	1.4977127	9.7674557
1.4977128	12.614	9677184	17	507085	1.4977128	9.7674558
1.4977129	-29.724832	9677185	17	507086	1.4977129	9.7674559
1.4977130	7.714	9677186	17	507087	1.4977130	9.7674560
1.4977131	-22.624722	9677187	17	507088	1.4977131	9.7674561
1.4977132	12.614	9677188	17	507089	1.4977132	9.7674562
1.4977133	-29.724832	9677189	17	507090	1.4977133	9.7674563
1.4977134	7.714	9677190	17	507091	1.4977134	9.7674564
1.4977135	-22.624722	9677191	17	507092	1.4977135	9.7674565
1.4977136	12.614	9677192	17	507093	1.4977136	9.7674566
1.4977137	-29.724832	9677193	17	507094	1.4977137	9.7674567
1.4977138	7.714	9677194	17	507095	1.4977138	9.7674568
1.4977139	-22.624722	9677195	17	507096	1.4977139	9.7674569
1.4977140	12.614	9677196	17	507097	1.4977140	9.7674570
1.4977141	-29.724832	9677197	17	507098	1.4977141	9.7674571
1.4977142	7.714	9677198	17	507099	1.4977142	9.7674572
1.4977143	-22.624722	9677199	17	507100	1.4977143	9.7674573
1.4977144	12.614	9677200	17	507101	1.4977144	9.7674574
1.4977145	-29.724832	9677201	17	507102	1.4977145	9.7674575
1.4977146	7.714	9677202	17	507103	1.4977146	9.7674576
1.4977147	-22.624722	9677203	17	507104	1.4977147	9.7674577
1.4977148	12.614	9677204	17	507105	1.4977148	9.7674578
1.4977149	-29.724832	9677205	17	507106	1.4977149	9.7674579
1.4977150	7.714	9677206	17	507107	1.4977150	9.7674580
1.4977151	-22.624722	9677207	17	507108	1.4977151	9.7674581
1.4977152	12.614	9677208	17	507109	1.4977152	9.7674582
1.4977153	-29.724832	9677209	17	507110	1.4977153	9.7674583
1.4977154	7.714	9677210	17	507111	1.4977154	9.7674584
1.4977155	-22.624722	9677211	17	507112	1.4977155	9.7674585
1.4977156	12.614	9677212	17	507113	1.4977156	9.7674586
1.4977157	-29.724832	9677213	17	507114	1.4977157	9.7674587
1.4977158	7.714	9677214	17	507115	1.4977158	9.7674588
1.4977159	-22.624722	9677215	17	507116	1.4977159	9.7674589
1.4977160	12.614	9677216	17	507117	1.4977160	9.7674590
1.4977161	-29.724832	9677217	17	507118	1.4977161	9.7674591
1.4977162	7.714	9677218	17	507119	1.4977162	9.7674592
1.4977163	-22.624722	9677219	17	507120	1.4977163	9.7674593
1.4977164	12.614	9677220	17	507121	1.4977164	9.7674594
1.4977165	-29.724832	9677221	17	507122	1.4977165	9.7674595
1.4977166	7.714	9677222	17	507123	1.4977166	9.7674596
1.4977167	-22.624722	9677223	17	507124	1.4977167	9.7674597
1.4977168	12.614	9677224	17	507125	1.4977168	9.7674598
1.4977169	-29.724832	9677225	17	507126	1.4977169	9.7674599
1.4977170	7.714	9677226	17	507127	1.4977170	9.7674600
1.4977171	-22.624722	9677227	17	507128	1.4977171	9.7674601
1.4977172	12.614	9677228	17	507129	1.4977172	9.7674602
1.4977173	-29.724832	9677229	17	507130	1.4977173	9.7674603
1.4977174	7.714	9677230	17	507131	1.4977174	9.7674604
1.4977175	-22.624722	9677231	17	507132	1.4977175	9.7674605
1.4977176	12.614	9677232	17	507133	1.4977176	9.7674606
1.4977177	-29.724832	9677233	17	507134	1.4977177	9.7674607
1.4977178	7.714	9677234	17	507135	1.4977178	9.7674608
1.4977179	-22.624722	9677235	17	507136	1.4977179	9.7674609
1.4977180	12.614	9677236	17	507137	1.4977180	9.7674610
1.4977181	-29.724832	9677237	17	507138	1.4977181	9.7674611
1.4977182	7.714	9677238	17	507139	1.4977182	9.7674612
1.4977183	-22.624722	9677239	17	507140	1.4977183	9.7674613
1.4977184	12.614	9677240	17	507141	1.4977184	9.7674614
1.4977185	-29.724832	9677241	17	507142	1.4977185	9.7674615
1.4977186	7.714	9677242	17	507143	1.4977186	9.7674616
1.4977187	-22.624722	9677243	17	507144	1.4977187	9.7674617
1.4977188	12.614	9677244	17	507145	1.4977188	9.7674618
1.4977189	-29.724832	9677245	17	507146	1.4977189	9.7674619
1.4977190	7.714	9677246	17	507147	1.4977190	9.7674620
1.4977191	-22.624722	9677247	17	507148	1.4977191	9.7674621
1.4977192	12.614	9677248	17	507149	1.4977192	9.7674622
1.4977193	-29.724832	9677249	17	507150	1.4977193	9.7674623
1.4977194	7.714	9677250	17	507151	1.4977194	9.7674624
1.4977195	-22.624722	9677251	17	507152	1.4977195	9.7674625
1.4977196	12.614	9677252	17	507153	1.4977196	9.7674626
1.4977197	-29.724832	9677253	17	507154	1.4977197	9.7674627
1.4977198	7.714	9677254	17	507155	1.4977198	9.7674628
1.4977199	-22.624722	9677255	17	507156	1.4977199	9.7674629
1.4977200	12.614	9677256	17	507157	1.4977200	9.7674630

1.4977201	-29.724832	9677257	17	507158	1.4977201	9.7674631
1.4977202	7.714	9677258	17	507159	1.4977202	9.7674632
1.4977203	-22.624722	9677259	17	507160	1.4977203	9.7674633
1.4977204	12.614	9677260	17	507161	1.4977204	9.7674634
1.4977205	-29.724832	9677261	17	507162	1.4977205	9.7674635
1.4977206	7.714	9677262	17	507163	1.4977206	9.7674636
1.4977207	-22.624722	9677263	17	507164	1.4977207	9.7674637
1.4977208	12.614	9677264	17	507165	1.4977208	9.7674638
1.4977209	-29.724832</					



1	0.25	17475	2,722000	10741	48027501
2	0.25	17475	22,222700	10755	48027501
3	0.25	17475	27,222700	10769	48027501
4	0.50	17475	22,222700	20773	48027501
5	0.50	17475	22,222700	20787	48027501
6	0.50	17475	22,222700	20801	48027501

Force history on pile head  
 Horizontal load on pile head  
 Vertical load on pile head

Time	Force	Displacement	Stiffness	Area	Volume	Mass	Energy
sec	lb	in	lb/in	in <sup>2</sup>	in <sup>3</sup>	lb-sec	in-lb

Layering Data for Analysis, Depth of Soil in Each Layer

Layer No.	Top of Layer (ft)	Bottom of Layer (ft)	Layer Thickness (ft)	Soil Type	Soil Description	Soil Unit Weight (pcf)	Soil Modulus (ksi)	Soil Poisson's Ratio
1	0.00	0.25	0.25	S.S.	...	...	...	...
2	0.25	0.50	0.25	S.S.	...	...	...	...
3	0.50	1.00	0.50	S.S.	...	...	...	...
4	1.00	2.00	1.00	S.S.	...	...	...	...
5	2.00	3.00	1.00	S.S.	...	...	...	...
6	3.00	4.00	1.00	S.S.	...	...	...	...
7	4.00	5.00	1.00	S.S.	...	...	...	...
8	5.00	6.00	1.00	S.S.	...	...	...	...
9	6.00	7.00	1.00	S.S.	...	...	...	...
10	7.00	8.00	1.00	S.S.	...	...	...	...
11	8.00	9.00	1.00	S.S.	...	...	...	...
12	9.00	10.00	1.00	S.S.	...	...	...	...
13	10.00	11.00	1.00	S.S.	...	...	...	...
14	11.00	12.00	1.00	S.S.	...	...	...	...
15	12.00	13.00	1.00	S.S.	...	...	...	...

Notes: 1. The soil modulus and Poisson's ratio are the sum of the 10 and 20 layers. 2. The soil modulus and Poisson's ratio are constant within each layer. 3. The soil unit weight is the same for all layers. 4. The soil modulus and Poisson's ratio are the same for all layers. 5. The soil unit weight is the same for all layers.

Computed values of pile reaction and load for lateral loading for each layer

Reaction and load on pile head and on each layer

Time (sec)	Force (lb)	Displacement (in)	Stiffness (lb/in)	Area (in <sup>2</sup> )	Volume (in <sup>3</sup> )	Mass (lb-sec)	Energy (in-lb)
0.00	0.00	0.00	1.00E+07	0.00	0.00	0.00	0.00
0.01	1.00	0.01	1.00E+07	0.00	0.00	0.00	0.01
0.02	2.00	0.02	1.00E+07	0.00	0.00	0.00	0.04
0.03	3.00	0.03	1.00E+07	0.00	0.00	0.00	0.09
0.04	4.00	0.04	1.00E+07	0.00	0.00	0.00	0.16
0.05	5.00	0.05	1.00E+07	0.00	0.00	0.00	0.25
0.06	6.00	0.06	1.00E+07	0.00	0.00	0.00	0.36
0.07	7.00	0.07	1.00E+07	0.00	0.00	0.00	0.49
0.08	8.00	0.08	1.00E+07	0.00	0.00	0.00	0.64
0.09	9.00	0.09	1.00E+07	0.00	0.00	0.00	0.81
0.10	10.00	0.10	1.00E+07	0.00	0.00	0.00	1.00
0.11	11.00	0.11	1.00E+07	0.00	0.00	0.00	1.21
0.12	12.00	0.12	1.00E+07	0.00	0.00	0.00	1.44
0.13	13.00	0.13	1.00E+07	0.00	0.00	0.00	1.69
0.14	14.00	0.14	1.00E+07	0.00	0.00	0.00	1.96
0.15	15.00	0.15	1.00E+07	0.00	0.00	0.00	2.25
0.16	16.00	0.16	1.00E+07	0.00	0.00	0.00	2.56
0.17	17.00	0.17	1.00E+07	0.00	0.00	0.00	2.89
0.18	18.00	0.18	1.00E+07	0.00	0.00	0.00	3.24
0.19	19.00	0.19	1.00E+07	0.00	0.00	0.00	3.61
0.20	20.00	0.20	1.00E+07	0.00	0.00	0.00	4.00



12 1490	-0.2243	133014	117722	0.430-07	0.00	0.39112
28 978	49073	0.00				
12 1500	-0.2042	140811	117722	0.430-07	0.00	0.39112
178 787	-0.031	4.02				
12 1510	-0.0020	144390	115114	0.412-07	0.00	0.37012
178 787	1227	0.01				
12 1520	-0.4312	179791	115024	-0.301-07	0.00	0.39012
775 842	0.111	0.78				
14 1528	-0.0121	179791	115107	0.422-07	0.00	0.39012
790 452	1280	0.04				
15 1532	-0.0144	181929	116022	-0.222-07	0.01	0.09112
330 210	0.20	0.78				
15 1534	-0.0194	181929	116044	-0.222-07	0.01	0.09112
150 850	0.025	0.84				
15 1538	-0.0194	181929	117724	-0.222-04	0.04	0.09112
400 2100	0.03	0.00				
15 1539	-0.0194	181929	11840	-0.222-04	0.04	0.09112
400 2100	0.03	0.00				
15 1540	-0.0229	184044	11850	-0.222-04	0.04	0.09112
900 400	0.071	0.00				
12 1529	-0.1279	181929	10724	-0.122-04	0.04	0.19112
100 210	0.03	0.00				
12 1529	-0.0207	184044	10724	-0.122-04	0.04	0.19112
100 210	0.03	0.00				
12 1529	-0.0207	184044	10724	-0.122-04	0.04	0.19112
100 210	0.03	0.00				
16 1530	-0.2007	181929	11840	0.122-07	0.00	0.19112
177 842	0.031	0.02				
17 1530	-0.2007	181929	118716	0.122-07	0.00	0.19112
185 210	0.031	0.01				
17 1530	-0.4312	181929	118712	-0.301-07	0.00	0.19112
440 701	0.11	0.78				
17 1530	-0.4312	181929	7804	-0.071-07	0.00	0.19112
720 210	0.04	0.78				
17 1530	-0.4312	181929	8507	0.001-07	0.00	0.19112
890 775	0.120	0.04				
17 1532	-0.0144	184044	1807	0.021-04	0.00	0.19112
320	0.027	0.00				
18 1442	-0.0141	181929	1172	-0.041-07	0.00	0.19112
700	0.014	0.00				
18 1442	-2.0719	181929	-0084	0.021-07	0.00	0.19112
710	0.022	0.00				
18 1477	-2.0720	181929	0044	0.077-04	0.00	0.19112
120	0.034	0.00				
24 1414	-0.0000	184044	-0072	-0.011-00	0.00	0.19112
200	0.017	0.00				
24 1414	-0.0000	184044	-0207	-0.011-04	0.00	0.19112
210	0.014	0.00				
24 1414	-0.0000	184044	-0222	-0.011-04	0.00	0.19112
210	0.014	0.00				

17 1502	-0.0612	184044	0072	-0.022-04	0.00	0.19112
340	0.072	0.00				
17 1502	-0.0612	184044	0072	-0.022-04	0.00	0.19112
354	0.084	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
390	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
400	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
410	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
420	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
430	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
440	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
450	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
460	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
470	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
480	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
490	0.072	0.00				
17 1502	-0.0612	184044	1004	-0.022-04	0.00	0.19112
500	0.072	0.00				

\* This analysis compares pile behavior using nonlinear "beam-column" and "pile" models. Values of total moment at pile head and bearing capacity are computed only for elastic calculations and do not show the actual values for concrete and steel stresses in concrete and steel. They are computed from the output for nonlinear loading procedure relative to the magnitude of bearing capacity developed in the pile.

Output Summary for Load Case No. 11

Initial pile deflection	0.000000	in
Computed value at pile head	-0.046336	in
Final pile deflection	-0.046336	in
Final pile head force	111.275	lb
Final pile maximum bending moment	4.062940	lb-ft
Final pile maximum shear force	11.702790	lb
Final pile lateral displacement	0.00	in
Final pile axial displacement	0.00	in

Computed values of pile loading and deflection for lateral loading for load case No. 11

Individual loads are not shown as shown (loading type 0)									
Shear force at pile head	0	0072.0	lb						
Positive moment at pile head	0	094020.0	lb-ft						
Final lateral load at pile head	0	0072.0	lb						

Node	Deflect.	loading	Shear	Moment	Total	loading	soil
Node	Distort.	Force	Force	Moment	Force	Stiffness	p





100%	0.0000	0.00				
75.00%	-0.1200	2250	5700	7.75E+24	1.00	7.10E02
50%	0.0000	0.00				
25.00%	-0.1200	2250	4050	7.75E+24	1.00	7.10E02
00%	0.0000	0.00				
75.00%	-0.1200	0.00	7.50	7.75E+24	1.00	7.10E02
100%	0.0000	0.00				

\* This analysis consists of pile stresses, axial and shear moment-curvature relationships, values of lateral deflection, maximum axial and bending moments are reported only for the design load case only. We do not report the actual stresses in concrete and steel. Stresses in concrete and steel may be lower relative to the design load case. Actual loading parameters relative to the magnitude of loading is most critical to the pile.

**Output Summary for Case Design 100%**

pile-head deflection	=	0.000000000000
computed slope at pile head	=	0.000000000000
maximum bending moment	=	2960750.000000
maximum shear force	=	-8373.000000
depth of neutral loading point	=	0.000000000000 feet below pile head
depth of neutral shear force	=	0.000000000000 feet below pile head
number of elements	=	1
number of pile deflection nodes	=	2

Computed values of pile loading and lateral deflection for lateral loading for Case Design 100%

**Computed values of axial and lateral and moment bending loads**

axial force at pile head	=	4600.0 lbs
axial force at pile end	=	66455.0 lbs
axial stress at pile head	=	1.600E+04 psi
axial stress at pile end	=	1.950E+05 psi
shear force at pile head	=	0.000000 lbs
shear force at pile end	=	0.000000 lbs
bending moment at pile head	=	0.000000 ft-lbs
bending moment at pile end	=	2960750.000000 ft-lbs
curvature at pile head	=	0.000000 1/ft
curvature at pile end	=	0.000000 1/ft
lateral deflection at pile head	=	0.000000 ft
lateral deflection at pile end	=	0.000000 ft
slope at pile head	=	0.000000 1/ft
slope at pile end	=	0.000000 1/ft

1.0000	4.0100	944250	30070	0.2500	0.75	2.00E+02
0.9999	4.0100	1.00				
0.9998	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9997	-0.1440	1.00				
0.9996	0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9995	0.1440	1.00				
0.9994	-0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9993	-0.1440	1.00				
0.9992	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9991	0.1440	1.00				
0.9990	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9989	-0.1440	1.00				
0.9988	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9987	0.1440	1.00				
0.9986	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9985	-0.1440	1.00				
0.9984	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9983	0.1440	1.00				
0.9982	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9981	-0.1440	1.00				
0.9980	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9979	0.1440	1.00				
0.9978	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9977	-0.1440	1.00				
0.9976	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9975	0.1440	1.00				
0.9974	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9973	-0.1440	1.00				
0.9972	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9971	0.1440	1.00				
0.9970	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9969	-0.1440	1.00				
0.9968	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9967	0.1440	1.00				
0.9966	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9965	-0.1440	1.00				
0.9964	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9963	0.1440	1.00				
0.9962	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9961	-0.1440	1.00				
0.9960	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9959	0.1440	1.00				
0.9958	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9957	-0.1440	1.00				
0.9956	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9955	0.1440	1.00				
0.9954	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9953	-0.1440	1.00				
0.9952	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9951	0.1440	1.00				
0.9950	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9949	-0.1440	1.00				
0.9948	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9947	0.1440	1.00				
0.9946	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9945	-0.1440	1.00				
0.9944	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9943	0.1440	1.00				
0.9942	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9941	-0.1440	1.00				
0.9940	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9939	0.1440	1.00				
0.9938	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9937	-0.1440	1.00				
0.9936	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9935	0.1440	1.00				
0.9934	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9933	-0.1440	1.00				
0.9932	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9931	0.1440	1.00				
0.9930	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9929	-0.1440	1.00				
0.9928	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9927	0.1440	1.00				
0.9926	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9925	-0.1440	1.00				
0.9924	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9923	0.1440	1.00				
0.9922	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9921	-0.1440	1.00				
0.9920	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9919	0.1440	1.00				
0.9918	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9917	-0.1440	1.00				
0.9916	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9915	0.1440	1.00				
0.9914	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9913	-0.1440	1.00				
0.9912	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9911	0.1440	1.00				
0.9910	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9909	-0.1440	1.00				
0.9908	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9907	0.1440	1.00				
0.9906	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9905	-0.1440	1.00				
0.9904	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9903	0.1440	1.00				
0.9902	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9901	-0.1440	1.00				
0.9900	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9899	0.1440	1.00				
0.9898	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9897	-0.1440	1.00				
0.9896	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9895	0.1440	1.00				
0.9894	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9893	-0.1440	1.00				
0.9892	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9891	0.1440	1.00				
0.9890	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9889	-0.1440	1.00				
0.9888	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9887	0.1440	1.00				
0.9886	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9885	-0.1440	1.00				
0.9884	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9883	0.1440	1.00				
0.9882	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9881	-0.1440	1.00				
0.9880	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9879	0.1440	1.00				
0.9878	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9877	-0.1440	1.00				
0.9876	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9875	0.1440	1.00				
0.9874	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9873	-0.1440	1.00				
0.9872	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9871	0.1440	1.00				
0.9870	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9869	-0.1440	1.00				
0.9868	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9867	0.1440	1.00				
0.9866	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.9865	-0.1440	1.00				
0.9864	0.1440	664550	30070	0.0200	0.25	4.00E+02
0.9863	0.1440	1.00				
0.9862	-0.1440	664550	30070	-0.0200	0.25	4.00E+02
0.						



15.000	-0.0000	332257	-32257	5.779 66	0.00	4.100 10
244.000	0.0000	0.00				
10.000	-0.0000	330000	-30000	5.779 66	0.00	4.100 10
474.000	0.0000	0.00				
10.000	-0.0000	310000	-30000	5.779 66	0.00	4.100 10
484.000	0.0000	0.00				
10.000	0.0000	300000	-30000	5.779 66	0.00	4.100 10
504.000	0.0000	0.00				
10.000	0.0000	290000	-30000	5.779 66	0.00	4.100 10
524.000	0.0000	0.00				
10.000	0.0000	280000	-30000	5.779 66	0.00	4.100 10
544.000	0.0000	0.00				
10.000	0.0000	270000	-30000	5.779 66	0.00	4.100 10
564.000	0.0000	0.00				
10.000	0.0000	260000	-30000	5.779 66	0.00	4.100 10
584.000	0.0000	0.00				
10.000	0.0000	250000	-30000	5.779 66	0.00	4.100 10
604.000	0.0000	0.00				
10.000	0.0000	240000	-30000	5.779 66	0.00	4.100 10
624.000	0.0000	0.00				
10.000	0.0000	230000	-30000	5.779 66	0.00	4.100 10
644.000	0.0000	0.00				
10.000	0.0000	220000	-30000	5.779 66	0.00	4.100 10
664.000	0.0000	0.00				
10.000	0.0000	210000	-30000	5.779 66	0.00	4.100 10
684.000	0.0000	0.00				
10.000	0.0000	200000	-30000	5.779 66	0.00	4.100 10
704.000	0.0000	0.00				
10.000	0.0000	190000	-30000	5.779 66	0.00	4.100 10
724.000	0.0000	0.00				
10.000	0.0000	180000	-30000	5.779 66	0.00	4.100 10
744.000	0.0000	0.00				
10.000	0.0000	170000	-30000	5.779 66	0.00	4.100 10
764.000	0.0000	0.00				
10.000	0.0000	160000	-30000	5.779 66	0.00	4.100 10
784.000	0.0000	0.00				
10.000	0.0000	150000	-30000	5.779 66	0.00	4.100 10
804.000	0.0000	0.00				
10.000	0.0000	140000	-30000	5.779 66	0.00	4.100 10
824.000	0.0000	0.00				
10.000	0.0000	130000	-30000	5.779 66	0.00	4.100 10
844.000	0.0000	0.00				
10.000	0.0000	120000	-30000	5.779 66	0.00	4.100 10
864.000	0.0000	0.00				
10.000	0.0000	110000	-30000	5.779 66	0.00	4.100 10
884.000	0.0000	0.00				
10.000	0.0000	100000	-30000	5.779 66	0.00	4.100 10
904.000	0.0000	0.00				
10.000	0.0000	90000	-30000	5.779 66	0.00	4.100 10
924.000	0.0000	0.00				
10.000	0.0000	80000	-30000	5.779 66	0.00	4.100 10
944.000	0.0000	0.00				
10.000	0.0000	70000	-30000	5.779 66	0.00	4.100 10
964.000	0.0000	0.00				
10.000	0.0000	60000	-30000	5.779 66	0.00	4.100 10
984.000	0.0000	0.00				
10.000	0.0000	50000	-30000	5.779 66	0.00	4.100 10
1004.000	0.0000	0.00				
10.000	0.0000	40000	-30000	5.779 66	0.00	4.100 10
1024.000	0.0000	0.00				
10.000	0.0000	30000	-30000	5.779 66	0.00	4.100 10
1044.000	0.0000	0.00				
10.000	0.0000	20000	-30000	5.779 66	0.00	4.100 10
1064.000	0.0000	0.00				
10.000	0.0000	10000	-30000	5.779 66	0.00	4.100 10
1084.000	0.0000	0.00				
10.000	0.0000	0	-30000	5.779 66	0.00	4.100 10

Notes: 1. All pile load capacity values were determined using nonlinear computer simulations using the same model of total capacity due to combined axial and bending stresses as presented only in plastic sections only and at two points per section. 2. All pile load capacity values are based on ultimate strength of concrete and steel and do not include any safety factor for nonlinear bending response and do not include any safety factor for bending moment distribution in the pile.

Output Summary for Load Case No. 1:

Allowable deflection	=	0.000000 ft
Integrated slope at pile head	=	0.000000 rad
Maximum bending moment	=	1110000 lb-ft
Maximum axial force	=	-60000 lb
Maximum positive bending moment	=	0.000000 ft-lb
Maximum negative bending moment	=	1110000 lb-ft
Maximum axial force	=	0.000000 lb
Minimum axial force	=	0.000000 lb
Minimum axial force	=	0.000000 lb

Summary of Allowable Stresses for Designated Load Case:

Definitions of Allowable Loading Conditions:

- Load Case 1: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 2: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 3: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 4: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 5: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 6: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 7: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 8: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 9: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 10: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 11: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 12: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 13: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 14: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 15: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 16: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 17: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 18: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 19: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0
- Load Case 20: Load 1 - Shear, 0.175, and 1.0 ft from top of pile, N=1.0

Load Case	Load Type	Max. Allow. Deflection (ft)	Max. Allow. Slope (rad)	Max. Allow. Bending Moment (lb-ft)	Max. Allow. Axial Force (lb)
1	1	0.0000	0.0000	1110000	-60000
2	1	0.0000	0.0000	1110000	-60000
3	1	0.0000	0.0000	1110000	-60000
4	1	0.0000	0.0000	1110000	-60000
5	1	0.0000	0.0000	1110000	-60000
6	1	0.0000	0.0000	1110000	-60000
7	1	0.0000	0.0000	1110000	-60000
8	1	0.0000	0.0000	1110000	-60000
9	1	0.0000	0.0000	1110000	-60000
10	1	0.0000	0.0000	1110000	-60000
11	1	0.0000	0.0000	1110000	-60000
12	1	0.0000	0.0000	1110000	-60000
13	1	0.0000	0.0000	1110000	-60000
14	1	0.0000	0.0000	1110000	-60000
15	1	0.0000	0.0000	1110000	-60000
16	1	0.0000	0.0000	1110000	-60000
17	1	0.0000	0.0000	1110000	-60000
18	1	0.0000	0.0000	1110000	-60000
19	1	0.0000	0.0000	1110000	-60000
20	1	0.0000	0.0000	1110000	-60000

radial pressure distribution = 9.09499E-01 radian  
 radial pressure distribution = 1.00000E-01 radian = -0.283429 deg.

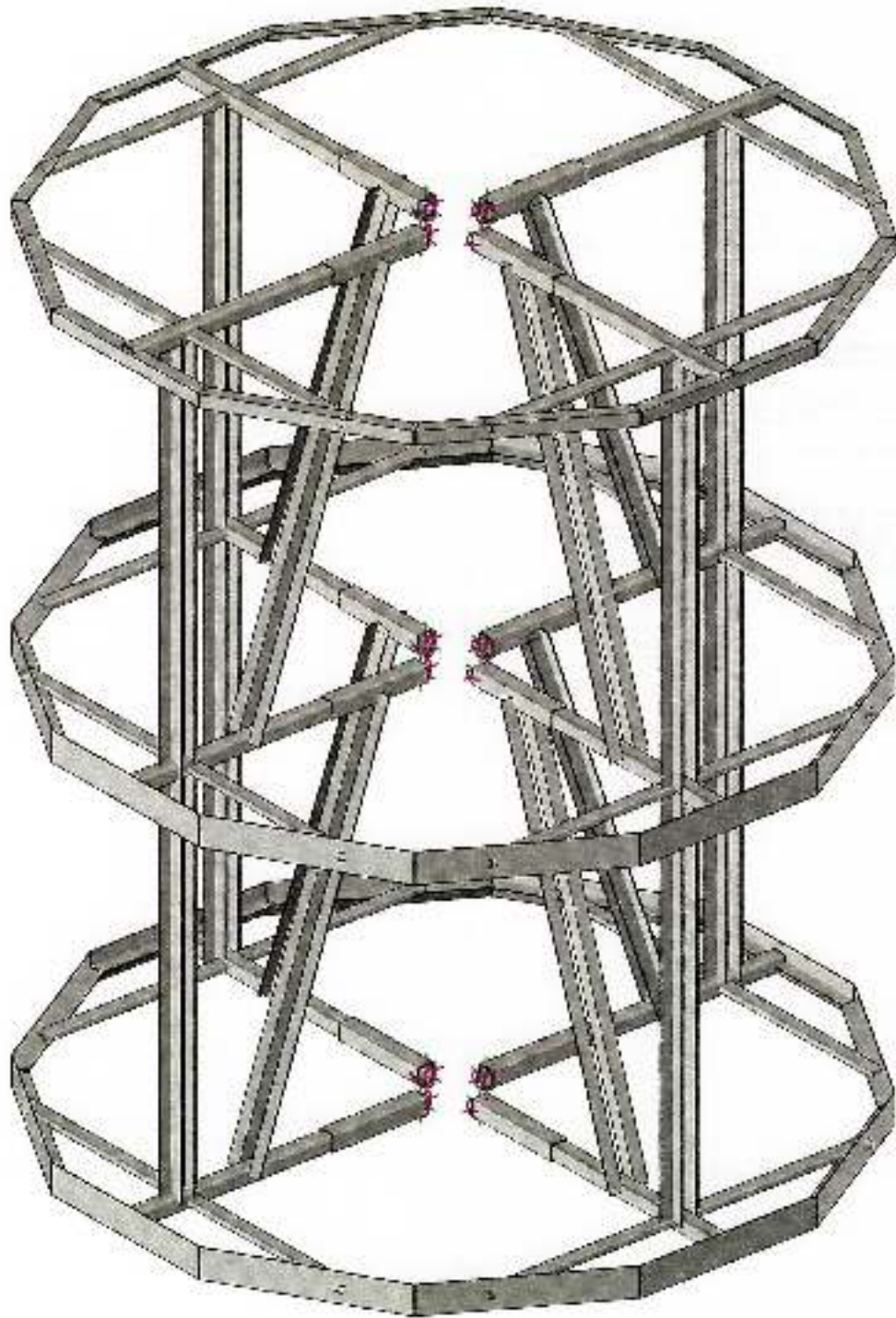
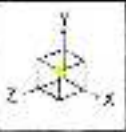
.....  
 Summary of Results Assigned  
 .....

The following chart gives a plot of the

..... charting .....

The above values for friction angle are values which are less than 20 degrees or higher than 40 degrees and are values of  $k$  and  $\alpha$  which are fixed for a soil type defined using the two criteria. They are not intended to be used for other soils. For  $k$ , but the friction angle is within the range of 10 to 20 degrees, above this range the values of  $k$  and  $\alpha$  are not shown.

See analysis manual for details.

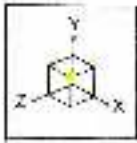


Vector SE

SK-1

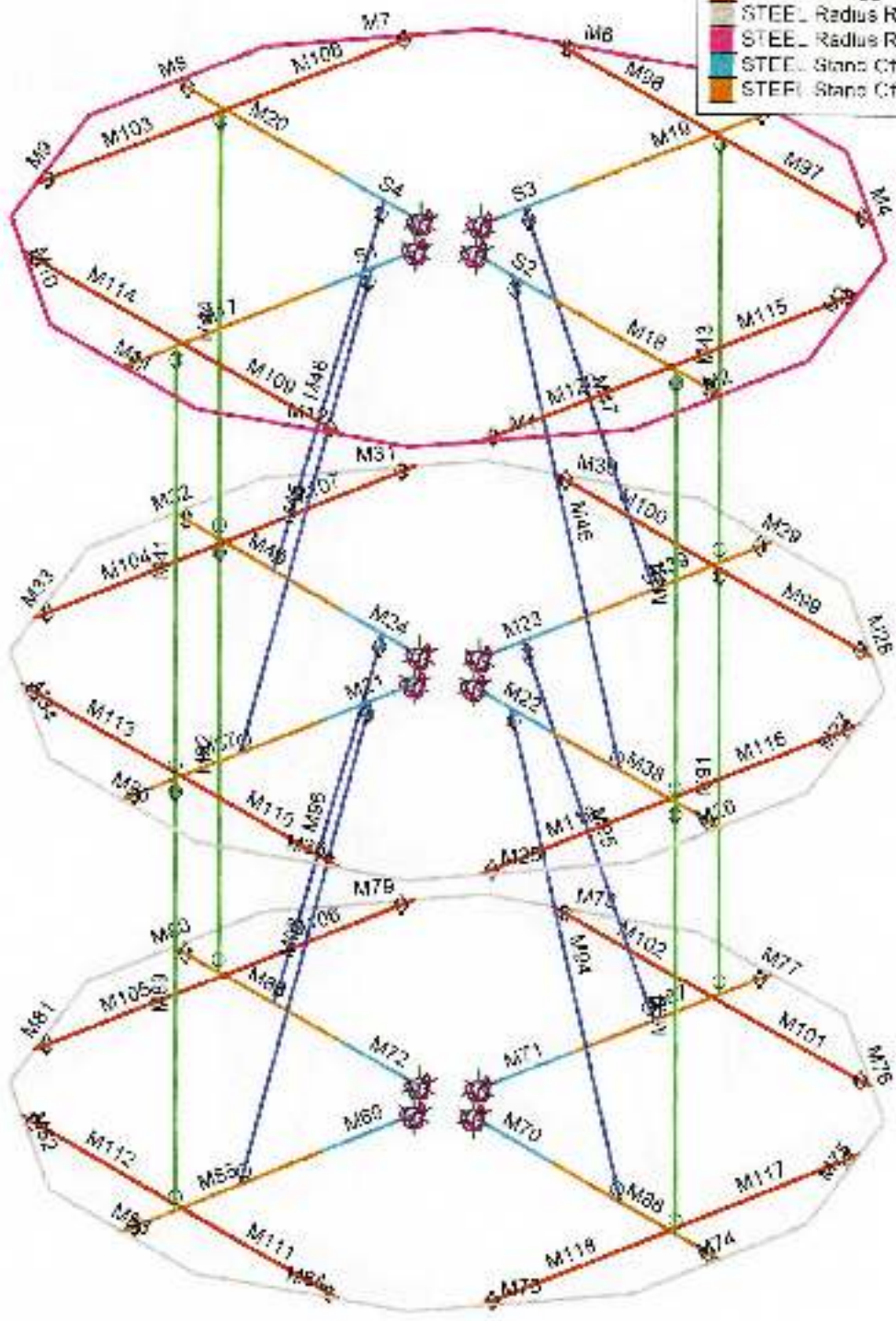
Oct 24, 2024 at 10:53 AM

NM1-115 Spoke Concealmen..



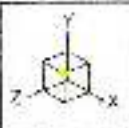
Section Sets

FRP Kicker Brace
FRP Vertical Brace
STEEL Outrigger Weldment
STEEL Radius Ring Assembly
STEEL Radius Ring Assembly Top
STEEL Stand Off Arm
STEEL Stand Off Arm inner

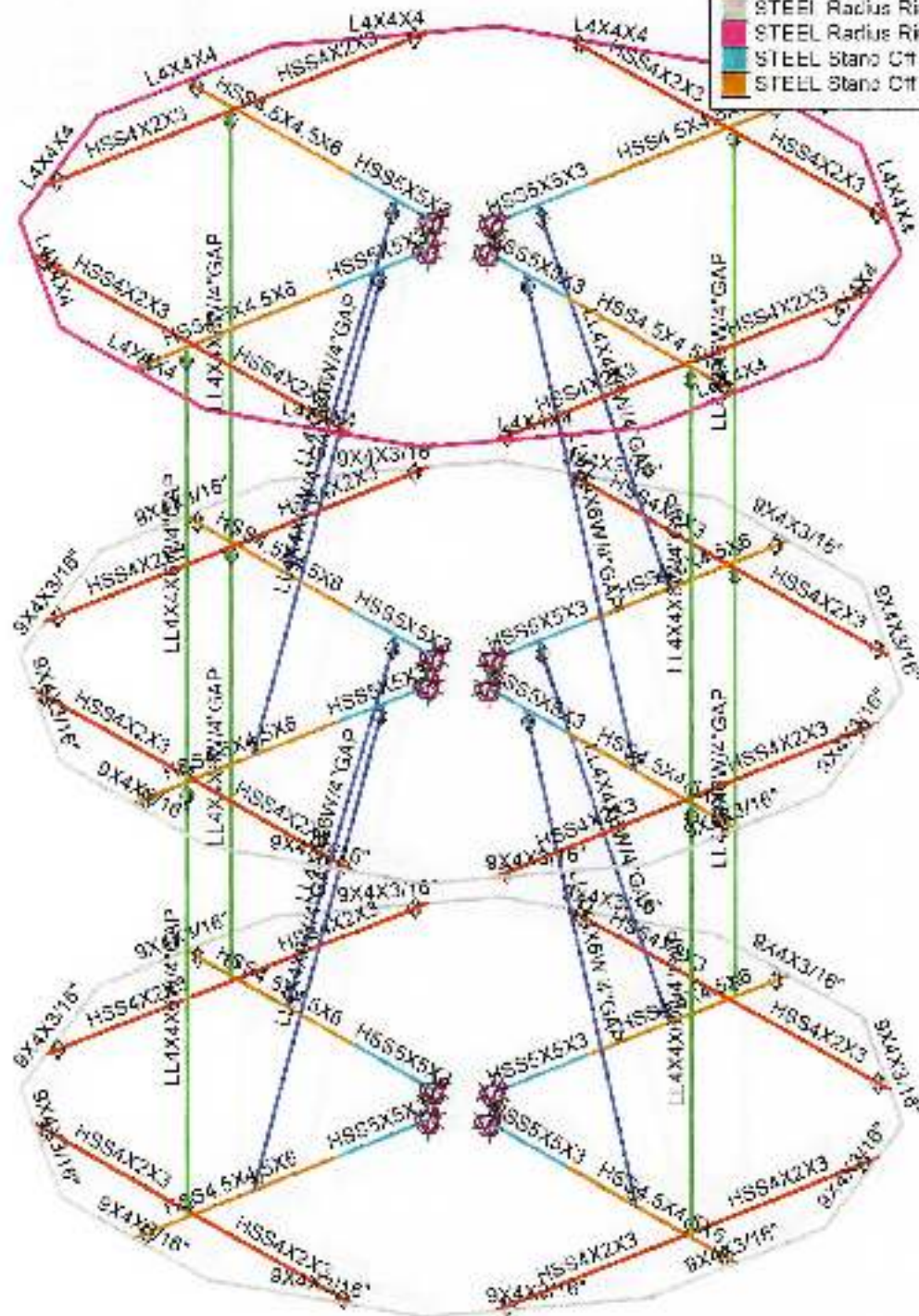


Vector SE

SK-2  
Oct 24, 2024 at 10:53 AM  
NM-1/8 Soko Concealmen...

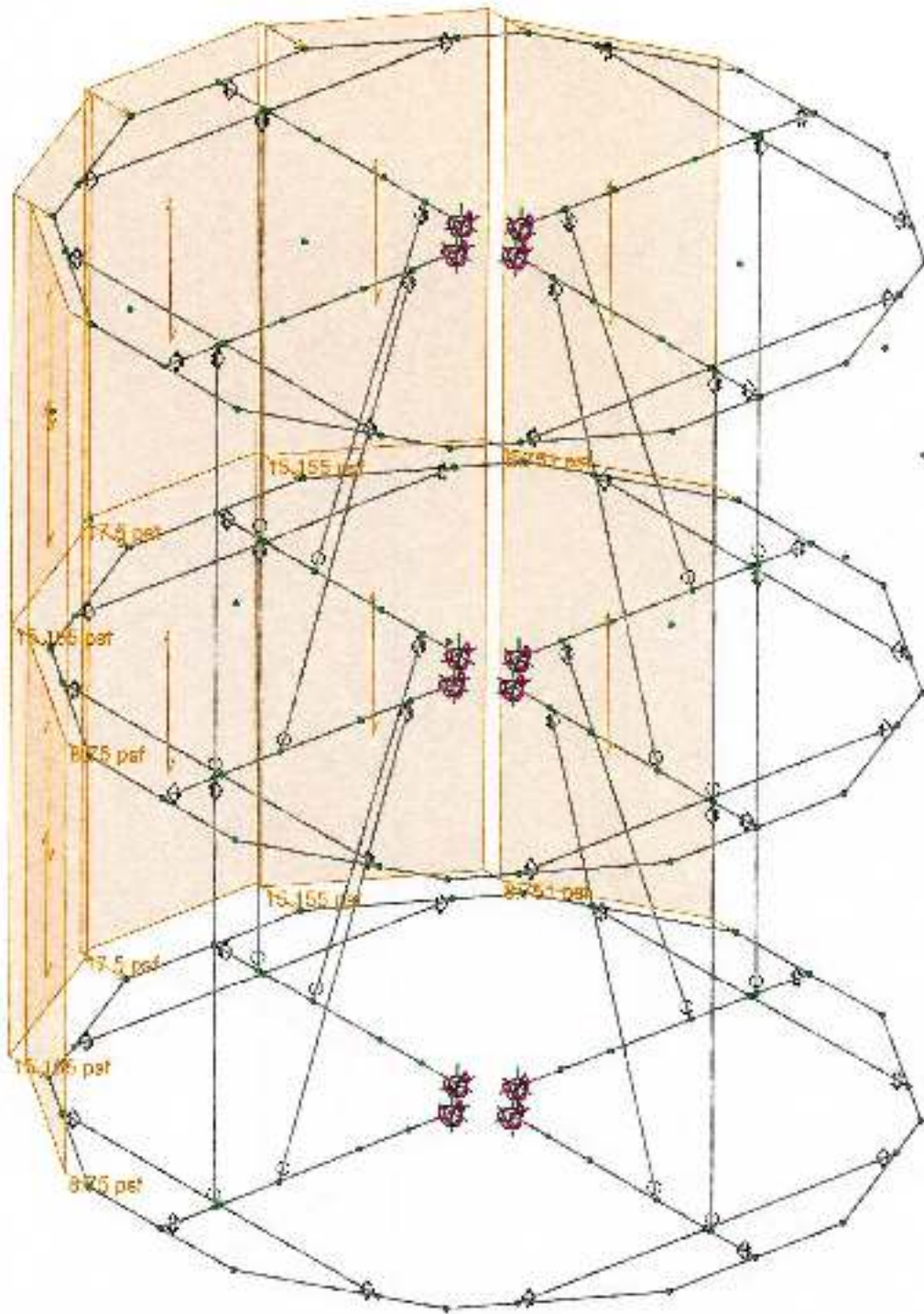
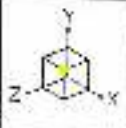


Section Sets	
<span style="color: blue;">█</span>	FRP Kicker Brace
<span style="color: green;">█</span>	FRP Vertical Brace
<span style="color: orange;">█</span>	STEEL Outrigger Weldment
<span style="color: grey;">█</span>	STEEL Radius Ring Assembly
<span style="color: pink;">█</span>	STEEL Radius Ring Assembly Top
<span style="color: cyan;">█</span>	STEEL Stand Ct Arm
<span style="color: brown;">█</span>	STEEL Stand Ct Arm Inner



Vector SE

SK-3  
 Oct 24, 2024 at 10:53 AM  
 NM1-148 Spike Concoalmen...



Loads: BLC 2, WLX

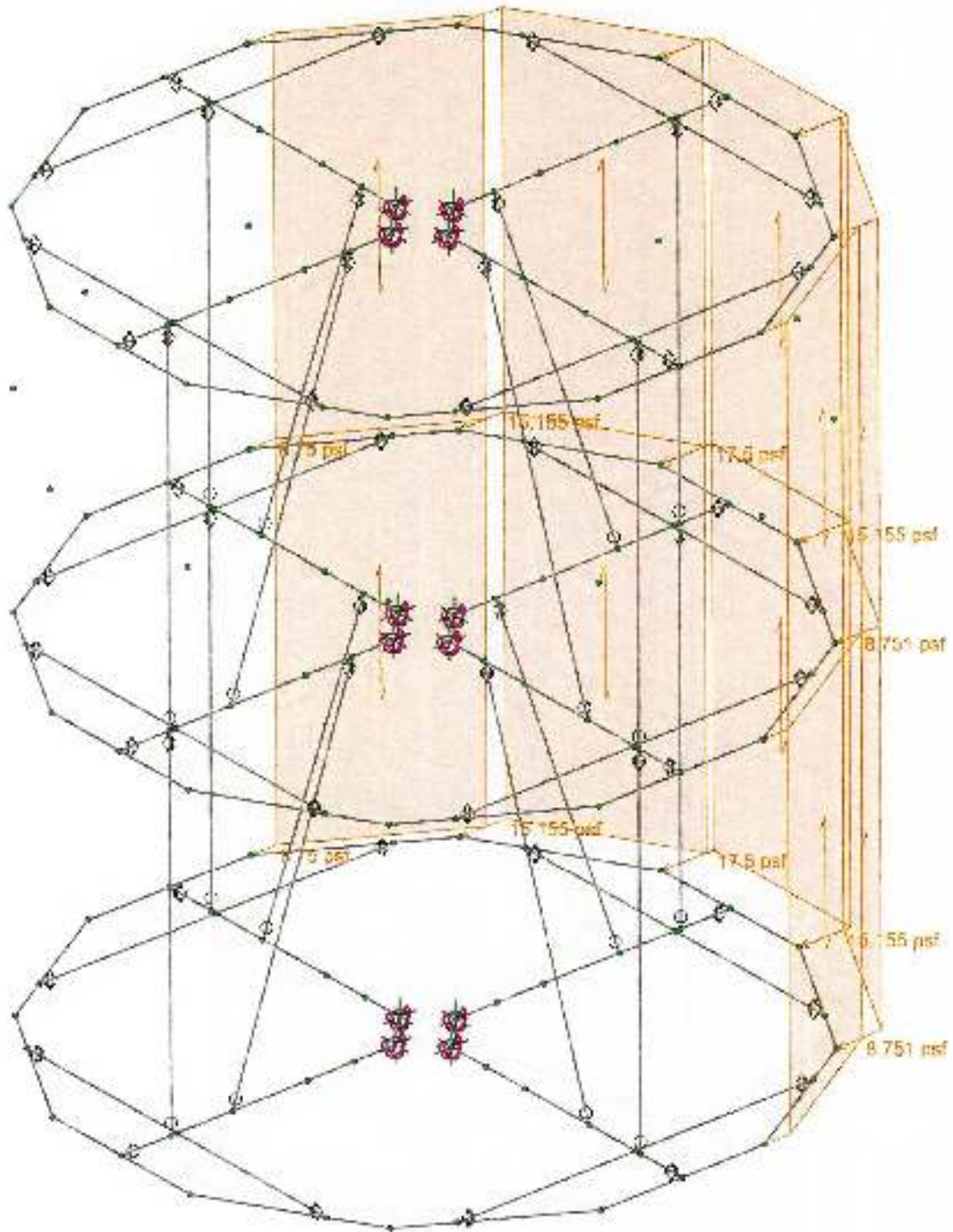
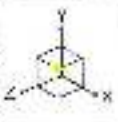


Vector SE

SK-1

Oct 24, 2024 at 10:53 AM

NM1-145 Spike Corroalmen

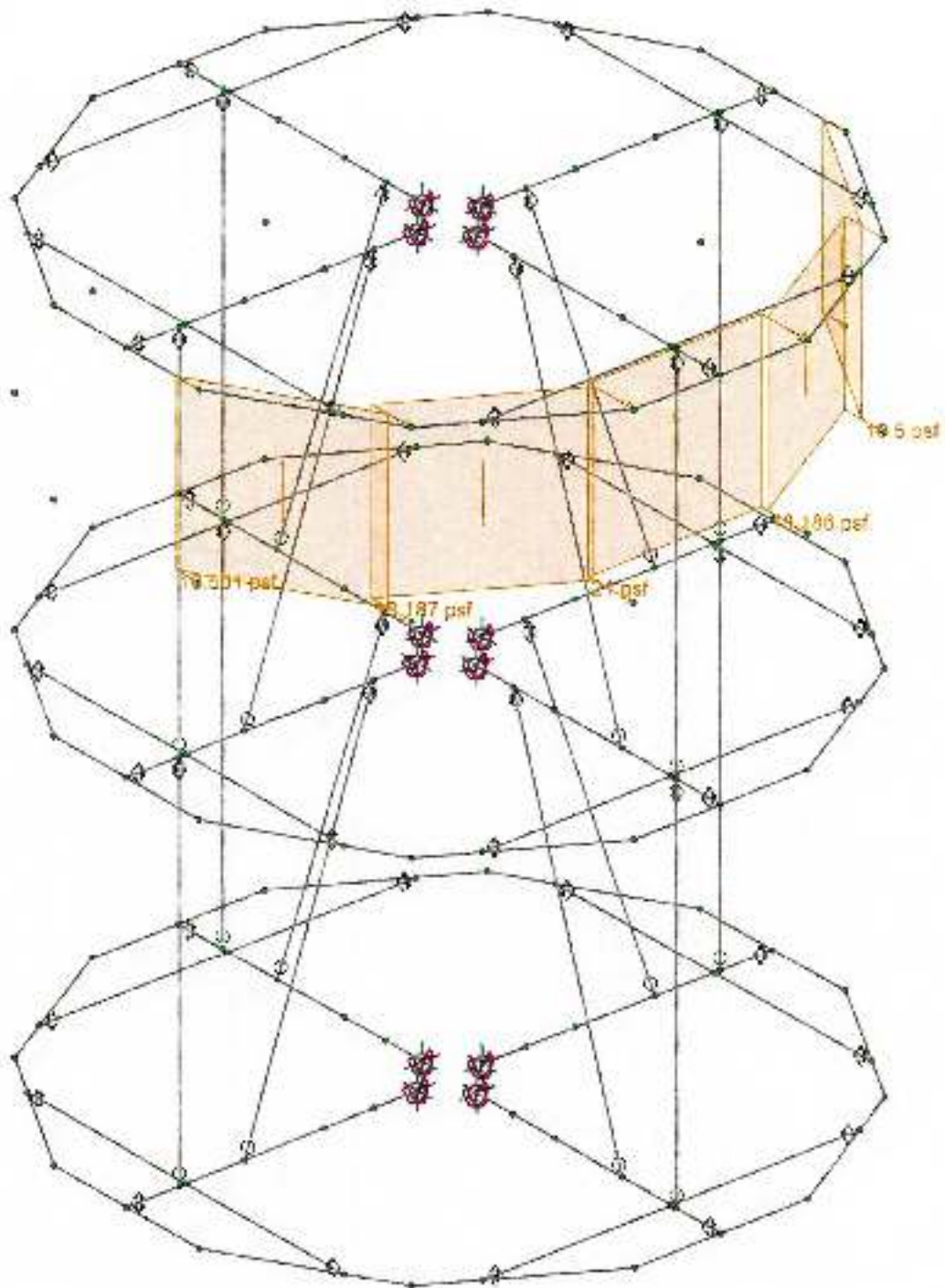


Loads: BLC 2 WLZ



Vector RE

SK-5  
Oct 24, 2024 at 10:53 AM  
NM1-148 Spike Conocalmen



Loads: BLD 4, WLX Inside

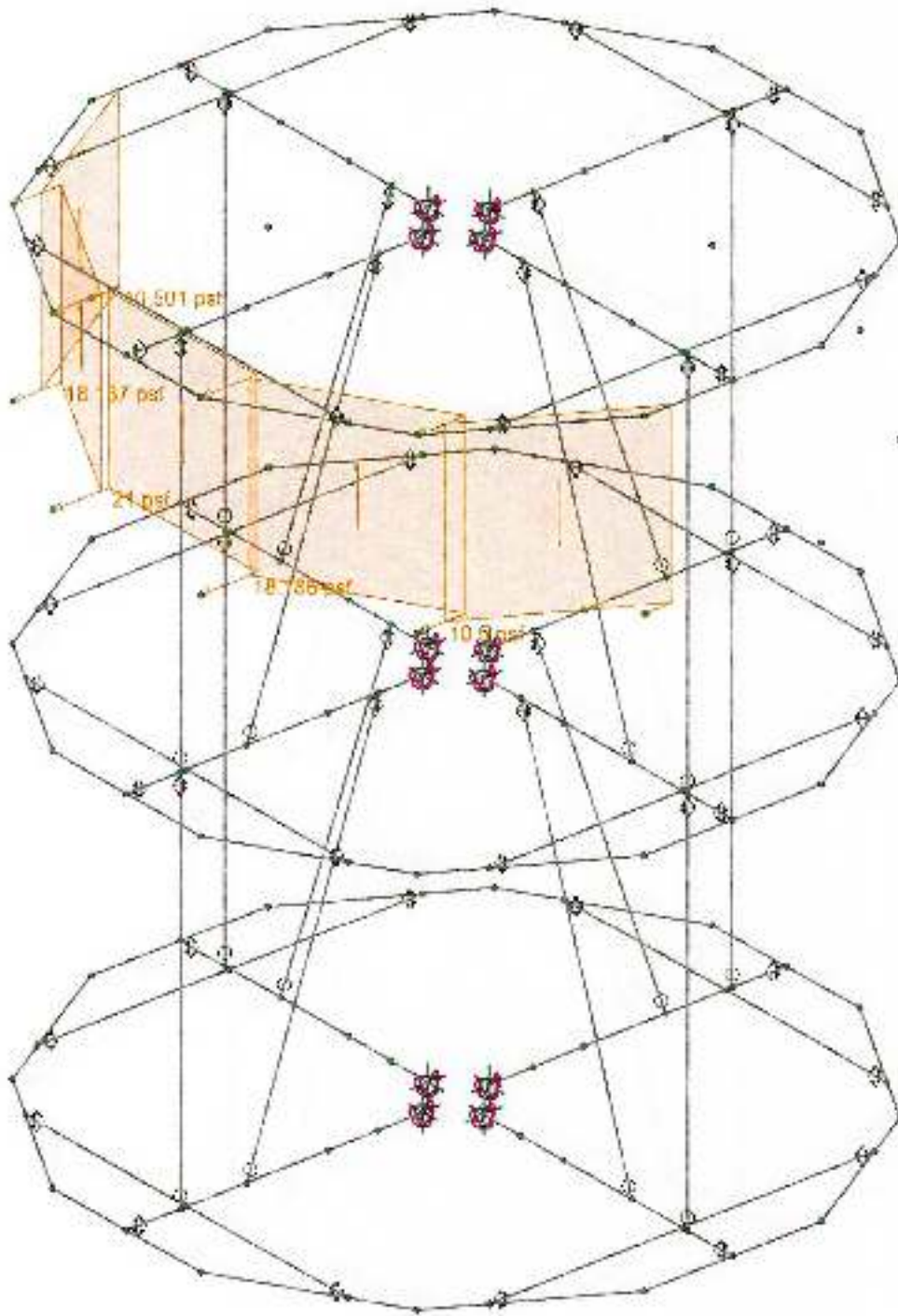


Vector SE

SK-R

Oct 24, 2024 at 10:54 AM

NM1-148 Spike Concealmen...



Loads: BLC 5, WLZ Inside

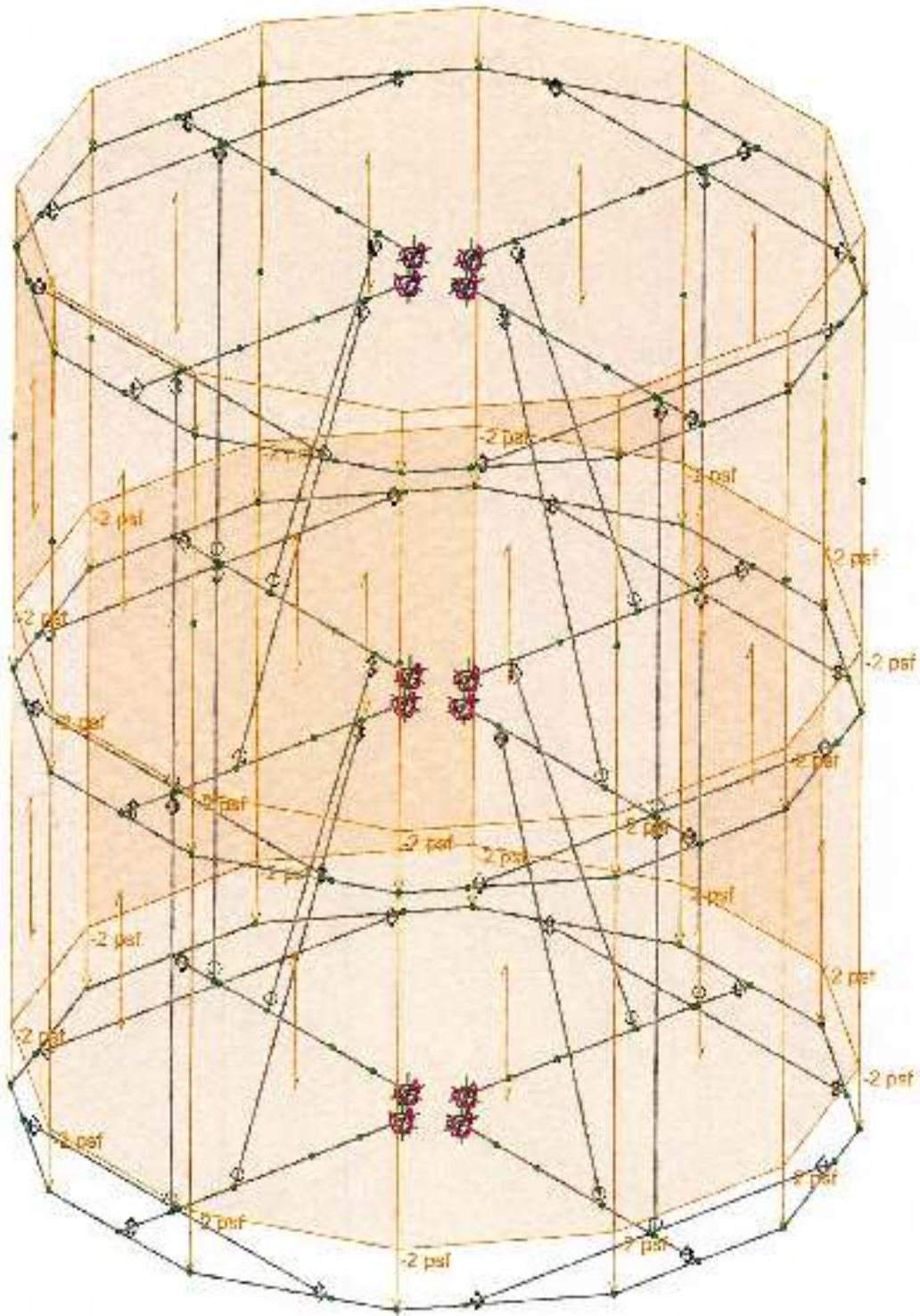
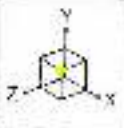


Vector SE

BK 7

Oct 24, 2024 at 10:54 AM

NM1-148 Spike Concreme1...



Loads: BLC 5, Panels

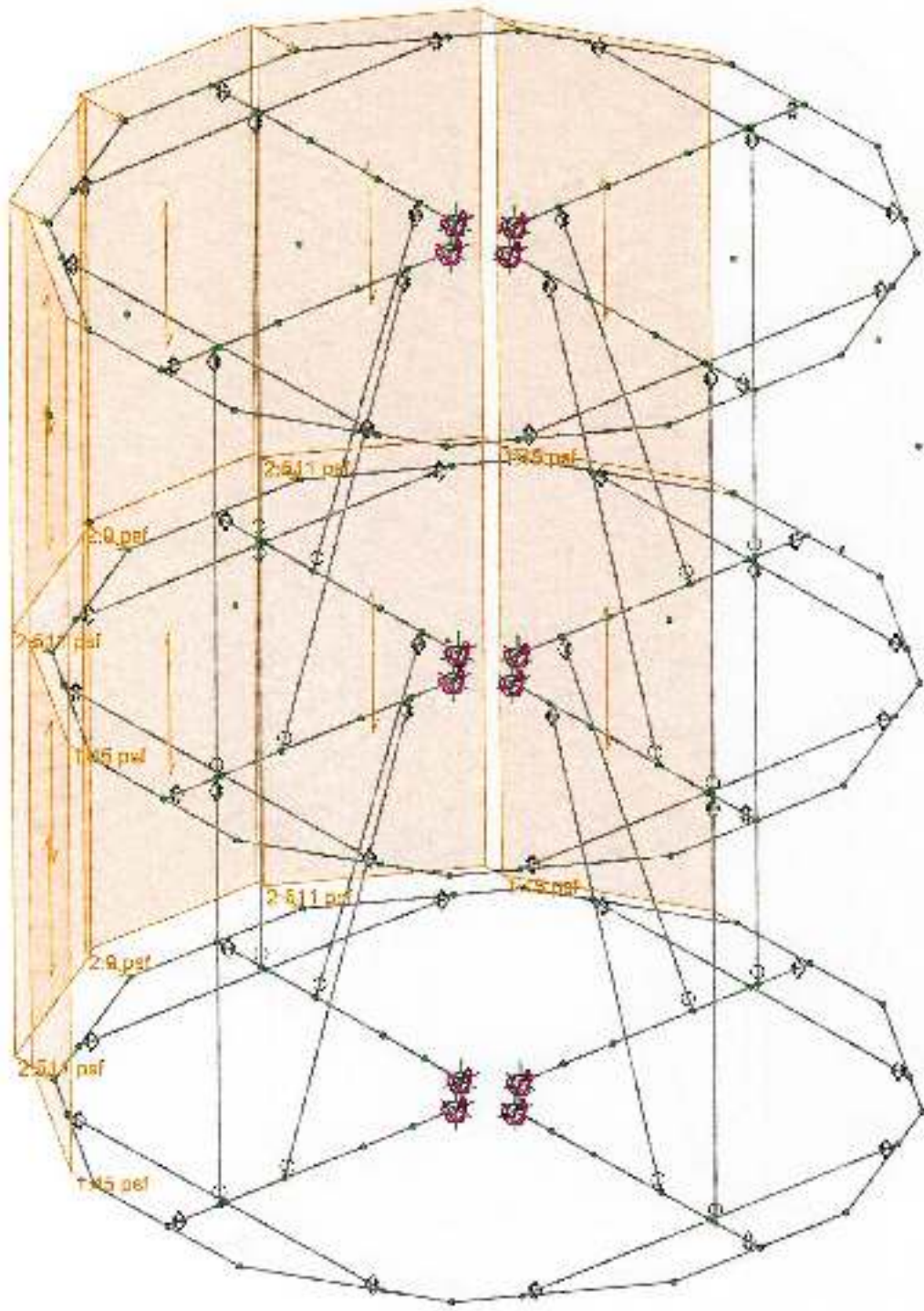


Vector SF

SK-3

Oct 24, 2024 9:10:54 AM

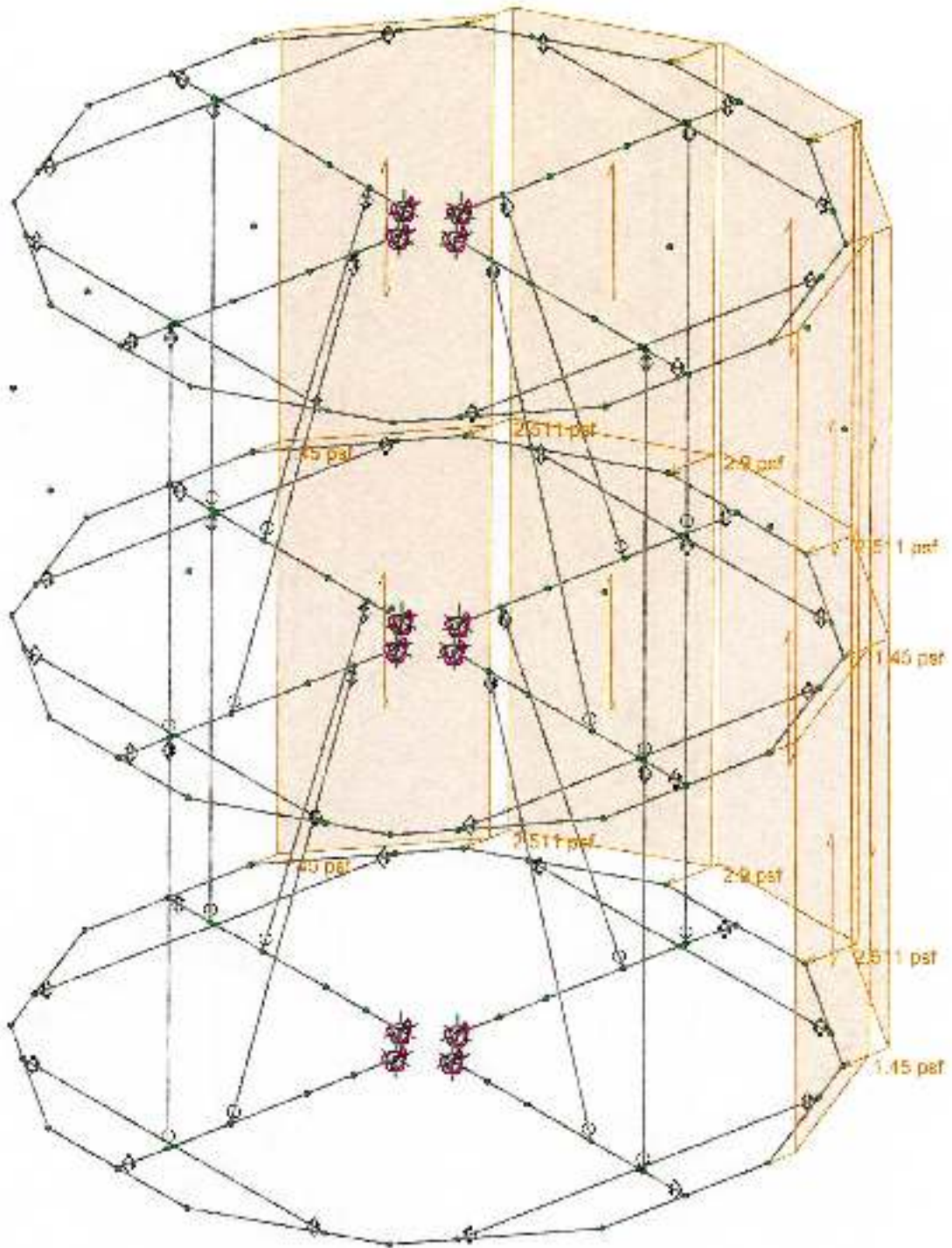
NW1-148 Spike Concealmen...



Loops: BLC 8, WLX Ice

**IRISA** Vector SE

SK-8  
Dec 24, 2024 at 10:54 AM  
NM1-148 Spike Concentration



Loads: RLC 9, W, Z Ice

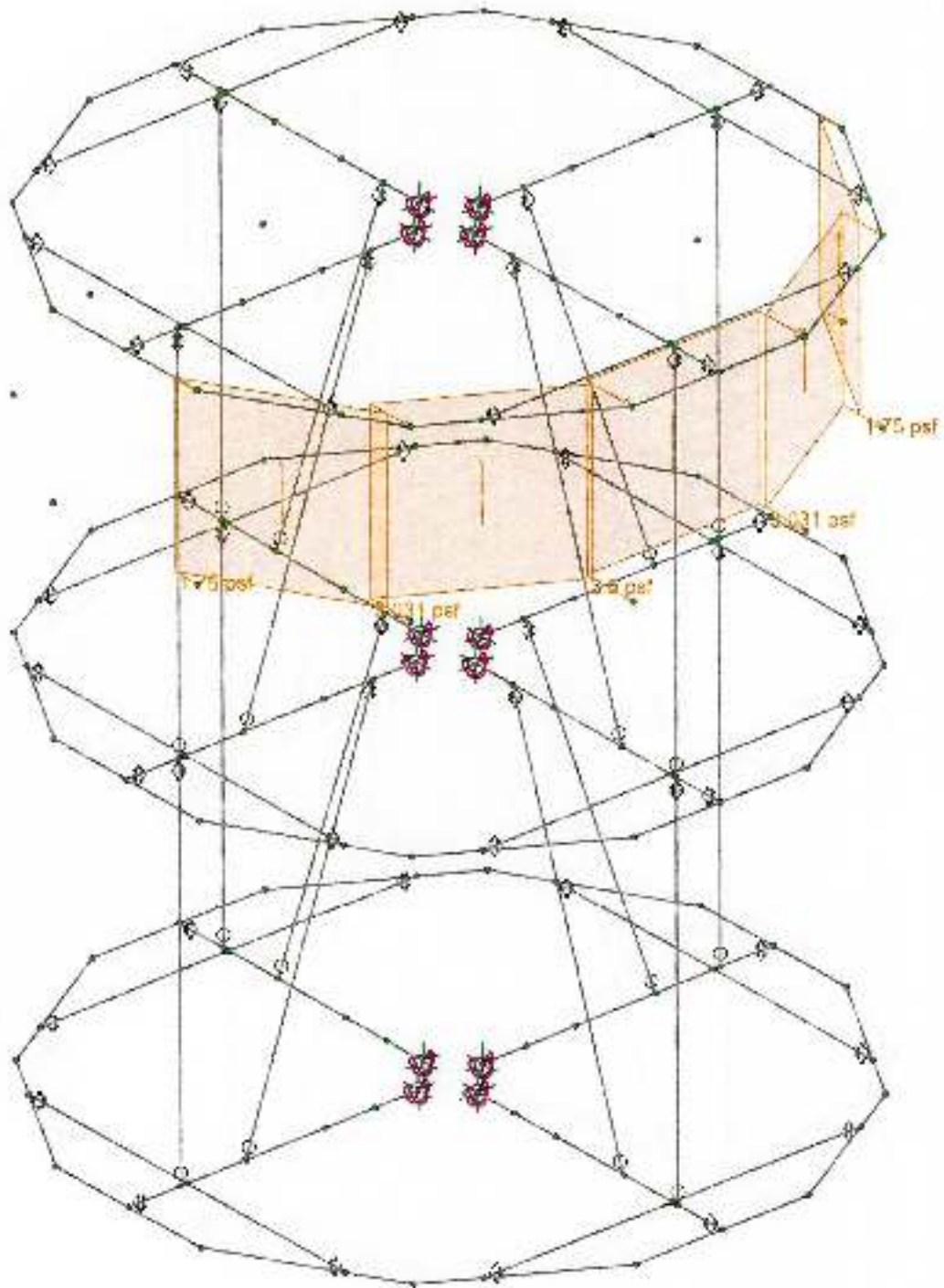
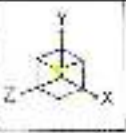


Vector SE

SK-10

Oct 24, 2024 at 10:54 AM

NM1-148 Spike Corrosalmon



Loads: BLC 10, WLX, loc inside

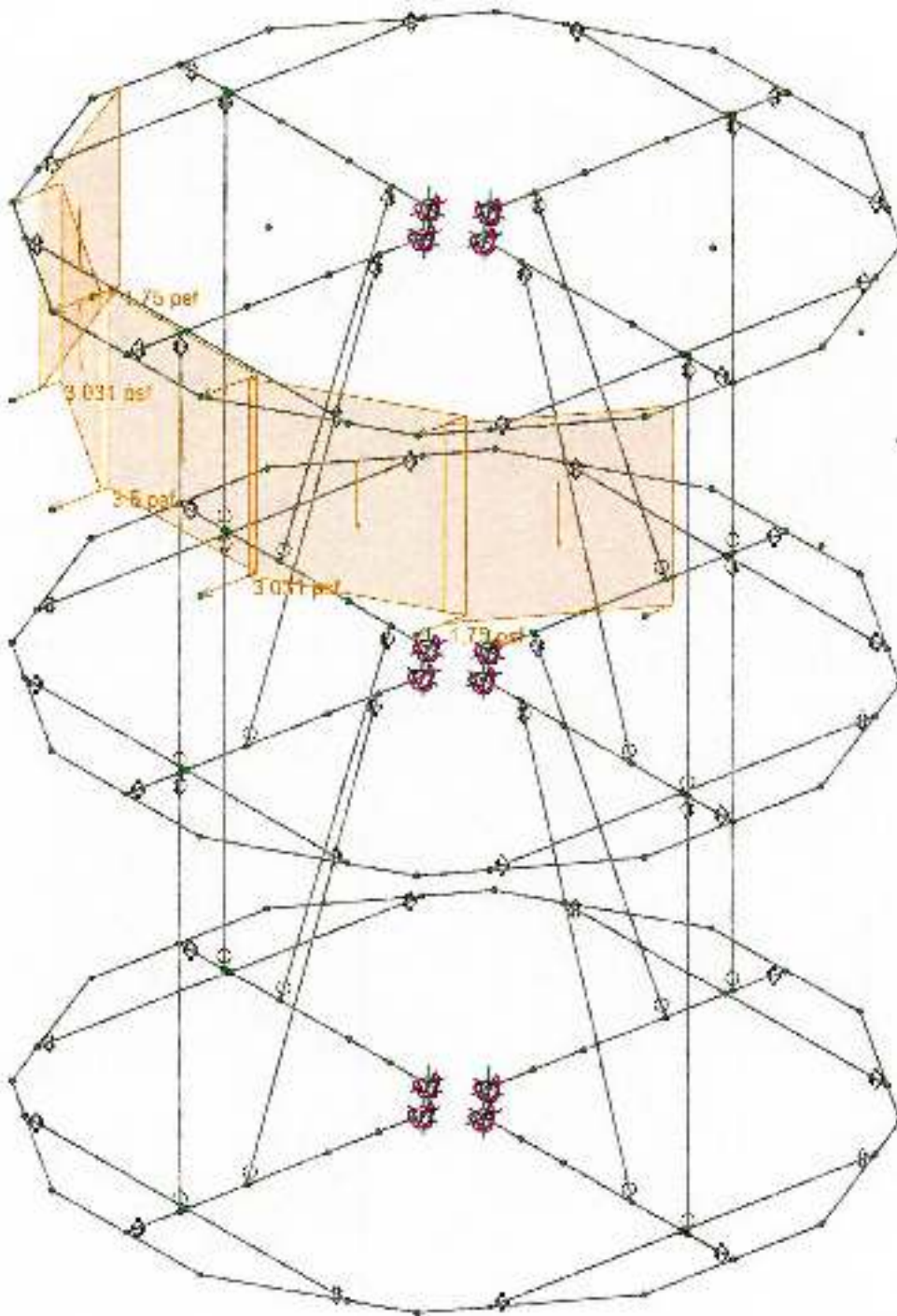
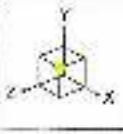


Vector 8F

SK-11

Oct 24, 2024 at 10:54 AM

NM1-148 Spike Concealmer



Load: B\_C 11, WLZ Ice inside

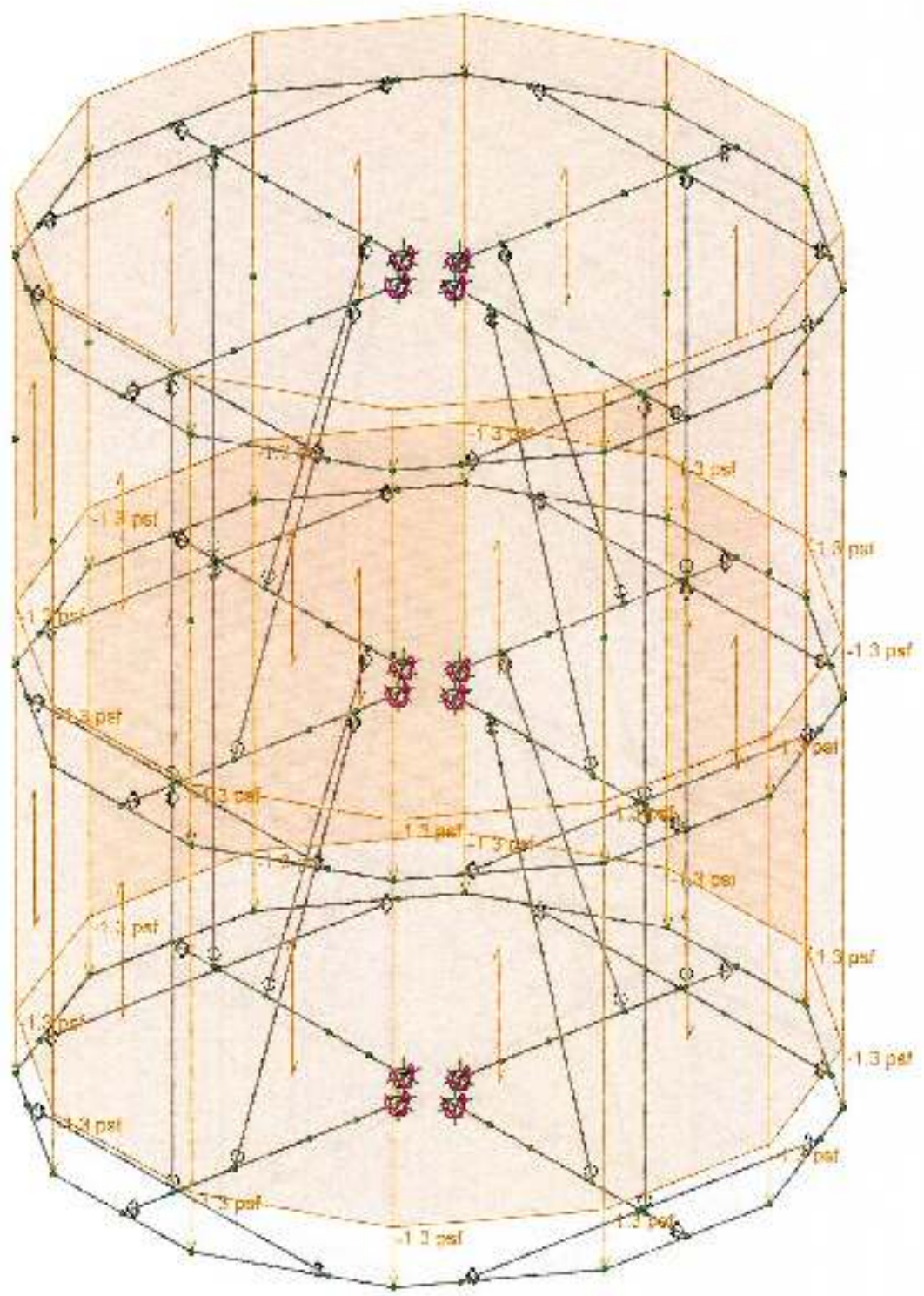


Vector SE

SK-12

Oct 24, 2024 at 10:54 AM

NM1-148 Spke Conces me1



Loads: BLC 12: Ice Weigh1

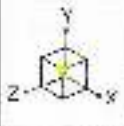


Vector SE

SK-13

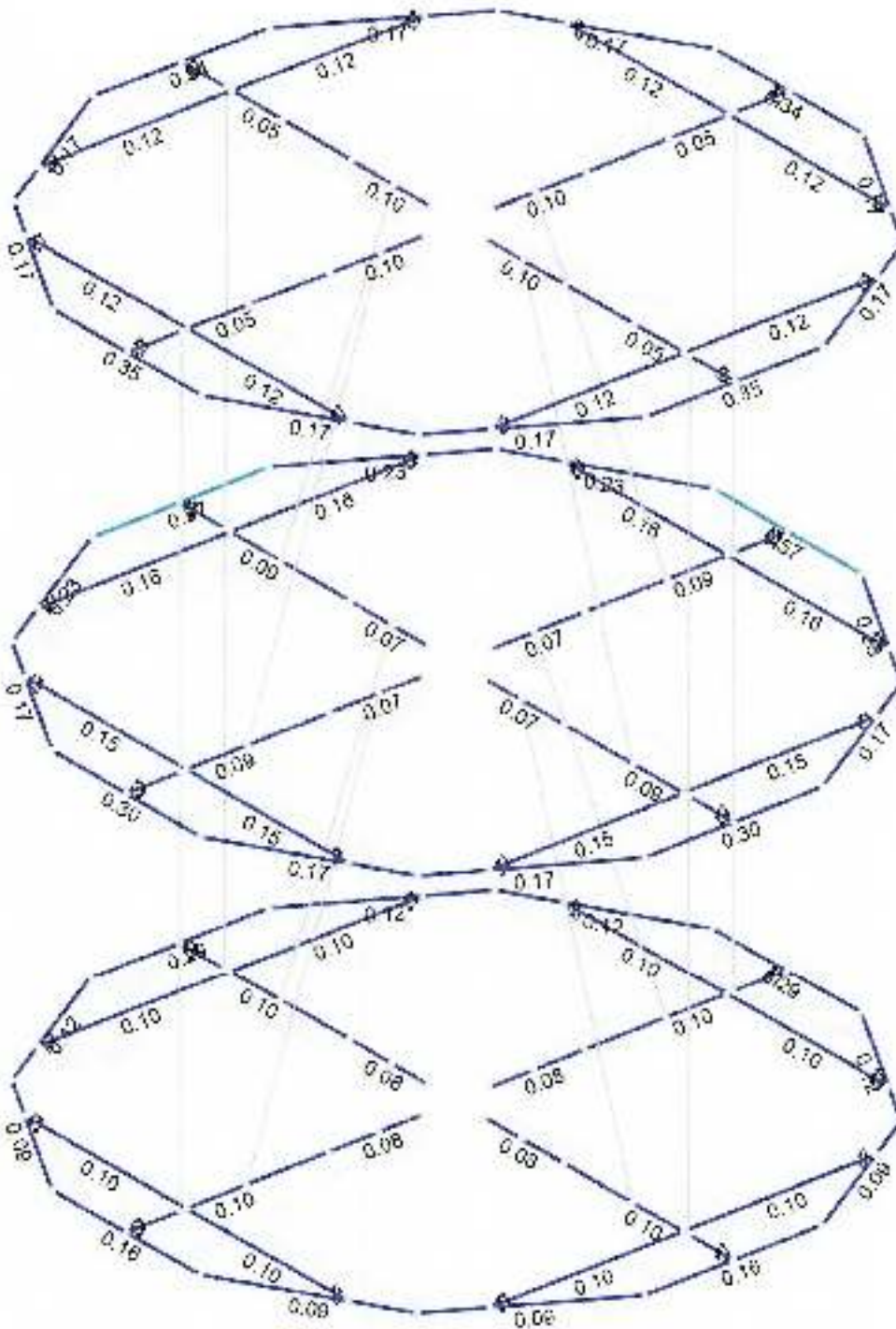
Oct 24 2024 at 10:54 AM

NM1-148 Spike Conicalmen...



Code Check (Env)

- No Calc
- > 1.0
- .90-1.0
- .75-.90
- .50-.75
- 0 - .50



Member Code Checks Displayed (Enveloped):

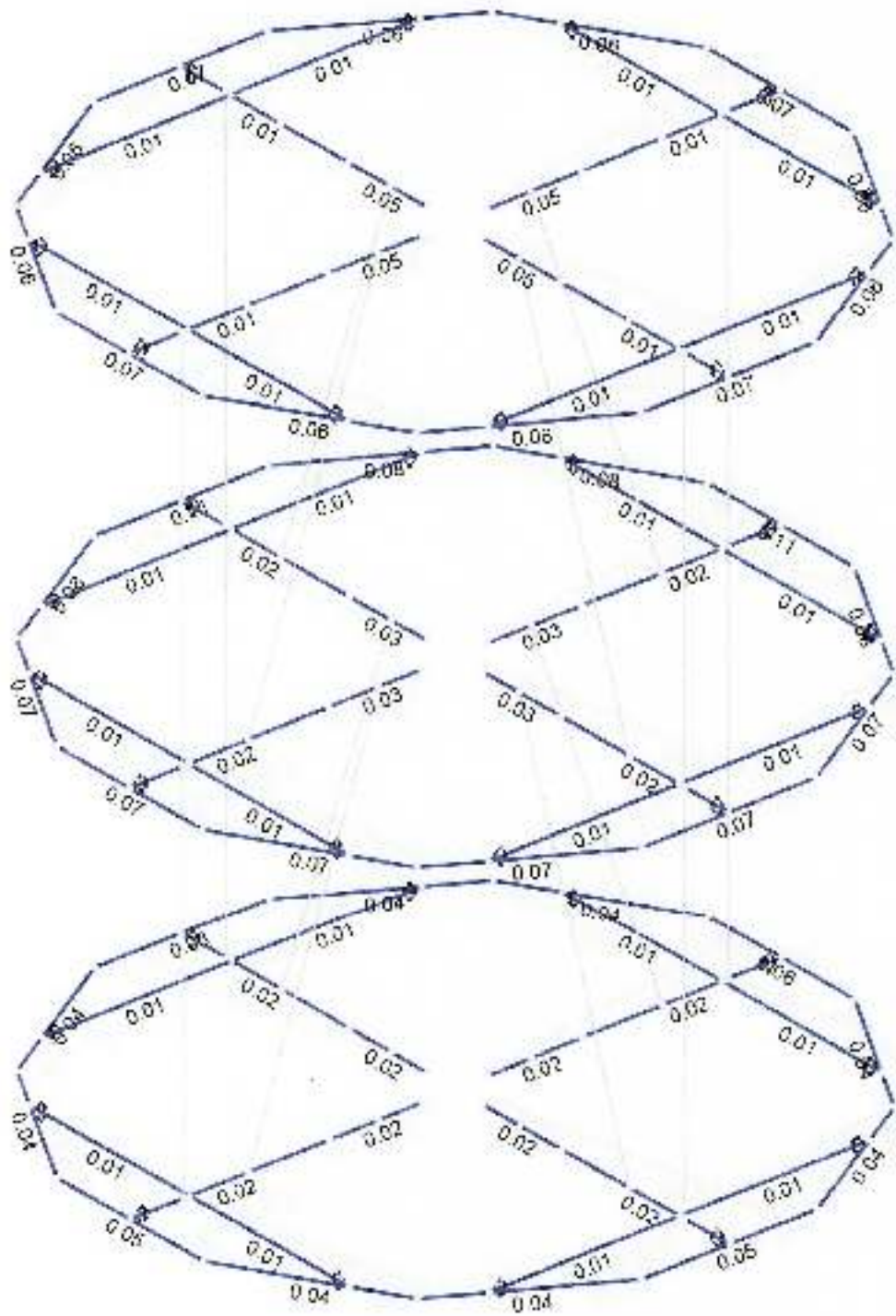
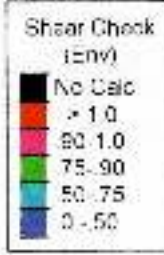
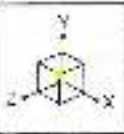


Vector BE

SK-14

Oct 24, 2024 at 10:54 AM

NM-148 Spoke Corralmen...



Member Shear Checks (Displayed - Enveloped)

<b>IRISA</b>	Vector SF

SK-15
Oct 24, 2024 at 10:55 AM
NM1-148 Spike Concealmen...



Company : Vector SF  
 Designer  
 Job Number  
 Model Name :

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 10/24/2024  
 10:55:17 AM  
 Checked By :

**Model Settings**

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in)	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes
Approximate Mesh Size (in)	24
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3
Single	No
Multiple (Optimum)	No
Maximum	Yes

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes
Default Global Plane for z-axis	XZ
Plate Local Axis Orientation	Global

Hot Rolled Steel	AISC 15.1 (360-16) LRFD
Stiffness Adjustment	Yes (Iterative)
Notional Annex	None
Connections	None
Cold Formed Steel	None
Stiffness Adjustment	Yes (Iterative)
Wood	None
Temperature	< 100F
Concrete	None
Masonry	None
Aluminum	None
Structure Type	Building
Stiffness Adjustment	Yes (Iterative)
Stainless	None
Stiffness Adjustment	Yes (Iterative)

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar apices (2"d bar spacing)	No
List forces which were ignored for design in the Detail Report	Yes

Column Min Steel	1
Column Max Steel	8
Rebar Material Spec	ASTM A513
Warn if beam-column framing arrangement is not understood	No
Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Code	ASCE 7-15
Risk Category	For II
Drift Cat	Other



Company : Vector SF  
 Designer :  
 Job Number :  
 Model Name :

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 10/24/2024  
 10:55:17 AM  
 Checked By :

**Hot Rolled Steel Properties**

	Label	F [ksi]	G [ksi]	Nu	Therm. Coeff. [1e-6/F-1]	Density [kN/m³]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.26	29000	11164	0.3	0.65	0.49	36	1.5	58	1.2
2	A500 Gr.B RECT	29000	11164	0.3	0.65	0.527	45	1.4	58	1.3
3	A500 Gr.B RND	29000	11164	0.3	0.65	0.527	42	1.4	58	1.3
4	FRP	2500	450	0.3	0.65	0.11	10	1.2	30	1.1

**Hot Rolled Steel Section Sets**

	Label	Shape	Type	Design List	Material	Design Rule	Area [in²]	Iyy [in⁴]	Izz [in⁴]	J [in⁶]
1	FRP Kicker Brace	LL4X4X8W4'GAP	MBrace	None	FRP	Typical	5.719	65.042	6.717	0.251
2	FRP Vertical Brace	.L4X4X8W4'GAP	MBrace	None	FRP	Typical	5.719	65.042	6.717	0.251
3	STEEL Outrigger Weldment	HSS4X2X3	Beam	None	A500 Gr.B RECT	Typical	1.89	1.22	3.66	3.08
4	STEEL Radius Ring Assembly	9X4X5/16"	Beam	None	A36 Gr.26	Typical	2.429	11.423	2.887	0.028
5	STEEL Radius Ring Assembly Top	L4X4X4	Beam	None	A36 Gr.26	Typical	1.93	3	3	0.044
6	STEEL Stand Off Arm	HSS5X5X3	Beam	None	A500 Gr.B RECT	Typical	3.26	12.5	12.5	19.9
7	STEEL Stand Off Arm Inner	HSS4.5X4.5X6	Beam	None	A500 Gr.B RECT	Typical	5.48	15.5	15.3	25.7

**Load Combinations**

	Description	Solve	P Delta	BLC	Factor	RLC	Factor	BLC	Factor
1	1.0D	Yes	Y	DL	1				
2	1.4D	Yes	Y	DL	1.4				
3	1.2D+1.6L	Yes	Y	DL	1.2	LL	1.6		
4	1.2D + 0.5LL + 1.0WLx	Yes	Y	DL	1.2	LL	0.5	WLX	1
5	1.2D + 0.5LL + 1.0WLz	Yes	Y	DL	1.2	LL	0.5	WLZ	1
6	1.2D + 0.5LL - 1.0WLx	Yes	Y	DL	1.2	LL	0.5	WLX	-1
7	1.2D + 0.5LL - 1.0WLz	Yes	Y	DL	1.2	LL	0.5	WLZ	-1
8	1.2D + 1.0WLx	Yes	Y	DL	1.2	WLX	1		
9	1.2D + 1.0WLz	Yes	Y	DL	1.2	WLZ	1		
10	1.2D - 1.0WLx	Yes	Y	DL	1.2	WLX	-1		
11	1.2D - 1.0WLz	Yes	Y	DL	1.2	WLZ	-1		
12	0.9D + 1.0WLx	Yes	Y	DL	0.9	WLX	1		
13	0.9D + 1.0WLz	Yes	Y	DL	0.9	WLZ	1		
14	0.9D - 1.0WLx	Yes	Y	DL	0.9	WLX	-1		
15	0.9D - 1.0WLz	Yes	Y	DL	0.9	WLZ	-1		
16	1.2D + 1.0Di + 1.0Wi	Yes	Y	DL	1.2	OL1	1	OL2	1
17	1.2D + 1.0Di + 1.0Wz	Yes	Y	DL	1.2	OL1	1	OL3	1
18	1.2D + 1.0Di - 1.0Wi	Yes	Y	DL	1.2	OL1	1	OL2	-1
19	1.2D + 1.0Di - 1.0Wz	Yes	Y	DL	1.2	OL1	1	OL3	-1

**Envelope Maximum Member Section Forces**

Member	Axial [lb]	Loc [ft]	Cy Shear [lb]	Loc [ft]	Cz Shear [lb]	Loc [ft]	LC Torsion [lb-ft]	Loc [ft]	Cy y Moment [lb-ft]	Loc [ft]	Cz z Moment [lb-ft]	Loc [ft]
1 M96	max-1414.201	0	14	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
2	min-2352.771	10.5919	-11.722	10.592	0	0	1	0	0	1	-31.034	5.2952
3 M94	max-1418.207	0	12	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
4	min-2361.772	10.5919	-11.722	10.592	0	0	1	0	0	1	-31.034	5.2952
5 M93	max-1418.207	0	13	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
6	min-2361.772	10.5919	-11.722	10.592	0	0	1	0	0	1	-31.034	5.2952
7 M95	max-1414.201	0	15	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
8	min-2362.771	10.5919	-11.722	10.592	0	0	1	0	0	1	-31.034	5.2952
9 M48	max-1445.854	0	14	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
10	min-2384.567	10.5919	-11.722	10.592	0	0	1	0	0	1	-31.034	5.2952
11 M47	max-1445.854	0	15	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
12	min-2384.567	10.5919	-11.722	10.592	0	0	1	0	0	1	-31.034	5.2952



**Envelope Maximum Member Section Forces (Continued)**

Member	Axial [lb]	Loz [lb]	Col Shear [lb]	End [lb]	Loz Shear [lb]	Loz [lb]	Col Torque [lb-ft]	End Torque [lb-ft]	Col y Moment [lb-ft]	Loz y Moment [lb-ft]	Loz z Moment [lb-ft]	End z Moment [lb-ft]						
13 M40	max 1449.261	0	12	11.722	0	2	0	10.5919	0	10.5919	0	10.5919						
14	min 2383.898	10.5919	8	-11.722	10.5919	2	0	0	0	0	0	1	-31.034	5.2952				
15 M45	max 1449.261	0	13	11.722	0	2	0	10.5919	0	10.5919	0	10.5919						
16	min -2383.898	10.5919	8	-11.722	10.5919	2	0	0	0	0	0	1	-31.034	5.2952				
17 M89	max 905.681	0	19	0	10	19	0	10	19	0	10	19	0	10	19			
18	min 501.605	10	15	0	0	1	0	0	0	0	0	1	0	0	1			
19 M90	max 905.681	0	18	0	10	19	0	10	19	0	10	19	0	10	19			
20	min 501.605	10	12	0	0	1	0	0	0	0	0	1	0	0	1			
21 M91	max 906.079	0	17	0	10	19	0	10	19	0	10	19	0	10	19			
22	min 499.864	10	15	0	0	1	0	0	0	0	0	1	0	0	1			
23 M42	max 1083.508	0	19	0	10	19	0	10	19	0	10	19	0	10	19			
24	min 540.87	10	13	0	0	1	0	0	0	0	0	1	0	0	1			
25 M41	max 1083.508	0	19	0	10	19	0	10	19	0	10	19	0	10	19			
26	min 540.87	10	13	0	0	1	0	0	0	0	0	1	0	0	1			
27 M44	max 1083.507	0	19	0	10	19	0	10	19	0	10	19	0	10	19			
28	min 640.958	10	14	0	0	1	0	0	0	0	0	1	0	0	1			
29 M92	max 905.079	0	16	0	10	19	0	10	19	0	10	19	0	10	19			
30	min 499.864	10	15	0	0	1	0	0	0	0	0	1	0	0	1			
31 M43	max 1083.507	0	17	0	10	19	0	10	19	0	10	19	0	10	19			
32	min 540.868	10	15	0	0	1	0	0	0	0	0	1	0	0	1			
33 M31	max 1072.307	4.6591	10	425.526	1.5041	2	104.12	4.6591	19	709	1.4581	19	65.031	4.6591	19	-492.438	4.6110	
34	min -1059.54	4.6591	12	-407.959	1.5041	6	-45.95	1.5041	16	11.031	1.5041	13	-73.855	0	18	-486.454	4.6112	
35 M77	max 471.748	4.6591	11	474.091	2.2811	11	130.859	2.3291	17	11.71	4.6591	17	267.953	2.3291	17	613.707	2.3291	
36	min -449.358	2.3291	13	-475.853	2.3291	7	-131.021	2.3291	17	11.742	0	16	25.126	0	14	-628.636	2.3291	
37 M78	max 545.708	0	11	205.188	3.1541	3	30.017	3.1541	7	-6.659	3.1541	5	42.484	0	17	248.948	0.0491	
38	min -521.659	0	13	-201.678	3.1541	3	-82.515	0	19	-11.039	0	17	-41.099	4.6591	15	-241.279	0.0491	
39 M76	max 545.758	4.6591	11	201.859	1.5041	3	62.514	4.6591	18	11.053	4.6591	15	42.628	4.6591	15	248.914	4.6111	
40	min -521.651	4.6591	13	-205.167	1.5041	3	-30.012	1.5041	19	6.607	0	14	-41.239	0	16	-241.247	4.5613	
41 M75	max 599.936	3.1541	9	127.066	4.6591	4	30.011	3.1541	7	-6.659	4.6591	14	42.578	0	16	179.503	0	9
42	min -575.737	0	14	-130.845	3.2031	4	-62.509	0	19	-11.045	0	13	-41.241	4.6591	15	-171.773	0	14
43 M79	max 545.758	4.6591	11	201.859	1.5041	3	62.512	4.6591	19	11.01	4.6591	15	42.49	4.6591	15	248.914	4.6110	
44	min -521.651	4.6591	13	-205.167	1.5041	3	-30.012	1.5041	19	6.659	1.5041	14	-41.099	0	17	-241.247	4.5612	
45 M36	max 1180.933	3.1541	9	258.237	4.6591	4	48.928	3.1541	19	-10.558	3.1541	14	69.514	0	18	353.366	0	9
46	min -1186.378	0	15	-258.014	3.2031	5	-104.087	0	16	-19.946	0	16	-74.426	4.6591	17	-347.814	0	15
47 M35	max 1127.185	2.3291	8	410.613	2.2811	9	214.421	2.2811	19	17.487	4.6591	18	443.316	2.3291	18	592.959	2.3291	
48	min -1112.849	0	14	-110.625	2.3291	5	-216.745	2.3291	19	-17.455	0	17	37.464	4.6591	14	-603.146	2.3291	
49 M34	max 1161.031	4.6591	9	258.942	1.4581	9	104.06	4.6591	18	19.934	4.6591	17	60.437	4.6591	17	353.337	4.6591	
50	min -1186.092	1.5041	7	-256.251	0	15	-48.902	1.5041	16	10.6	0	15	-74.426	0	17	-347.772	4.6591	
51 M33	max 1072.331	0	10	406	3.1541	10	46.968	3.1541	16	-10.558	4.6591	15	69.514	0	17	492.507	0.0491	
52	min -1059.591	0	12	-405.573	3.1541	2	-104.124	0	18	-19.946	0	17	-74.422	4.6591	17	-486.575	0.0491	
53 M32	max 925.705	4.6591	9	942.911	2.3291	2	214.037	2.2811	16	17.487	4.6591	17	443.891	2.3291	16	1235.293	2.3291	
54	min -912.475	2.3291	12	-950.439	2.3291	5	-216.352	2.3291	16	-17.374	0	19	37.464	4.6591	13	-1248.78	2.3291	
55 M30	max 1072.331	0	11	406	3.1541	11	46.968	3.1541	17	-11.03	3.1541	2	69.023	0	18	492.507	0.0491	
56	min -1059.591	0	13	-405.573	3.1541	3	-104.124	0	19	-19.792	3.2031	8	-73.96	4.6591	11	-486.575	0.0491	
57 M25	max 1127.185	2.3291	8	410.613	2.2811	8	215.926	2.3291	19	17.485	4.6591	16	443.316	2.3291	18	592.959	2.3291	
58	min -1112.846	0	14	-110.626	2.3291	4	-216.745	2.3291	18	-17.487	0	17	37.469	0	19	-603.146	2.3291	
59 M28	max 1072.307	4.6591	11	405.526	1.5041	3	104.12	4.6591	19	19.948	1.4581	15	69.523	4.6591	16	482.438	4.6111	
60	min -1059.54	4.6591	13	-407.959	1.5041	3	-45.95	1.5041	17	10.559	1.5041	14	-74.422	0	16	-486.454	4.6113	
61 M29	max 925.705	4.6591	11	942.911	2.3291	3	215.926	2.3291	16	17.375	4.6591	18	443.891	2.3291	17	1235.293	2.3291	
62	min -912.473	2.3291	13	-950.439	2.3291	7	-216.352	2.3291	17	-17.487	0	16	37.468	0	14	-1248.78	2.3291	
63 M54	max 599.936	3.1541	9	127.066	4.6591	3	30.018	3.1541	7	-6.605	4.6591	14	42.622	0	16	179.503	0	9
64	min -575.737	0	15	-130.845	3.2031	5	-62.517	0	18	-11.052	3.2031	16	-41.241	4.6591	17	-171.773	0	15
65 M83	max 572.347	2.3291	9	208.825	2.2811	9	129.698	2.2811	19	11.742	4.6591	18	266.031	2.3291	19	292.357	2.3291	
66	min -549.593	0	15	-209.837	2.3291	5	-131.124	2.3291	19	-11.725	0	17	35.123	4.6591	14	-306.563	2.3291	
67 M82	max 599.964	4.6591	9	130.85	1.4581	9	62.508	4.6591	18	11.045	4.6591	17	42.583	4.6591	17	179.477	4.6591	

**Envelope Maximum Member Section Forces (Continued)**

Member	Axial [k]	Loc [ft]	Loc-y	Shear [k]	Loc [ft]	Loc-z	Shear [k]	Loc [ft]	Loc-z	Torque [k-ft]	Loc [ft]	Loc-y	Moment [k-ft]	Loc [ft]	Loc-z	Moment [k-ft]	Loc [ft]	Loc-z	
68	min	-575.769	1.504	0	-127.073	0	15	-30.008	1.504	6.531	0	15	-41.241	0	17	-171.752	4.658	15	
69	M73	max	599.951	4.558	8	130.85	4.658	8	52.514	4.658	17	11.053	1.456	17	42.629	4.658	17	179.477	4.658
70	min	-575.769	1.504	0	-127.073	0	15	-30.013	1.504	6.507	0	15	-41.241	0	15	171.752	4.658	14	
71	M80	max	471.748	4.659	10	474.391	2.281	10	129.595	2.281	16	11.742	4.659	17	267.953	2.329	16	613.707	2.329
72	min	-449.358	2.329	12	-478.653	2.329	6	-131.221	2.329	-17.71	0	13	25.123	4.659	15	-628.635	2.329	6	
73	M25	max	1181.031	4.658	8	256.942	1.456	8	104.083	1.456	17	19.948	4.658	17	89.523	4.658	17	353.237	4.658
74	min	-1166.092	1.504	0	-256.251	0	14	-46.32	1.504	10.558	0	15	-74.426	0	18	-347.772	4.658	14	
75	M74	max	572.347	2.329	8	208.825	2.281	8	130.858	2.329	16	11.725	4.659	15	263.061	2.329	16	292.337	2.329
76	min	-549.593	0	14	-208.837	2.329	4	-131.124	2.329	-17.742	0	17	25.125	0	16	-306.963	2.329	4	
77	M27	max	1180.933	3.154	8	256.237	4.658	14	46.911	3.154	17	-10.599	3.154	14	69.429	0	16	353.366	0
78	min	-1766.078	0	14	-255.817	3.203	4	-104.064	0	18	-19.932	0	16	-74.426	4.658	16	-347.814	0	
79	M51	max	545.768	0	10	205.188	3.154	10	30.018	3.154	10	-8.506	3.154	10	42.622	0	17	248.949	0.049
80	min	-521.559	0	12	-207.678	3.154	12	-32.517	0	17	-11.552	3.203	17	-41.239	4.658	17	-241.070	0.070	
81	M1	max	1161.402	4.658	8	69.213	4.658	16	306.015	1.504	12	16.22	1.456	16	320.076	4.658	9	263.337	4.658
82	min	-1261.695	4.658	14	-17.538	1.504	18	-329.222	1.504	7.945	1.504	14	-294.19	4.658	14	-342.409	4.658	5	
83	M2	max	1045.489	2.329	8	131.65	2.329	17	733.885	2.329	5	12.733	4.658	16	725.485	2.329	0	482.88	2.329
84	min	-970.538	0	14	-131.779	2.329	8	-729.272	2.281	4	-27.732	0	16	-599.268	2.329	2	901.106	2.329	
85	M3	max	1181.098	0	6	17.543	3.154	18	329.237	3.154	10	-7.945	3.154	10	320.12	0	5	263.379	0
86	min	-1261.658	0	14	-85.215	0	16	-306.041	3.154	2	-6.219	0	16	-254.213	0	14	-342.437	0	
87	M4	max	1165.957	4.658	11	89.194	4.658	19	297.906	1.504	16	16.226	1.456	19	316.268	4.658	11	259.369	4.658
88	min	-1088.154	4.658	3	-17.519	1.504	17	-321.113	1.504	7.925	0	3	-290.376	4.658	13	-338.136	4.658	5	
89	M5	max	1053.681	2.329	11	131.65	2.329	16	712.407	2.329	11	12.743	4.658	19	707.765	2.329	9	464.888	2.329
90	min	-378.645	0	13	-131.805	2.329	7	-708.227	2.281	7	-12.74	0	9	-581.491	2.329	15	-883.095	2.329	
91	M7	max	1155.957	4.658	10	89.194	4.658	18	297.906	1.504	14	16.225	1.456	18	316.208	4.658	10	259.369	4.658
92	min	-1065.164	4.658	12	-17.519	1.504	16	-321.113	1.504	7.925	0	12	-290.376	4.658	12	-338.438	4.658	4	
93	M8	max	1053.681	2.329	10	131.651	2.329	18	712.497	2.329	10	12.742	4.658	18	707.768	2.329	8	464.888	2.329
94	min	-878.646	0	12	-131.805	2.329	16	-708.227	2.281	6	-12.74	0	18	-581.491	2.329	14	-883.095	2.329	
95	M9	max	1165.931	0	10	17.524	3.154	15	321.12	3.154	8	-7.925	3.154	12	316.303	0	12	259.408	0
96	min	-1068.126	0	12	-69.136	0	18	-297.925	3.154	14	-16.225	3.203	18	-290.405	0	12	-338.459	0	
97	M11	max	1045.489	2.329	9	131.651	2.329	18	733.885	2.329	9	12.733	4.658	17	725.485	2.329	11	482.88	2.329
98	min	-970.539	0	15	-131.779	2.329	18	-729.272	2.281	5	-12.732	0	17	-599.268	2.329	13	-901.105	2.329	
99	M12	max	1181.098	0	9	17.543	3.154	19	329.237	3.154	11	-7.945	3.154	15	320.12	0	9	263.379	0
100	min	-1081.658	0	15	-69.215	0	17	-306.041	3.154	13	-6.219	3.203	17	-294.213	0	18	-342.437	0	
101	M6	max	1165.931	0	11	17.524	3.154	17	321.12	3.154	9	-7.925	3.154	13	316.303	0	11	259.408	0
102	min	-1089.124	0	13	-69.195	0	19	-297.925	3.154	15	-16.225	3.203	19	-290.405	0	13	-338.458	0	
103	M10	max	1161.402	4.658	9	69.213	4.658	17	306.015	1.504	13	16.22	1.456	17	320.076	4.658	9	263.337	4.658
104	min	-1261.695	4.658	15	-17.538	1.504	19	-329.222	1.504	7.945	1.504	15	-294.19	4.658	15	-342.409	4.658	7	
105	S1	max	1442.868	2.5	15	1879.352	0	19	101.831	2.5	3	1.059	2.5	14	243.321	2.5	9	176.943	0
106	min	-2229.018	0	5	-412.193	2.5	19	-101.815	1.172	3	1.052	0	12	-243.288	2.5	6	-2002.893	1.172	
107	M71	max	1838.182	2.5	8	-346.145	0	15	41.198	1.146	10	0.071	2.5	12	98.775	2.5	10	1505.203	2.5
108	min	-938.469	0	15	-623.792	2.5	17	41.17	0	4	-0.073	0	14	-98.718	2.5	4	-4.202	0	
109	M70	max	1056.078	2.5	10	-347.787	0	12	41.198	1.146	11	0.071	1.146	13	99.775	2.5	11	1505.203	2.5
110	min	28.387	1.172	12	-623.397	2.5	18	41.17	0	5	-0.073	0	15	-98.718	2.5	5	-4.202	0	
111	M69	max	1056.078	2.5	11	-347.787	0	13	41.152	1.146	5	0.068	2.5	14	99.691	2.5	8	1505.203	2.5
112	min	28.387	1.172	3	-623.397	2.5	19	-41.174	0	5	-0.073	0	12	-98.725	2.5	6	4.202	0	
113	S2	max	1442.868	2.5	14	1879.352	0	18	101.819	2.5	11	1.057	1.146	13	243.295	2.5	11	176.863	0
114	min	-2229.018	0	4	-412.193	2.5	18	-101.809	1.172	5	-1.064	0	15	-243.287	2.5	13	-2002.893	1.172	
115	S3	max	1367.253	2.5	13	1879.85	0	17	101.818	2.5	10	1.057	2.5	12	243.295	2.5	10	176.943	0
116	min	-2182.479	0	7	-412.317	2.5	17	-101.809	1.172	4	-1.064	0	14	-243.287	2.5	12	-2003.394	1.172	
117	S4	max	1397.253	2.5	12	1879.85	0	16	101.831	2.5	9	1.059	2.5	15	243.321	2.5	9	176.943	0
118	min	-2182.479	0	6	-412.317	2.5	16	-101.815	1.172	7	-1.062	0	13	-243.299	2.5	7	-2003.394	1.172	
119	M24	max	2648.43	2.5	6	1217.787	0	16	82.329	2.5	9	1.694	1.146	10	197.043	2.5	13	68.87	0
120	min	-1995.455	0	14	-1055.778	2.5	16	-82.402	1.172	7	-1.565	0	7	-197.259	2.5	15	-1317.708	1.172	
121	M23	max	2645.43	2.5	9	1217.787	0	17	82.462	2.5	10	1.555	1.146	10	197.355	2.5	14	68.87	0
122	min	-1999.455	0	15	-1055.778	2.5	17	-82.4	1.172	4	-1.705	0	4	-197.171	2.5	12	-1317.708	1.172	



Company: Vector SE  
 Designer:  
 Job Number:  
 Model Name:

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Envelope Maximum Member Section Forces (Continued)

Member	Axis	Force	Loc	Uy	Shear	Loc	Uz	Shear	Loc	Torque	Loc	Uy-y	Moment	Loc	Uz-z	Moment	Loc		
123	M22	max	1515.153	2.5	101217.065	0	18	82.452	2.5	11	1.555	1.140	197.355	2.5	15	86.765	0	19	
124		min	-869.006	0	-121055.431	2.5	18	-32.4	1.172	0	-1.705	0	5	-197.171	2.5	13	-1316.945	1.721	
125	M21	max	1515.153	2.5	11217.065	0	19	82.325	2.5	8	1.592	1.140	197.043	2.5	12	86.789	0	19	
126		min	-869.006	0	-131055.431	2.5	19	-32.407	1.172	0	-1.555	0	5	-197.259	2.5	14	-1316.945	1.721	
127	M72	max	1533.182	2.5	8-348.145	0	14	41.152	1.146	0	0.068	2.5	15	89.831	2.5	9	1506.218	2.5	16
128		min	-538.460	0	14-623.782	2.5	18	-11.174	0	7	-0.076	0	13	-98.725	2.5	7	-4.198	0	16
129	M17	max	1442.866	2.105	15-300.464	3.933	19	194.382	5.318	14	1.059	3.712	621.371	3.712	8	366.293	3.933	19	
130		min	-584.209	0	5-723.908	3.878	19	-184.419	3.933	4	-1.062	0	12	-821.318	3.712	8	-1459.424	0	19
131	M18	max	1442.866	2.105	14-300.464	3.933	19	194.377	5.318	13	1.057	3.712	621.335	3.712	11	366.293	3.933	18	
132		min	-584.209	0	4-723.908	3.878	13	-194.368	3.933	15	-1.064	0	18	-821.256	3.712	5	-1459.424	0	18
133	M19	max	1397.253	2.105	13-300.529	3.933	17	194.377	5.318	12	1.057	3.712	621.335	3.712	10	366.372	3.933	17	
134		min	-1539.545	0	7-723.851	3.878	17	-194.368	3.933	14	-1.064	0	14	-821.256	3.712	4	-1469.761	0	17
135	M85	max	1086.073	2.105	11-491.806	2.161	19	86.619	3.878	10	0.058	2.105	251.182	3.712	12	2892.162	2.161	19	
136		min	-448.314	2.161	5-676.074	2.105	19	-85.55	3.767	4	-0.075	0	12	-251.102	3.712	14	-23.451	5.318	17
137	M87	max	1535.182	2.105	9-1492.054	2.161	17	86.611	3.878	5	0.071	0.712	251.24	3.712	14	2893.737	2.161	17	
138		min	-1013.866	2.161	7-676.338	2.105	17	-86.605	3.767	6	-0.073	2.18	11	-251.3	3.712	2	-23.44	5.318	16
139	M86	max	1086.073	2.105	10-1491.806	2.161	18	86.611	3.878	9	0.071	3.712	251.24	3.712	5	2892.162	2.161	18	
140		min	-448.314	2.161	4-676.074	2.105	18	-86.685	3.767	7	-0.073	2.151	15	-251.3	3.712	3	-23.451	5.318	16
141	M20	max	1397.253	3.712	12-300.529	3.933	18	194.382	5.318	15	1.059	2.105	621.371	3.712	9	366.372	3.933	16	
142		min	-538.546	2.161	6-723.861	3.878	13	-184.419	3.933	5	-1.062	2.151	13	-821.318	3.712	7	-1459.761	0	16
143	M37	max	1515.153	2.105	11-1080.863	2.161	17	173.158	5.318	13	1.694	2.105	502.544	3.712	8	2392.771	2.161	19	
144		min	-580.983	2.161	9-1110.322	1.919	17	-172.842	3.933	4	-1.565	0	6	-502.325	3.712	6	-34.911	5.318	17
145	M39	max	2546.43	2.105	8-1080.798	2.161	17	173.036	5.318	8	1.555	3.712	502.61	3.712	10	2393.101	2.161	17	
146		min	-2012.362	2.161	7-1111.218	1.951	17	-173.304	3.933	6	-1.705	2.101	4	-502.943	3.712	4	-34.524	5.318	15
147	M40	max	2546.43	2.105	8-1080.798	2.161	16	173.168	5.318	11	1.594	3.712	502.544	3.712	9	2393.101	2.161	16	
148		min	-2012.362	2.161	6-1111.218	1.951	16	-172.842	3.933	5	-1.565	0	7	-502.325	3.712	7	-34.924	5.318	17
149	M88	max	1633.182	2.105	6-1492.054	2.161	16	86.619	3.878	11	0.068	3.712	251.182	3.712	13	2893.737	2.161	16	
150		min	-1013.866	2.161	8-676.338	2.105	16	-85.55	3.767	5	-0.075	2.18	13	-251.102	3.712	15	-23.44	5.318	13
151	M58	max	1515.153	2.105	10-1080.863	2.161	16	173.036	5.318	9	1.555	2.105	502.61	3.712	11	2392.771	2.161	14	
152		min	-860.983	2.161	4-1110.922	1.951	16	-173.304	3.933	7	-1.705	2.151	5	-502.943	3.712	5	-34.511	5.318	16
153	M97	max	920.748	5.072	13-57.795	5.072	15	-30.152	5.072	15	0	5.072	414.198	0	17	293.137	0	15	
154		min	-924.235	0	7-58.42	0	5	-104.818	0	17	0	0	1	0	5.072	1	-256.308	0	5
155	M59	max	920.67	5.072	13-58.422	5.072	9	-30.15	5.072	15	0	5.072	414.194	0	17	296.323	0	9	
156		min	-924.243	0	7-57.8	0	15	-104.816	0	17	0	0	1	0	5.072	1	-293.167	0	15
157	M29	max	1012	5.072	13-55.385	5.072	11	-62.726	5.072	14	0	5.072	722.458	0	18	285.986	0	11	
158		min	-1018.222	0	7-55.84	0	13	-155.594	0	13	0	0	1	0	5.072	1	-283.223	0	13
159	M100	max	1012.050	5.072	13-55.851	5.072	13	-62.95	5.072	14	0	5.072	722.356	0	18	283.279	0	13	
160		min	-1018.245	0	7-56.393	0	7	-165.514	0	16	0	0	1	0	5.072	1	-286.026	0	7
161	M101	max	502.04	5.072	13-28.455	5.072	11	-42.211	5.072	14	0	5.072	494.084	0	18	144.326	0	11	
162		min	-514.168	0	7-27.723	0	13	-120.568	0	16	0	0	1	0	5.072	1	-140.61	0	13
163	M102	max	502.045	5.072	13-27.726	5.072	13	-42.186	5.072	14	0	5.072	494.089	0	18	140.629	0	13	
164		min	-514.18	0	7-28.456	0	7	-120.568	0	16	0	0	1	0	5.072	1	-144.347	0	7
165	M103	max	920.67	5.072	13-58.422	5.072	6	-30.15	5.072	14	0	5.072	414.194	0	16	296.323	0	6	
166		min	-924.243	0	6-57.8	0	4	-104.816	0	16	0	0	1	0	5.072	1	-293.167	0	14
167	M104	max	1012.050	5.072	13-55.851	5.072	13	-62.723	5.072	15	0	5.072	722.451	0	17	283.279	0	12	
168		min	-1018.245	0	6-56.393	0	6	-165.552	0	17	0	0	1	0	5.072	1	-285.028	0	6
169	M105	max	502.045	5.072	13-27.726	5.072	12	-42.21	5.072	15	0	5.072	494.079	0	17	140.629	0	12	
170		min	-514.18	0	6-28.459	0	6	-120.566	0	17	0	0	1	0	5.072	1	-144.347	0	6
171	M106	max	502.04	5.072	13-28.455	5.072	10	-42.197	5.072	15	0	5.072	494.093	0	17	144.326	0	10	
172		min	-514.183	0	6-27.723	0	12	-120.57	0	16	0	0	1	0	5.072	1	-140.61	0	12
173	M107	max	1012	5.072	13-56.385	5.072	10	-62.952	5.072	15	0	5.072	722.065	0	17	285.986	0	10	
174		min	-1018.222	0	6-55.84	0	12	-155.517	0	17	0	0	1	0	5.072	1	-283.223	0	12
175	M108	max	920.748	5.072	13-57.795	5.072	14	-30.152	5.072	14	0	5.072	414.198	0	16	293.137	0	14	
176		min	-924.235	0	6-58.42	0	4	-104.818	0	18	0	0	1	0	5.072	1	-256.308	0	4
177	M109	max	926.452	5.072	15-59.672	5.072	11	-29.762	5.072	13	0	5.072	414.815	0	19	303.676	0	11	



Company : Vector SF  
 Designer :  
 Job Number :  
 Model Name :

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10/24/2024

10:55:17 AM

Checked By : \_\_\_\_\_

**Envelope Maximum Member Section Forces (Continued)**

Member	Axial [k]	LC	LC	LC	LC	LC	LC	LC	LC	LC	LC	LC	LC	LC
178	min	-529.948	0	5	-59.254	0	13	-104.899	0	19	0	0	1	0
179	M110	max	873.921	5.07215	33.905	5.07214	-61.921	5.07215	0	5.07219	723.818	0	17	171.969
190	min	-821.283	0	5	-34.491	0	4	-155.961	0	17	0	0	1	0
181	M111	max	433.152	5.07215	16.757	5.07214	-42.11	5.07215	0	5.07219	494.253	0	17	84.992
182	min	-445.585	0	5	-17.501	0	4	-120.6	0	17	0	0	1	0
183	M112	max	433.199	5.07215	15.457	5.07214	-42.112	5.07215	0	5.07219	494.257	0	17	78.399
184	min	-445.623	0	5	-14.737	0	15	-120.602	0	17	0	0	1	0
185	M113	max	874.015	5.07215	30.38	5.07214	-61.925	5.07215	0	5.07219	723.825	0	17	154.086
186	min	-821.422	0	5	-29.983	0	15	-165.654	0	17	0	0	1	-151.567
187	M114	max	925.508	5.07215	59.247	5.07213	-29.763	5.07215	0	5.07219	414.618	0	19	300.504
188	min	-929.954	0	5	-59.868	0	7	-104.901	0	19	0	0	1	-303.849
189	M115	max	925.452	5.07214	59.872	5.07210	-29.762	5.07214	0	5.07219	414.615	0	18	303.878
190	min	-929.948	0	4	-59.254	0	13	-104.899	0	18	0	0	1	-300.543
191	M116	max	873.921	5.07214	29.882	5.07214	-61.921	5.07214	0	5.07219	723.818	0	16	151.586
192	min	-821.283	0	4	-30.376	0	4	-165.851	0	16	0	0	1	-154.07
193	M117	max	433.152	5.07214	14.737	5.07214	-42.11	5.07214	0	5.07219	494.253	0	16	74.745
194	min	-445.585	0	4	-15.459	0	4	-120.6	0	16	0	0	1	-75.403
195	M118	max	433.199	5.07214	17.503	5.07210	-42.112	5.07214	0	5.07219	494.257	0	16	88.776
196	min	-445.623	0	4	-16.76	0	15	-120.602	0	16	0	0	1	-85.009
197	M119	max	874.015	5.07214	34.501	5.07210	-61.923	5.07214	0	5.07219	723.825	0	16	174.989
198	min	-821.422	0	4	-33.912	0	15	-155.654	0	16	0	0	1	-172.001
199	M120	max	925.508	5.07214	59.247	5.07212	-29.763	5.07214	0	5.07219	414.618	0	16	300.504
200	min	-929.954	0	4	-59.868	0	6	-104.901	0	16	0	0	1	-303.849

**Envelope Node Reactions**

Node Label	X [k]	LC	LC	LC	Z [k]	LC	LC	LC	LC	LC	LC	LC	LC
1	R4	max	2182.479	10	1882.095	10	102.294	11	1.052	13	10.868	11	-110.414
2	min	-910.27	12	1189.088	14	-102.281	5	-1.059	15	-10.876	5	176.943	
3	R1	max	102.294	10	1882.095	10	956.345	15	-110.111	13	10.868	10	1.059
4	min	-102.281	4	1190.199	13	-2229.018	5	-176.803	19	-10.875	4	-1.062	
5	R3	max	102.3	10	1882.065	17	2182.479	11	176.943	17	10.863	8	1.064
6	min	-102.263	4	1189.088	15	-910.27	13	-110.114	15	-10.871	6	-1.057	
7	R2	max	956.348	14	1881.573	19	102.3	11	1.057	13	10.863	9	176.863
8	min	-2229.018	4	1190.199	12	-102.263	5	-1.064	15	-10.871	7	110.711	
9	N53	max	81.825	14	1216.824	19	874.296	11	-55.055	13	8.356	14	1.894
10	min	-82.28	12	770.079	13	-969.006	13	-86.789	19	-8.351	12	-1.565	
11	N54	max	874.296	10	1216.824	18	81.872	15	1.555	11	8.366	9	86.789
12	min	-869.006	12	770.079	12	-82.345	13	-1.705	5	-8.379	7	55.055	
13	N55	max	81.872	14	1217.227	17	1899.405	15	86.87	17	8.366	8	1.705
14	min	-82.345	12	767.985	15	-2003.773	5	54.645	19	-8.379	6	-1.565	
15	N56	max	1999.405	14	1217.227	16	81.825	15	1.565	11	8.356	15	54.848
16	min	-2003.773	4	767.985	14	82.28	13	-1.694	5	-8.351	13	-86.87	
17	N101	max	40.895	14	-347.786	13	1056.073	11	4.202	19	4.179	10	0.068
18	min	-41.014	12	-584.106	19	25.327	13	1.505	13	-4.181	4	-0.076	
19	N102	max	1066.073	10	-347.766	12	40.919	15	0.071	13	4.19	13	-1.505
20	min	28.387	12	-584.106	19	-41.035	13	-0.073	15	-4.191	7	-4.202	
21	N103	max	40.919	14	-346.152	15	538.469	15	-1.561	15	4.19	12	0.073
22	min	-41.035	12	-584.106	17	-1933.162	5	-4.198	17	-4.191	6	-0.071	
23	N104	max	538.469	14	-346.152	14	40.895	15	0.075	13	4.179	11	4.198
24	min	-1633.162	4	-584.106	19	-41.014	13	-0.068	16	-4.181	5	1.561	
25	Totals	max	7728.274	10	10057.249	19	7728.274	11					
26	min	-7728.274	12	6452.807	14	-7728.274	13						



JOB NO.: U0142 2054.242

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PROJECT: NM01-148 SPIKE

**ENCLOSURE CALCULATIONS**

FRP Member Design for Compression (RISA):

Label: FRP Kicker Brace

**INPUT:**

Unbraced Length, L [ft] 10.6  
 Axial C [lb] 652  
 K 1

**Notes:**

See RISA model member M18 for max axial force. Force divided by 2 to account for double angles. Force multiplied by 0.6 to convert LRFD forces to ASD

Column: 4x4x3/8 FRP Angle

r [in]: 0.79  
 C [psi]: 2,800,000  
 A [in<sup>2</sup>]: 2.85

**OUTPUT:**

$f_c$  [psi]: 242 <  $F_c$  [psi]: 356 OK, 68%

**Select 4x4x3/8 FRP Angle FRP column**

FRP Shear Connection w/ Steel Bolts:

Label: Kicker to IHSB, typ.

Bearing stress of FRP member controls

**INPUT:**

Design Force, P [lb] 652  
 Steel Bolt Diameter,  $d_b$  [in] 1/2  
 # Bolts, n 2  
 FRP Web Thickness,  $t_w$  [in] 3/8  
 Double Shear: No  
 Bearing Stress: Lengthwise  
 Factor of Safety, FS 4

**Notes:**

Design Force - axial in FRP Kicker Brace, typ.

**OUTPUT:**

$f_{c2}$  [psi] 1,844 <  $F_{c2}$  [psi] 7,500 OK, 25%

**Select (2) 1/2" diameter steel bolts**

See attached FRP material and section properties.



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PROJECT: NMD1-148 SPIKE  
 FRP Member Design for Compression (RISA):

Label: FRP Vertical Brace

**INPUT:**

Unbraced Length,  $L [ft]$ : 10.8  
 Axial,  $C [lb]$ : 318  
 $K$ : 1

**Notes:**

See RISA model member M42 for max axial force. Force divided by 2 to account for double angles. Force multiplied by 0.0 to convert LRFD forces to ASD

Column: 4x4x3/8 FRP Angle

$r [in]$ : 0.75  
 $E [psi]$ : 2,800,000  
 $A [in^2]$ : 2.85

**OUTPUT:**

$f_c [psi]$ : 111 <  $F_c [psi]$ : 356 OK, 31%

Select 4x4x3/8 FRP Angle FRP column

FRP Shear Connection w/ Steel Bolts:

Label: Vertical Brace to HSS typ.

Bearing stress of FRP member controls.

**INPUT:**

Design Force,  $P [lb]$ : 318  
 Steel Bolt Diameter,  $d_b [in]$ : 1/2  
 # Bolts,  $n_b$ : 2  
 FRP Web Thickness,  $t_w [in]$ : 3/8  
 Double Shear: No  
 Bearing Stress: Longwise  
 Factor of Safety, FS: 4

**Notes:**

Design Force = axial in FRP Vertical Brace, typ.

**OUTPUT:**

$f_{c,v} [psi]$ : 847 <  $F_{c,v} [psi]$ : 7,500 OK, 11%

Select (2) 1/2" diameter steel bolts

See attached FRP material and section properties.



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PROJECT: NMC1-148 Spike

DESIGN APPROACH: LRFD

**BOLTED SHEAR CONNECTION**

Location: STEEL Stand Off Arm

Bolt Grade: ASTM A325

Bolt Diameter: 0.625 in

Number of Bolts: 2

Double Shear? No

Bolt Capacity: 24850 lbs (AISC Equation J3-1)

Shear Load: 2646 lbs

Check Bolt: 10.6%

Result: Select (2) 0.625 in. dia. ASTM A325 bolts.

Note: See RISA model section set 'STEEL Stand Off Arm' load combination 4 for max Axial [lb]

**BOLT/PIN BEARING & MATERIAL TENSILE/SHEAR STRENGTH**

Location: STEEL Stand Off Arm

Bolt or Pin Diameter: 0.525 in

Hole Diameter or Slot Width: 0.6875 in

Number of Bolts or Pins: 2

Plate Thickness: 0.375 in

Plate Yield Strength ( $F_y$ ): 36 ksiPlate Ultimate Strength ( $F_u$ ): 58 ksi

Bolt/Pin Parallel Edge Distance: 1 in

Bearing Capacity: 25692 lbs

Perpendicular Edge Distance: 1 in

Effective Perp. Edge Distance: 1 in

Tensile Rupture Capacity: 42820 lbs

Shear Rupture Capacity: 37927 lbs

Load: 2646 lbs

Check Bearing: 10.3%

Result: Selected connection type is adequate.

Note: See RISA model section set 'STEEL Stand Off Arm' load combination 4 for max Axial [lb]

## Available AISC Checks

Equation	Check?	Capacity
J3-6a	Yes	12846
J3-6b	No	
J3-6c	No	
J7-1	No	

(measured from center of hole)

(measured from center of hole)

(AISC Equation D5-1)

(AISC Equation D5-2)

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PROJECT: NMD1-148 Spike

**BOLTED SHEAR CONNECTION** Location: STEEL Outrigger Weldment

Bolt Grade:	ASTM A325		
Bolt Diameter:	0.625	in	
Number of Bolts:	1		
Double Shear?	No		
Bolt Capacity:	12425	lbs	(AISC Equation J3-1)
Shear Load:	1018	lbs	
Check Bolt	8.2%		

Result: Select (1) 0.625 in. dia. ASTM A325 bolt.

Note: See RISA model section set 'STEEL Outrigger Weldment' load combination 6 for max Axial [lb]

**BOLT/PIN BEARING & MATERIAL TENSILE/SHEAR STRENGTH** Location: STEEL Outrigger Weldment

Bolt or Pin Diameter:	0.625	in		
Hole Diameter or Slot Width:	0.5875	in		
Number of Bolts or Pins:	1			
Plate Thickness:	0.375	in		
Plate Yield Strength ( $F_y$ ):	36	ksi		
Plate Ultimate Strength ( $F_u$ ):	58	ksi		
Bolt/Pin Parallel Edge Distance:	1	in		(measured from center of hole)
Bearing Capacity:	12846	lbs		
Perpendicular Edge Distance:	1	in		(measured from center of hole)
Effective Perp. Edge Distance:	1			
Tensile Rupture Capacity:	21410	lbs		(AISC Equation D5-1)
Shear Rupture Capacity:	18963	lbs		(AISC Equation D5-2)
Load:	1018	lbs		
Check Bearing	7.9%			

Result: Selected connection type is adequate.

Note: See RISA model section set 'STEEL Outrigger Weldment' load combination 6 for max Axial [lb]



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PROJECT: NM01-148 Spike

**BOLTED  
SHEAR CONNECTION**

Location: STEEL Stand Off Arm Inner

Bolt Grade:	ASTM A325	
Bolt Diameter:	0.75	in
Number of Bolts:	3	
Double Shear?	No	
Bolt Capacity:	53677	lbs (AISC Equation J3-1)
Shear Load:	1898	lbs
Check Bolt:	3.5%	

Result: **Select (3) 0.75 in. dia. ASTM A325 bolts.**

Note: See RISA model section set 'STEEL Stand Off Arm Inner' load combination 6 for max Axial [lb]

**BOLT/PIN BEARING  
& MATERIAL TENSILE/SHEAR STRENGTH**

Location: STEEL Stand Off Arm Inner

			Available AISC Checks		
			Equation	Check?	Capacity
Bolt or Pin Diameter:	0.75	in			
Hole Diameter or Slot Width:	0.8125	in			
Number of Bolts or Pins:	3		J3-6a	Yes	11623
Plate Thickness:	0.375	in	J3-6b	No	
Plate Yield Strength ( $F_y$ ):	36	ksi	J3-6c	No	
Plate Ultimate Strength ( $F_u$ ):	58	ksi	J7-1	No	
Bolt/Pin Parallel Edge Distance:	1	in	(measured from center of hole)		
Bearing Capacity:	34868	lbs			
Perpendicular Edge Distance:	1	in	(measured from center of hole)		
Effective Perp. Edge Distance:	1				
Tensile Rupture Capacity:	58113	lbs	(AISC Equation D5-1)		
Shear Rupture Capacity:	56800	lbs	(AISC Equation D5-2)		
Load:	1898	lbs			
Check Bearing:	5.4%				

Result: **Selected connection type is adequate.**

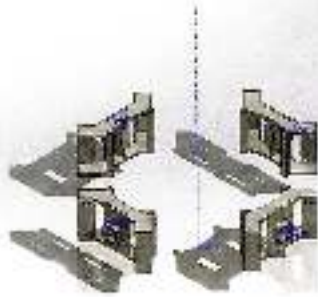
Note: See RISA model section set 'STEEL Stand Off Arm Inner' load combination 6 for max Axial [lb]



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## Simulation of MONOPOLE MOUNT

Date: Thursday, October 24, 2024  
 Designer: JJB  
 Study name: Static 1  
 Analysis type: Static

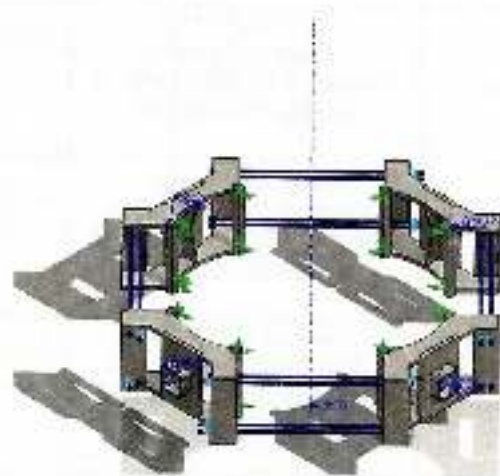


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**Description**  
 Four-sided Raycap Clamp





Model name: MONOPOLE MOUNT  
 Current Configuration: Default

Solid Bodies			
Document Name and Reference	Treated As	Volumetric Properties	Document Path/Date Modified
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024





Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup>	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt





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		Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	Oct 23 17:20:18 2024
Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024





Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024





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Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024





## Study Properties

Study name	Static 1
Analysis type	Static
Mesh type	Solid Mesh
Thermal Effect:	On
Thermal option	Include temperature loads
Zero strain temperature	77 Fahrenheit
Include fluid pressure effects from SOLIDWORKS Flow Simulation	Off
Solver type	FFEPlus
Inplane Effect:	Off
Soft Spring:	Off
Inertial Relief:	Off
Incompatible bonding options	Automatic
Large displacement	Off
Compute free body forces	Off
Friction	Off
Use Adaptive Method:	Off
Result folder	SOLIDWORKS document (C:\Users\joshua.blom\Desktop\Raycap Clamp\Results)


## Units

Unit system:	English (IPS)
Length/Displacement	in
Temperature	Fahrenheit
Angular velocity	Hertz
Pressure/Stress	ksi





## Material Properties

Model Reference	Properties	Components
	<p><b>Name:</b> ASTM A36 Steel  <b>Model type:</b> Linear Elastic Isotropic  <b>Default failure criterion:</b> Max von Mises Stress  <b>Yield strength:</b> 250 N/mm<sup>2</sup>  <b>Tensile strength:</b> 400 N/mm<sup>2</sup>  <b>Elastic modulus:</b> 200,000 N/mm<sup>2</sup>  <b>Poisson's ratio:</b> 0.26  <b>Mass density:</b> 7.85 g/cm<sup>3</sup>  <b>Shear modulus:</b> 79,300 N/mm<sup>2</sup></p>	<p>SolidBody  1(Mirror1)(Assem8*MONOPOLE MOUNT-1/2 x 0.145 - 6-1),  SolidBody  1(Mirror1)(Assem8*MONOPOLE MOUNT-1/2 x 0.145 - 6-2),  SolidBody 1(Cut-Extrude1)(Assem8*MONOPOLE MOUNT-1/4 - 6-1),  SolidBody 1(Cut-Extrude1)(Assem8*MONOPOLE MOUNT-1/4 - 6-2),  SolidBody 1(Boss-Extrude1)(Assem8*MONOPOLE MOUNT-1/MONOPOLE MOUNT PLATE-1),  SolidBody 1(Cut-Extrude1)(Assem8*MONOPOLE MOUNT-1/MONOPOLE MOUNT STEEL TUBE-1),  SolidBody 1(Boss-Extrude1)(Assem8*MONOPOLE MOUNT-1/MONOPOLE MOUNT SUPPORT-1),  SolidBody 1(Boss-Extrude1)(Assem8*MONOPOLE MOUNT-1/W PLATE-2),  SolidBody  2(Mirror2)(Assem8*MONOPOLE MOUNT-1/W PLATE-2),  SolidBody  1(Mirror1)(Assem8*MONOPOLE MOUNT-10/2 x 0.145 - 6-1),  SolidBody  1(Mirror1)(Assem8*MONOPOLE MOUNT-10/2 x 0.145 - 6-2),  SolidBody 1(Cut-Extrude1)(Assem8*MONOPOLE MOUNT-10/4 - 6-1),  SolidBody 1(Cut-Extrude1)(Assem8*MONOPOLE MOUNT-10/4 - 6-2),  SolidBody 1(Boss-Extrude1)(Assem8*MONOPOLE</p>





		<p>MOUNT-10/MONOPOLE MOUNT PLATE-1),          SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-10/MONOPOLE MOUNT STEEL TUBE-1),          SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-10/MONOPOLE MOUNT SUPPORT-1),          SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-10/W PLATE-2),          SolidBody 2(Mirror2)(Assem8^MONOPOLE MOUNT-10/W PLATE-2),          SolidBody 1(Mirror1)(Assem8^MONOPOLE MOUNT-11/2 x 0.145 - 6-1),          SolidBody 1(Mirror1)(Assem8^MONOPOLE MOUNT-11/2 x 0.145 - 6-2),          SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-11/4 - 6-1),          SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-11/4 - 6-2),          SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-11/MONOPOLE MOUNT PLATE-1),          SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-11/MONOPOLE MOUNT STEEL TUBE-1),          SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-11/MONOPOLE MOUNT SUPPORT-1),          SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-11/W PLATE-2),          SolidBody 2(Mirror2)(Assem8^MONOPOLE MOUNT-11/W PLATE-2),          SolidBody 1(Mirror1)(Assem8^MONOPOLE MOUNT-8/2 x 0.145 - 6-1),</p>
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		SolidBody 1(Mirror1)(Assem8" MONOPOLE MOUNT-8/2 x D.145 - 6-2), SolidBody 1(Cut- Extrude1)(Assem8" MONOPOLE MOUNT-8/4 - 6-1), SolidBody 1(Cut- Extrude1)(Assem8" MONOPOLE MOUNT-8/4 - 6-2), SolidBody 1(Boss- Extrude1)(Assem8" MONOPOLE MOUNT-8/MONOPOLE MOUNT PLATE-1), SolidBody 1(Cut- Extrude1)(Assem8" MONOPOLE MOUNT-8/MONOPOLE MOUNT STEEL TUBE-1), SolidBody 1(Boss- Extrude1)(Assem8" MONOPOLE MOUNT-8/MONOPOLE MOUNT SUPPORT-1), SolidBody 1(Boss- Extrude1)(Assem8" MONOPOLE MOUNT-8/W PLATE-2), SolidBody 2(Mirror2)(Assem8" MONOPOLE MOUNT-8/W PLATE-2)
Curve Data:N/A		





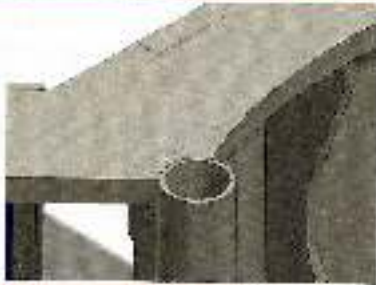
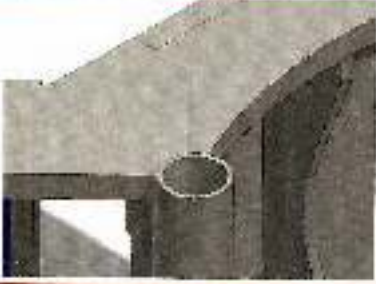

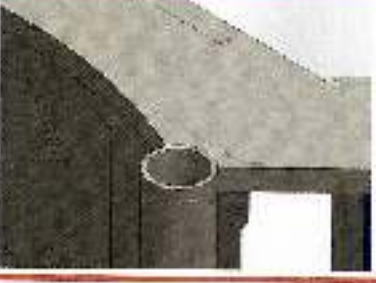

## Loads and Fixtures

Fixture name	Fixture Image	Fixture Details		
Reference Geometry-2		Entities: 8 edge(s) Reference: Face< 1 > Type: Use reference geometry Translation: 0, 0 rad., 0 Units: in		
<b>Resultant Forces</b>				
Components	X	Y	Z	Resultant
Reaction force(lbf)	0.729984	-7,184.11	0.138231	7,184.11
Reaction Moment(lbf.in)	0	0	0	0

Load name	Load Image	Load Details
Gravity-1		Reference: Top Plane Values: 0 0 -386.22 Units: in/s <sup>2</sup>
Force-1		Entities: 1 face(s) Type: Apply normal force Value: -2,229 lbf

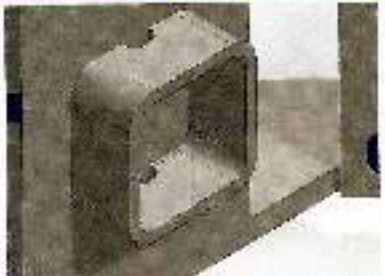
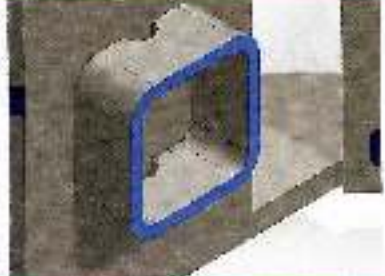
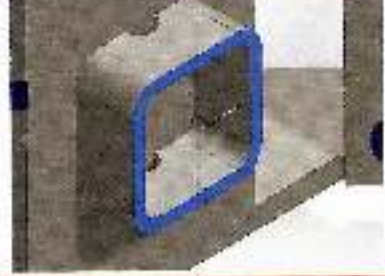





Force-2		<p>Entities: 1 face(s) Reference: Axis2 Type: Apply force Values: ---, ---, -1,879.9 lbf</p>
Torque-1		<p>Entities: 1 face(s) Reference: Axis6 Type: Apply torque Value: 18,074.6 lbf.in</p>
Copy[ 1 ] Force-1		<p>Entities: 1 face(s) Type: Apply normal force Value: -2.229 lbf</p>
Copy[ 1 ] Force-2		<p>Entities: 1 face(s) Reference: Axis17 Type: Apply force Values: ---, ---, 1,879.9 lbf</p>
Copy[ 1 ] Torque-1		<p>Entities: 1 face(s) Reference: Axis18 Type: Apply torque Value: 18,074.6 lbf.in</p>

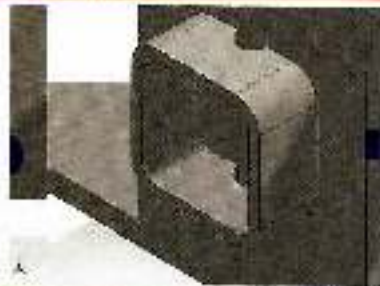
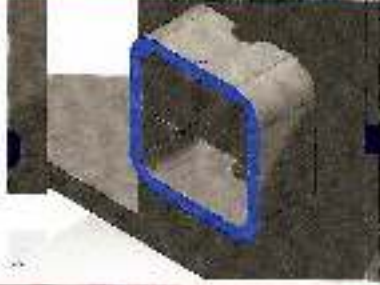




<p>Copy[ 1 ] Force-1[1]</p>		<p>Entities: 1 face(s) Type: Apply normal force Value: -2,229 lbf</p>
<p>Copy[ 1 ] Force-2[1]</p>		<p>Entities: 1 face(s) Reference: Axis19 Type: Apply force Values: ---, ---, 1,879.9 lbf</p>
<p>Copy[ 1 ] Torque-1[1]</p>		<p>Entities: 1 face(s) Reference: Axis20 Type: Apply torque Value: 18,074.6 lb·in</p>
<p>Copy[ 1 ] Force-1[1][1]</p>		<p>Entities: 1 face(s) Type: Apply normal force Value: -2,229 lbf</p>



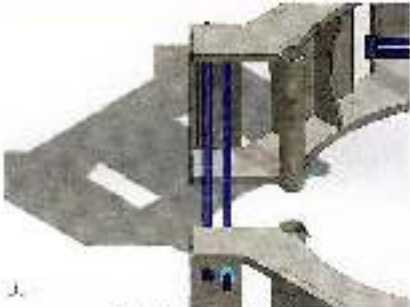



<p>Copy[ 1 ] Force-2{13}{1}</p>		<p>Entities: 1 face(s) Reference: Axis16 Type: Apply force Values: <math>-1,879.9</math> lbf</p>
<p>Copy[ 1 ] Torque-1{1}{1}</p>		<p>Entities: 1 face(s) Reference: Axis15 Type: Apply torque Value: <math>18,074.6</math> lbf.in</p>



## Connector Definitions

### Pin/Bolt/Bearing Connector

Model Reference	Connector Details			Strength Details
 <p>Pin Connector-1</p>	Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0	No Data		
<b>Connector Forces Joint 1</b>				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	299.43	0	299.43	423.46
Shear Force (lbf)	0.29259	0.15461	-0.29257	0.44171
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	95.95	137.48	-95.95	193.17
<b>Connector Forces Joint 2</b>				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-299.43	-0	-299.43	-423.46
Shear Force (lbf)	-0.29259	-0.15461	0.29257	0.44171
Torque (lbf.in)	4.2204e-06	0	4.2204e-06	5.9685e-06
Bending moment (lbf.in)	-99.197	-125.19	99.197	188.02
 <p>Pin Connector-2</p>	Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0	No Data		





### Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	167.08	-0	167.08	-236.29
Shear Force (lbf)	-0.14211	-0.044949	0.14209	0.20592
Torque (lbf.in)	-2.2336e-08	0	-2.2336e-08	3.1589e-08
Bending moment (lbf.in)	50.597	-57.461	-50.597	91.771

### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-167.08	0	-167.08	236.29
Shear Force (lbf)	0.14211	0.044949	-0.14209	0.20592
Torque (lbf.in)	6.4084e-08	-0	6.4084e-08	-9.0628e-08
Bending moment (lbf.in)	-51.588	63.724	51.588	96.868



Pin Connector-3

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

### Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	148.6	-0	148.6	-210.15
Shear Force (lbf)	0.34643	-0.28745	-0.34642	0.56802
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	-60.912	46.294	60.912	97.794

### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-148.6	0	-148.6	210.15
Shear Force (lbf)	-0.34643	0.28745	0.34642	0.56802
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	54.792	-61.043	-54.792	98.644





	<p>Entities: 2 face(s)                  Type: Pin                  With retaining ring (No translation): Yes                  With key (No rotation): No                  Connection Type: Rigid                  Units: English (IPS)                  Rotational stiffness value: 0</p>	No Data
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Pin Connector-4

Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	8.3205	0	8.3205	11.767
Shear Force (lbf)	-0.13743	0.077944	0.13743	0.2094
Torque (lbf.in)	6.2462e-08	0	6.2462e-08	8.8335e-08
Bending moment (lbf.in)	23.552	-22.282	-23.552	40.073

Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-8.3205	-0	-8.3205	-11.767
Shear Force (lbf)	0.13743	-0.077944	-0.13743	0.2094
Torque (lbf.in)	7.6283e-09	0	7.6283e-09	1.0788e-08
Bending moment (lbf.in)	-25.215	16.418	25.215	39.257

	<p>Entities: 2 face(s)                  Type: Pin                  With retaining ring (No translation): Yes                  With key (No rotation): No                  Connection Type: Rigid                  Units: English (IPS)                  Rotational stiffness value: 0</p>	No Data
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Pin Connector-5

Connector Forces Joint 1

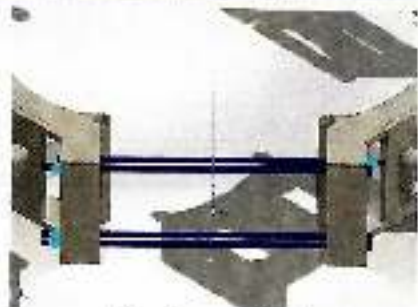
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	296.1	0	-296.1	418.75
Shear Force (lbf)	0.17629	-0.14127	0.17627	0.28655
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	-100.37	124.44	-100.37	188.77

Connector Forces Joint 2





Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-296.1	-0	296.1	-418.75
Shear Force (lbf)	-0.17629	0.14127	-0.17627	0.28655
Torque (lbf.in)	0	0	-0	0
Bending moment (lbf.in)	97.468	-131.69	97.468	190.64



Pin Connector-6

Entities: 2 face(s)  
 Type: Pin  
 With retaining ring (No translation): Yes  
 With key (No rotation): No  
 Connection: Rigid  
 Type:  
 Units: English (IPS)  
 Rotational stiffness value: 0

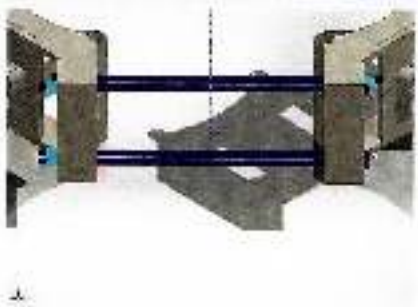
No Data

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	177.69	-0	-177.69	-251.29
Shear Force (lbf)	-0.041436	0.011963	-0.041423	0.059799
Torque (lbf.in)	3.2385e-07	-0	-3.2385e-07	-4.5799e-07
Bending moment (lbf.in)	-57.751	-60.293	-57.751	101.52

**Connector Forces Joint 2**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-177.69	0	177.69	251.29
Shear Force (lbf)	0.041436	-0.011963	0.041423	0.059799
Torque (lbf.in)	-3.0908e-07	0	3.0908e-07	4.3711e-07
Bending moment (lbf.in)	57.401	57.866	57.401	99.69



Pin Connector-7

Entities: 2 face(s)  
 Type: Pin  
 With retaining ring (No translation): Yes  
 With key (No rotation): No  
 Connection: Rigid  
 Type:  
 Units: English (IPS)  
 Rotational stiffness value: 0

No Data

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
------	-------------	-------------	-------------	-----------





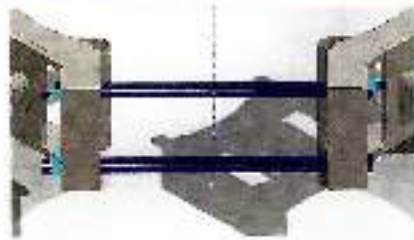
Vector Structural Engineers, LLC  
651 W Galena Park Blvd., Suite 101  
Draper, UT 84020

JJB  
10/24/2024

Axial Force (lbf)	-138.99	-0	138.99	-196.57
Shear Force (lbf)	-0.073459	0.13005	-0.073473	0.16646
Torque (lbf.in)	-2.034e-06	-0	2.034e-06	-2.8765e-06
Bending moment (lbf.in)	-51.875	-49.749	-51.875	88.64

#### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	138.99	0	-138.99	196.57
Shear Force (lbf)	0.073459	-0.13005	0.073473	0.16646
Torque (lbf.in)	1.913e-06	0	-1.913e-06	2.7054e-06
Bending moment (lbf.in)	54.745	52.992	54.745	93.82



Pin Connector-B

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

#### Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	12.477	0	-12.477	17.645
Shear Force (lbf)	-0.055332	-0.039551	-0.055333	0.08768
Torque (lbf.in)	0	0	-0	0
Bending moment (lbf.in)	-21.054	-17.507	-21.054	34.538

#### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-12.477	-0	12.477	-17.645
Shear Force (lbf)	0.055332	0.039551	0.055333	0.08768
Torque (lbf.in)	1.0551e-06	0	-1.0551e-06	1.4921e-06
Bending moment (lbf.in)	20.211	19.861	20.211	34.806





	<p>Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0</p>	No Data
--	---	---------

Pin Connector-9

## Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-289.93	0	-289.93	410.03
Shear Force (lbf)	0.31207	-0.4776	-0.31209	0.6503
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	-97.56	122.94	97.56	184.8

## Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	289.93	-0	289.93	-410.03
Shear Force (lbf)	-0.31207	0.4776	0.31209	0.6503
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	87.434	-136.17	-87.434	183.94

	<p>Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0</p>	No Data
--	---	---------

Pin Connector-10

## Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	195.92	-0	195.92	-277.07
Shear Force (lbf)	0.23139	-0.1846	-0.23138	0.37571
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	63.693	65.093	-63.693	111.13

## Connector Forces Joint 2





Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-195.92	0	-195.92	277.07
Shear Force (lbf)	-0.23139	0.1846	0.73138	0.37571
Torque (lbf.in)	2.1102e-06	-0	2.1102e-06	-2.9842e-06
Bending moment (lbf.in)	-67.595	-74.877	67.595	121.43



Pin Connector-11

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-140.61	-0	-140.61	-198.85
Shear Force (lbf)	0.40394	0.44276	-0.40395	0.72276
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	51.57	57.884	-51.57	92.11

Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	140.61	0	140.61	198.85
Shear Force (lbf)	-0.40394	-0.44276	0.40395	0.72276
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	-61.01	-40.66	61.01	95.382



Pin Connector-12

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
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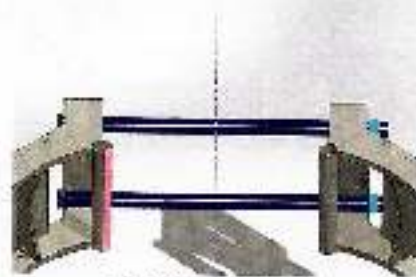




Axial Force (lbf)	21.421	0	21.421	30.293
Shear Force (lbf)	0.19279	0.31392	-0.19279	0.41578
Torque (lbf.in)	-9.8166e-09	-0	-9.8166e-09	-1.3883e-08
Bending moment (lbf.in)	12.75	24.596	-12.75	30.497

## Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-21.421	-0	-21.421	-30.293
Shear Force (lbf)	-0.19279	-0.31392	0.19279	0.41578
Torque (lbf.in)	-2.3525e-07	-0	-2.3525e-07	-3.327e-07
Bending moment (lbf.in)	-19.452	-16.364	19.452	32.008



Pin Connector-13

Entities: 2 face(s)  
 Type: Pin  
 With retaining ring (No translation): Yes  
 With key (No rotation): No  
 Connection Type: Rigid  
 Units: English (IPS)  
 Rotational stiffness value: 0

No Data

## Connector Forces Joint 1


Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-4.5667	0	4.5667	6.4583
Shear Force (lbf)	0.29607	1.3987	0.29607	1.46
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-17.015	14.157	-17.015	27.919

## Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	4.5667	-0	-4.5667	-6.4583
Shear Force (lbf)	-0.29607	-1.3987	-0.29607	1.46
Torque (lbf.in)	-5.2755e-07	0	5.2755e-07	7.4606e-07
Bending moment (lbf.in)	-12.839	-1.5182	-12.839	18.22





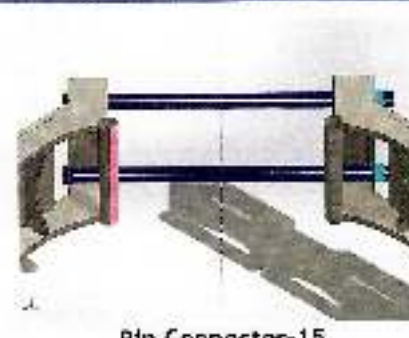
 <p>Pin Connector-14</p>	<p>Entities: 2 face(s)                  Type: Pin                  With retaining ring (No translation): Yes                  With key (No rotation): No                  Connection Type: Rigid                  Units: English (IPS)                  Rotational stiffness value: 0</p>	<p>No Data</p>
---	---	----------------

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	11.271	-0	-11.271	-15.94
Shear Force (lbf)	0.2995	1.7639	0.2995	1.814
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-18.251	7.4271	-18.251	26.858

**Connector Forces Joint 2**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-11.271	0	11.271	15.94
Shear Force (lbf)	-0.2995	-1.7639	-0.2995	1.814
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-19.398	5.3579	-19.398	27.951

 <p>Pin Connector-15</p>	<p>Entities: 2 face(s)                  Type: Pin                  With retaining ring (No translation): Yes                  With key (No rotation): No                  Connection Type: Rigid                  Units: English (IPS)                  Rotational stiffness value: 0</p>	<p>No Data</p>
---	---	----------------

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	4.7067	-0	-4.7067	-6.6563
Shear Force (lbf)	-0.36657	1.48	-0.36657	1.5682
Torque (lbf.in)	-2.8054e-07	0	2.8054e-07	3.9674e-07
Bending moment (lbf.in)	-18.377	-16.867	-18.377	30.983

**Connector Forces Joint 2**

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Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-4.7067	0	4.7067	6.6763
Shear Force (lbf)	0.36657	-1.48	0.36657	1.5682
Torque (lbf.in)	2.9124e-08	-0	-2.9124e-08	-4.1187e-08
Bending moment (lbf.in)	-13.708	1.221	-13.208	18.719



Pin Connector-16

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

## Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-11.411	0	11.411	16.138
Shear Force (lbf)	-0.22899	1.8998	-0.22899	1.9272
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-21.217	-4.4196	-21.217	30.329





## Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	11.411	-0	-11.411	-16.138
Shear Force (lbf)	0.22899	-1.8998	0.22899	1.9272
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-19.333	-5.3556	-19.333	27.861





## Interaction Information

Interaction	Interaction Image	Interaction Properties
Component Contact-9		<p><b>Type:</b> Bonded  <b>Components:</b> 5 component(s),            2 Solid Body (s)  <b>Options:</b> Continuous mesh</p>
Component Interaction-12		<p><b>Type:</b> Bonded  <b>Components:</b> 8 component(s)  <b>Options:</b> Independent mesh</p>
Component Interaction-13		<p><b>Type:</b> Bonded  <b>Components:</b> 8 component(s)  <b>Options:</b> Independent mesh</p>
Component Interaction-14		<p><b>Type:</b> Bonded  <b>Components:</b> 8 component(s)  <b>Options:</b> Independent mesh</p>





### Mesh information

Mesh type	Solid Mesh
Mesher Used:	Curvature-based mesh
Jacobian points for High quality mesh	16 Points
Maximum element size	2 in
Minimum element size	0.4 in
Mesh Quality	High
Remesh failed parts independently	Off

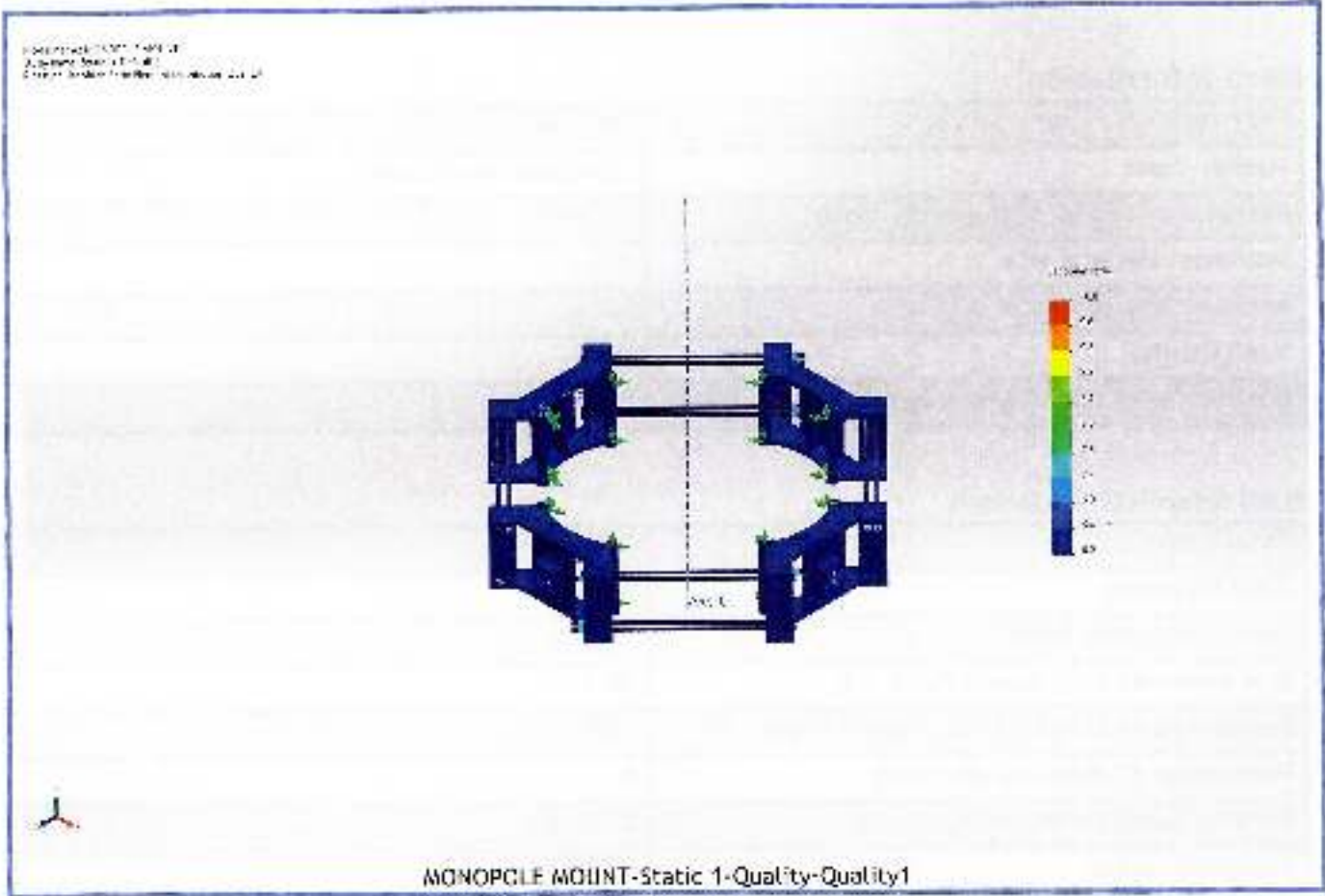
### Mesh information - Details

Total Nodes	74378
Total Elements	35555
Maximum Aspect Ratio	53.291
% of elements with Aspect Ratio < 3	49.7
Percentage of elements with Aspect Ratio > 10	3.55
Percentage of distorted elements	0
Time to complete mesh(hh:mm:ss):	00:00:05
Computer name:	VSE096

### Mesh Quality Plots

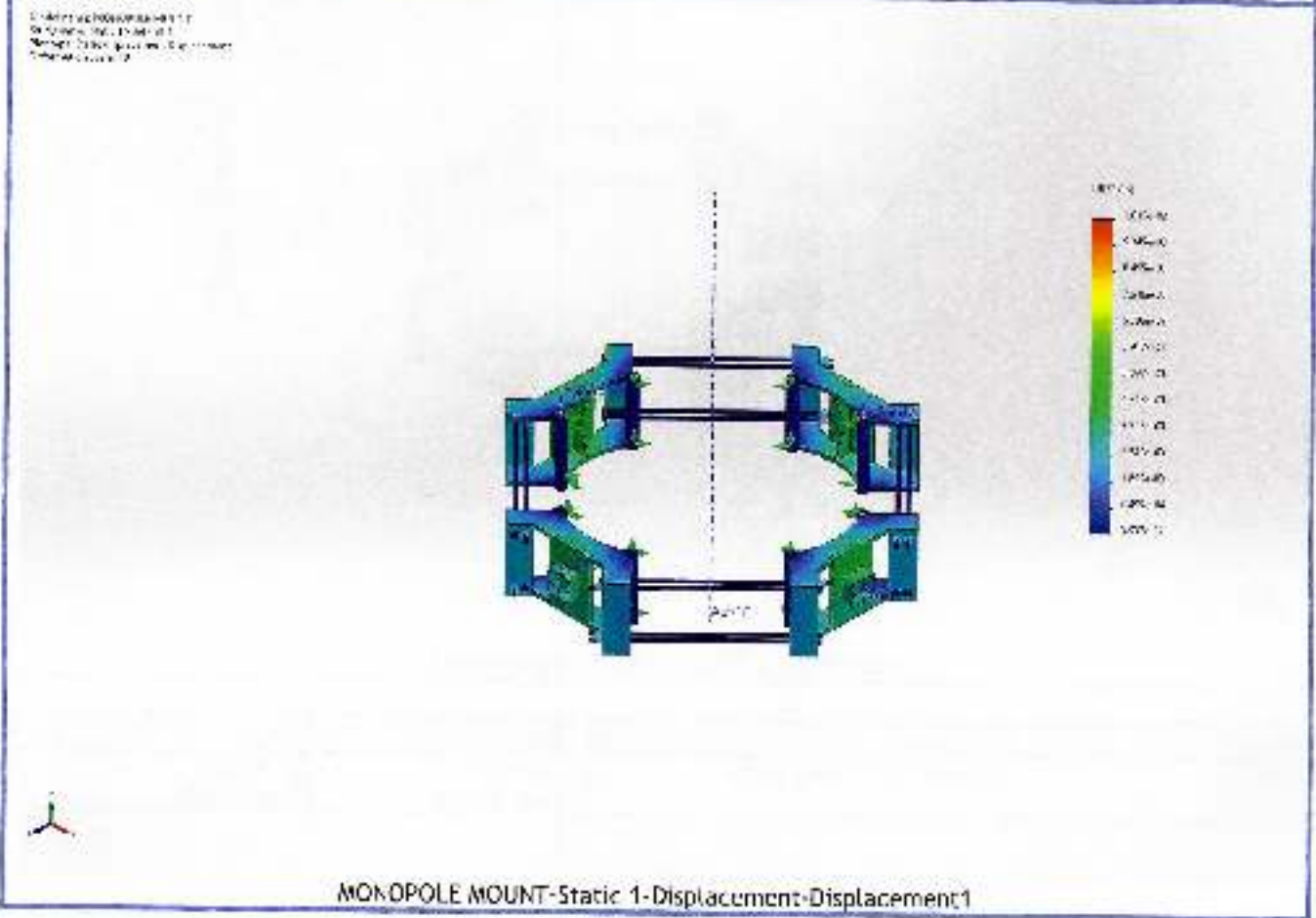
Name	Type	Min	Max
Quality1	Jacobian ratio	1.0 Element: 2023	28.9 Element: 20129



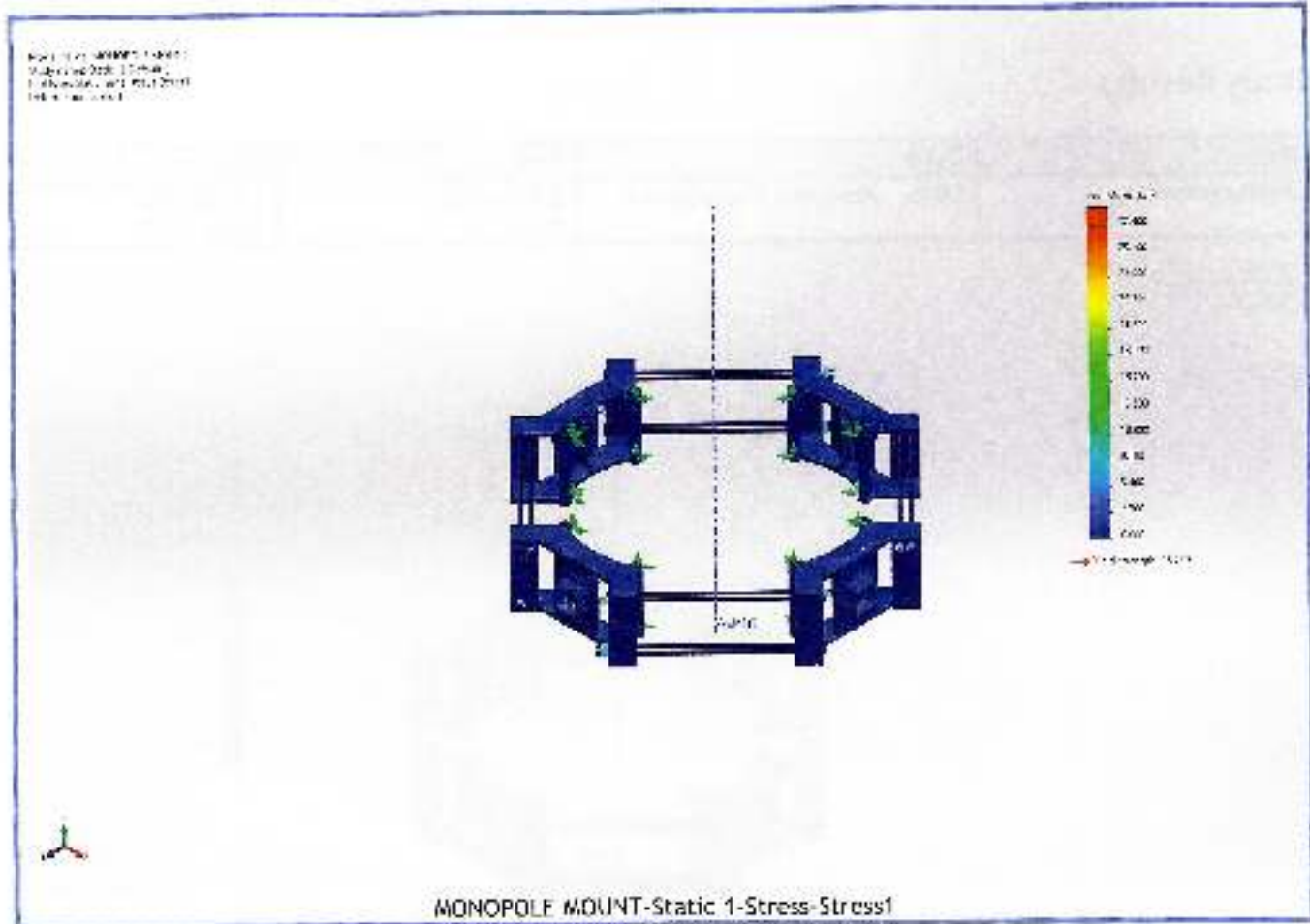


### Study Results

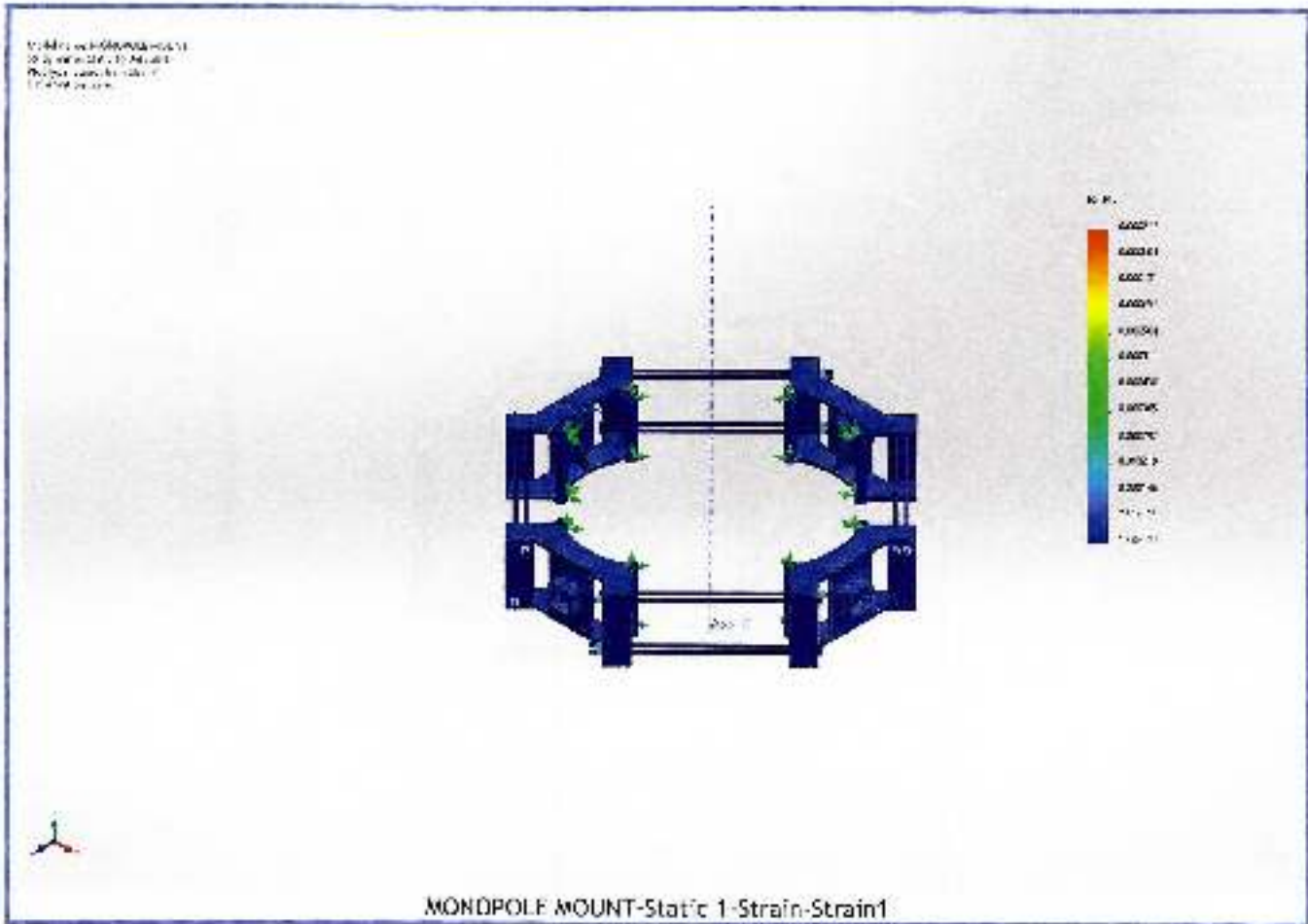
Name	Type	Min	Max
Displacement1	URES: Resultant Displacement	0.000e+00in Node: 15	1.019e-02in Node: B757



Name	Type	Min	Max
Stress1	VON: von Mises Stress	0.000ksi Node: 18526	30.273ksi Node: 479

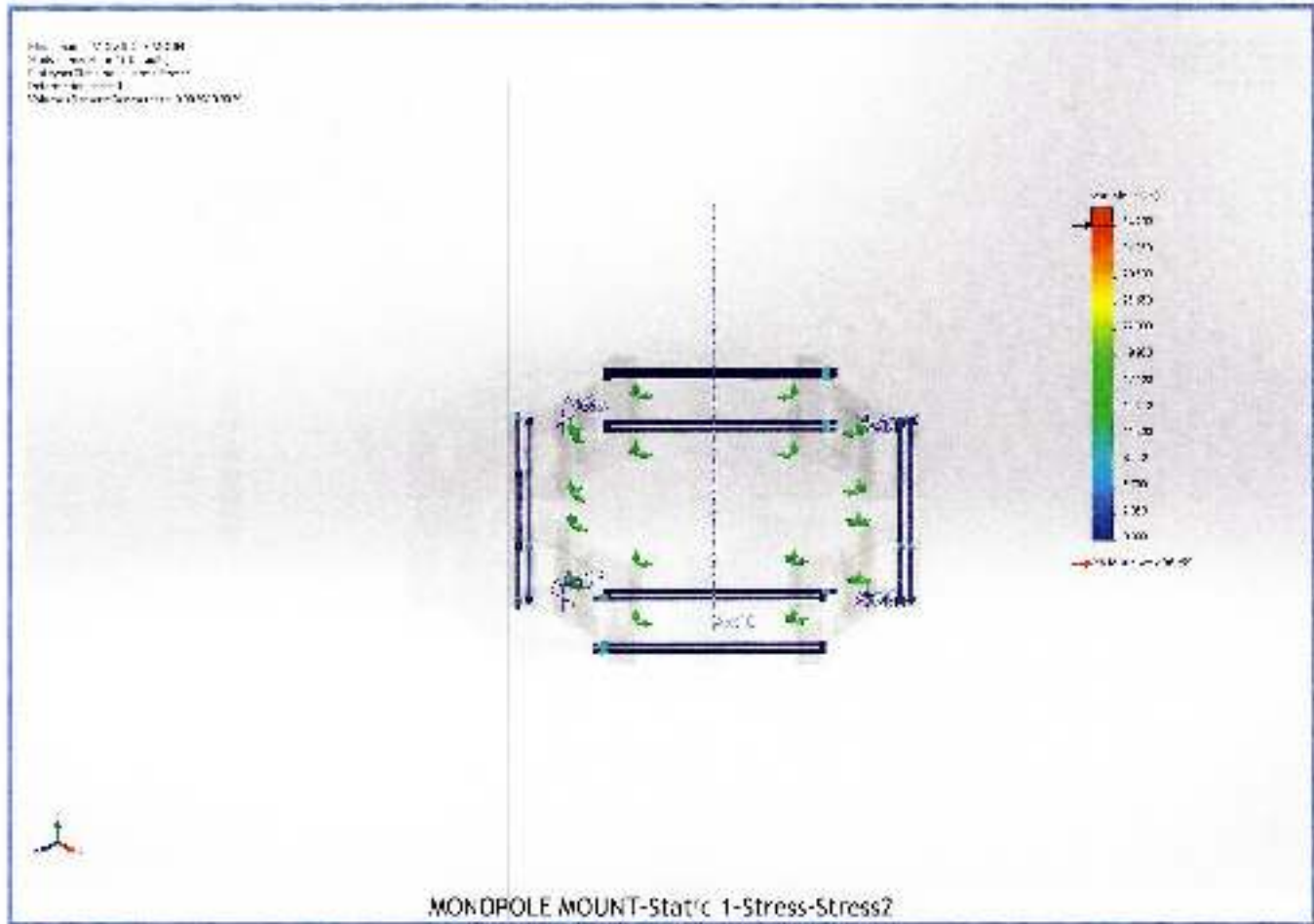


Name	Type	Min	Max
Strain1	ESTRN: Equivalent Strain	1.38e-09 Node: 18526	0.000877 Node: 479



Name	Type	Min	Max
Stress2	VON: von Mises Stress	0.000ksi Node: 18526	30.273ksi Node: 479





### Conclusion

#### Comments:

No part of the assembly exceeds the permissible Von-Mises stress. Therefore, OK.





## ASCE Hazards Report

**Address:**  
No Address at This Location

**Standard:** ASCE/SEI 7-16

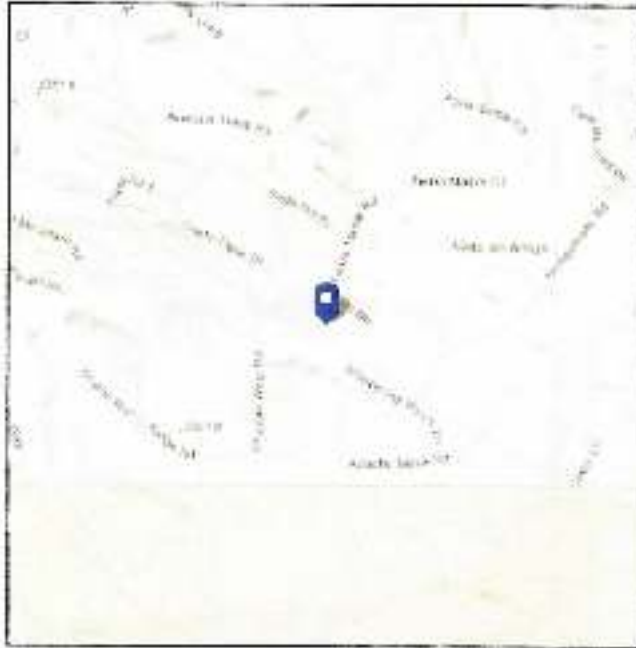
**Latitude:** 35.30946

**Risk Category:** II

**Longitude:** -106.49543

**Soil Class:** C - Very Dense  
Soil and Soft Rock

**Elevation:** 5504.708854228105 ft  
(NAVD 88)



### Wind

#### Results:

Wind Speed	104 Vmph
10-year MRI	75 Vmph
25-year MRI	82 Vmph
50-year MRI	86 Vmph
100-year MRI	91 Vmph

**Data Source:** ASCE/SEI 7-16, Fig. 26.5-1B and Figs. CC.2-1-CC.2-4, and Section 26.5.2

**Date Accessed:** Thu Oct 24 2024

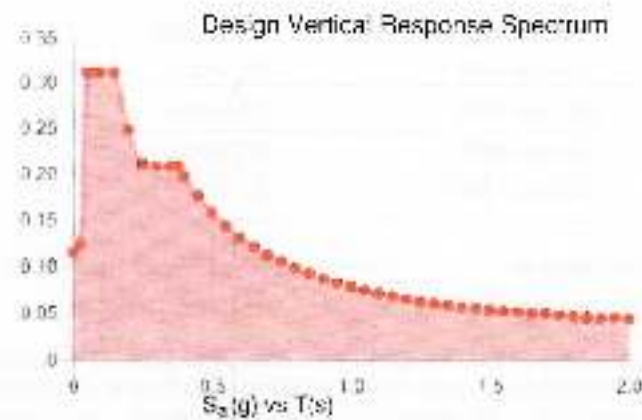
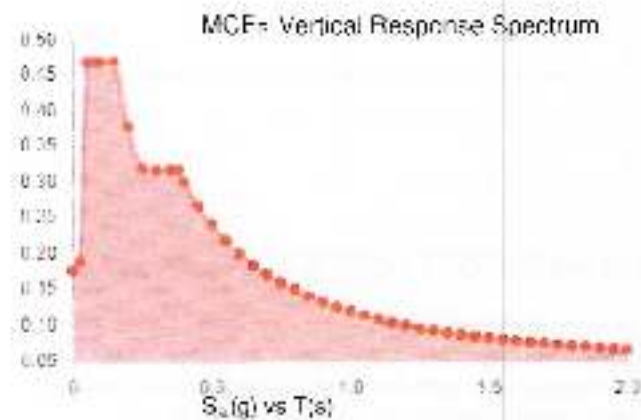
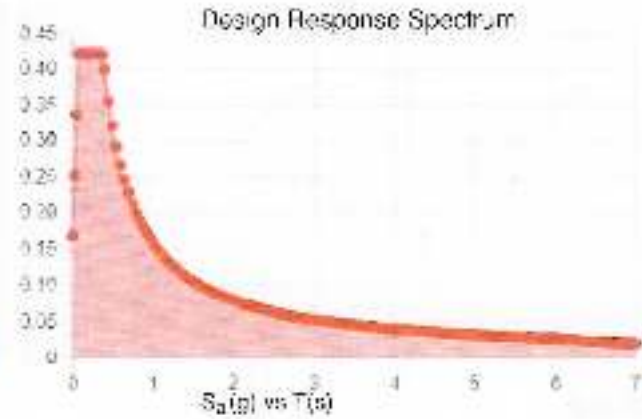
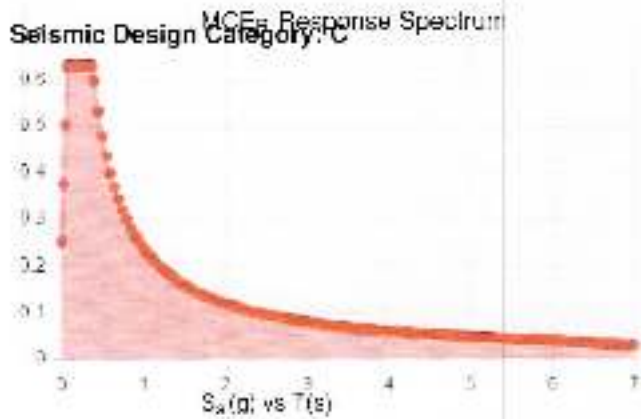
Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2.

Site Soil Class: C - Very Dense Soil and Soft Rock

Results:

$S_s$ :	0.487	$S_{1.0}$ :	0.16
$S_1$ :	0.15	$T_1$ :	6
$F_a$ :	1.3	PGA :	0.21
$F_v$ :	1.5	PGA <sub>w</sub> :	0.252
$S_{MS}$ :	0.633	$F_{PGA}$ :	1.2
$S_{M1}$ :	0.24	$I_a$ :	1
$S_{M2}$ :	0.422	$C_s$ :	0.925



Data Accessed: Thu Oct 24 2024

Date Source:

USGS Seismic Design Maps based on ASCE/SEI 7-16 and ASCE/SEI 7-16 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-16 Ch. 21 are available from USGS.



## Ice

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### Results:

Ice Thickness:	0.25 in.
Concurrent Temperature:	15 F
Gust Speed:	30 mph

**Data Source:** Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8

**Date Accessed:** Thu Oct 24 2024

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

In the mountain west, ice thicknesses may exceed the mapped values in the foothills and passes. However, at elevations above 5,000 ft, freezing rain is unlikely.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

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**STRUCTURAL CALCULATIONS**  
for  
**NM01-148 SPIKE**  
at  
**221 NEW MEXICO 165**  
**PLACITAS, NM 87043**  
for  
**PINNACLE CONSULTING, INC.**  
&  
**RAYCAP (SS24-01302H-00R1)**



**BY: JACOB PROCTOR, P.E.**  
**PROFESSIONAL ENGINEER**

**PROJECT #: U0142.2054.242**

**DATE: October 24, 2024**

**DESIGNED BY MAR; CHECKED BY KJG**

**Note:**

*The calculations presented in this package are intended for a single use at the location indicated above, for the client listed above. These calculations shall not be reproduced, reused, "card filed", sold to a third party, or altered in any way without the written authorization of Vector Structural Engineering, LLC and Raycap.*

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JOB NO.: U0142.2054.242

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PROJECT: NM01-148 SPIKE

**Design Criteria:**

- Code:** Structural design is based on the 2021 New Mexico Commercial Building Codes (2021 IRC) and the TIA-222-H standard.
- Wind:** Basic wind speed = 104 mph (5-second gust) per the TIA-222-H standard  
 Risk Category: II  
 Wind exposure: C  
 Topographic category: 1  
 Crest height: 0 ft
- Ice:** 0.25" radial ice @ 30 mph basic wind speed (5-second gust) per the TIA-222-H standard
- Seismic:** Seismic importance factor,  $I = 1$   
 Risk Category: II  
 Mapped spectral response accelerations:  $S_S = 0.487g$   $S_1 = 0.16g$   
 Site class: C  
 Spectral response coefficients:  $S_{LH} = 0.422g$   $S_{M1} = 0.16g$   
 Seismic design category: C  
 Basic seismic force-resisting-system: Telecom: Steel Pole  
 Seismic base shear:  $V = 5.17 k$   
 Seismic response coefficient,  $C_s = 0.222$   
 Response modification factor:  $R = 1.5$   
 Analysis procedure: Equivalent Lateral Force

**General Notes:**

- 1 The contractor shall verify dimensions, conditions and elevations before starting work. The engineer shall be notified immediately if any discrepancies are found.
- 2 The typical notes and details shall apply in all cases unless specifically detailed elsewhere. Where no detail is shown, the construction shall be as shown for other similar work and as required by the building code.
- 3 These calculations are limited to the structural members shown in these calculations only.
- 4 The contractor shall be responsible for compliance with local construction safety orders. Approval of shop drawings by the architect or structural engineer shall not be construed as accepting this responsibility.
- 5 All structural framing members shall be adequately shored and braced during erection and until full lateral and vertical support is provided by adjoining members.



JOB NO.: U0142.2054.242

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PROJECT: NMD1-148 SPIKE

### Structural Steel:

- 1 All structural steel code checks based on the AISC 15th Edition per the TIA-222-H standard
- 2 All 18-sided, tapered shaft steel to be per ASTM A572 GR. 65, U.N.O.
- 3 The design length of slip splices is equal to 1.67 times the inside width of the base of the upper section. Slip splice length tolerance is equal to  $\pm 10\%$  of the design slip splice length.
- 4 All steel pipe to be per ASTM A500 GR. B (42 KSI), U.N.O.
- 4 All steel round tubes (HSS) to be per U.N.O.
- 5 All steel rectangular tubes (HSS) to be per ASTM A500 GR. B (46 KSI), U.N.O.
- 5 All steel wide flange shapes to be per U.N.O.
- 6 All other structural steel shapes & plates shall be per ASTM A36, U.N.O.
- 7 All anchor bolts shall be per ASTM A615 GR. 75, U.N.O.
- 8 All bolts for steel-to-steel connections shall be per ASTM F3125 GR. A325 U.N.O.
- 9 All bolted connections shall be tightened per the 'turn-of-nut' method as defined by AISC.
- 10 All welding shall be performed by certified welders in accordance with the latest edition of the American Welding Society (AWS) D1.1. Utilize minimum E70XX low-hydrogen electrode if U.N.O. or where higher strength electrode is required by AWS D1.1.
- 11 All steel surfaces shall be galvanized in accordance with ASTM A123 and ASTM F2329 standards, thoroughly coated with a zinc-rich primer, or otherwise protected as noted on the structural drawings.

### Fiberglass Reinforced Plastic (FRP):

- 1 All structural shapes shall be Bedford Reinforced Plastics produced using the pultrusion process.
- 2 The fabricator and contractor shall exercise precautions necessary to protect the fiberglass pultruded structural shapes from abuse to prevent breakage, nicks, gouges, etc. during fabrication, handling, and installation.
- 3 Structural shapes shall be fabricated and assembled as indicated on the design drawings.
- 4 FRP threaded rods and nuts shall be tightened to snug tight and turned an additional 1/2 turn and locked with epoxy.

### Foundation / Concrete:

- 1 All concrete mixing, placement, forming, and reinforcing installation shall be performed in accordance with the requirements of "Building Code Requirements for Reinforced Concrete", ACI 318-19. Foundation installation shall be in accordance with the requirements of "Standard Specifications for the Construction of Drilled Piers", ACI 308, latest edition.
- 2 All concrete shall have a minimum compressive strength of 4000 psi at 28 days.
- 3 Cement for all concrete shall be II with 6% (+/- 1.5%) entrained air. Maximum aggregate size shall be 3/4".
- 4 Reinforcing steel shall be per ASTM A615 Gr. 60, U.N.O.
- 5 Foundation design is based upon the project soils report prepared by:

Contact: Tower Engineering Professionals, Inc.  
 Report No: 341545  
 Date: 31-Jul-24



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PROJECT: MM01-148 Spine

**DESIGN WIND LOADS ON LARGE RADOME CONCEALMENTS:**  
 (Screens for Concealments on Monopoles)

Round Concealment Calculations  
 Supported on a Pole structure  
 Design per: IA-222-H

Level: Concealment tower

**INPUT DATA:**

Basic Wind Speed, V (mph): 104  
 Exposure Category: C  
 Elevation Above Sea Level (ft): 5520

**Structure:**

Supporting Structure: Pole  
 Concealment Shape: Round  
 Tower Top or Steel (ft): 75  
 # of Concealments: 3

	Top	2nd	Bottom
Elevation Centerline (ft):	70	50	50
Concealment Height (ft):	10.0	10.0	10.0
Concealment Diameter (ft):	18.0	18.0	18.0
Open Area Top (%):	100%	0%	0%
Open Area Bottom (%):	0%	0%	100%

**WIND DESIGN SUMMARY:**

	70 ft	60 ft	50 ft
Full Wind Pressure, 1.0W (psf):	17.5	18.9	16.3
Full Ice Wind Pressure, 1.0W (psf):	2.8	2.8	2.7
Full Service Wind Pressure, 1.0W (psf):	5.8	5.5	5.4
Inside Wind Pressure, 1.0W (psf):	21.0	20.3	19.6
Inside Ice Wind Pressure, 1.0W (psf):	3.5	3.4	3.3
Inside Service Wind Pressure, 1.0W (psf):	7.0	6.8	6.6
Wind Force, Outside Face (lbs):	3151	3051	2936
Wind Force, Inside Face (lbs):	2228	0	2075
Total Wind Force (lbs):	5379	3051	5011



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PROJECT: NM01-148 Spike

**WEIGHT DESIGN SUMMARY:**

**Self Weight Only:**

	Component:	Densities		Length, Area, Quantity		Self Weight (lb)(Total = 10% lb)	
Top @ 73 Elevation	ESSV Panel:	2.00	psf	Area = ft <sup>2</sup>	565	1131	2084
	Framing w/o Grating	3.0	psf	Area = ft <sup>2</sup>	254	763	
22d @ 60 Elevation	ESSV Panel:	2.00	psf	Area = ft <sup>2</sup>	565	1131	2084
	Framing w/o Grating	3.0	psf	Area = ft <sup>2</sup>	254	763	
Bottom @ 50 Elevation	ESSV Panel:	2.00	psf	Area = ft <sup>2</sup>	565	1131	2084
	Framing w/o Grating	3.0	psf	Area = ft <sup>2</sup>	254	763	
						<b>W<sub>s</sub> =</b>	<b>6251</b>

**Ice Weight Only:**

	Component:	Ice Density		Length, Area		Ice Weight (lb) Total Weight (lb)	
Top @ 70' Elevation	ESSV Panel:	1.3	psf	Area = ft <sup>2</sup>	565	711	1031
	Framing w/o Grating	1.3	psf	Area = ft <sup>2</sup>	254	320	
22d @ 60 Elevation	ESSV Panel:	1.3	psf	Area = ft <sup>2</sup>	565	711	1031
	Framing w/o Grating	1.3	psf	Area = ft <sup>2</sup>	254	320	
Bottom @ 50 Elevation	ESSV Panel:	1.3	psf	Area = ft <sup>2</sup>	565	711	711
	Framing w/o Grating	1.3	psf	Area = ft <sup>2</sup>	0	0	
						<b>W<sub>i</sub> =</b>	<b>2774</b>

**Total W<sub>s</sub> = 9025**



JOB NO.: U2142.0054.042

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PROJECT: N401 - 140 SPIRE

ASCE 7-16

**Seismic Base Shear Calculations:**

Seismic Parameters:

Risk Category	I
Seismic Design Category	C
Importance I	1.00
Site Class	C
$R_w$	1.5
$T_w$	K

$S_s$	0.407	g
$F_a$	0.160	
$S_{M1}$	0.993	
$S_{M2}$	0.240	

$S_{M3}$	0.442	g
$S_{M4}$	0.170	g
$I_e$	1.50	
$F_p$	1.50	

Seismic Base Shear:

Structure Type	Telecom: Steel Pole	
Period Type	Wind Base Cx	
$h$	74.0	ft
$W$	2500	kip

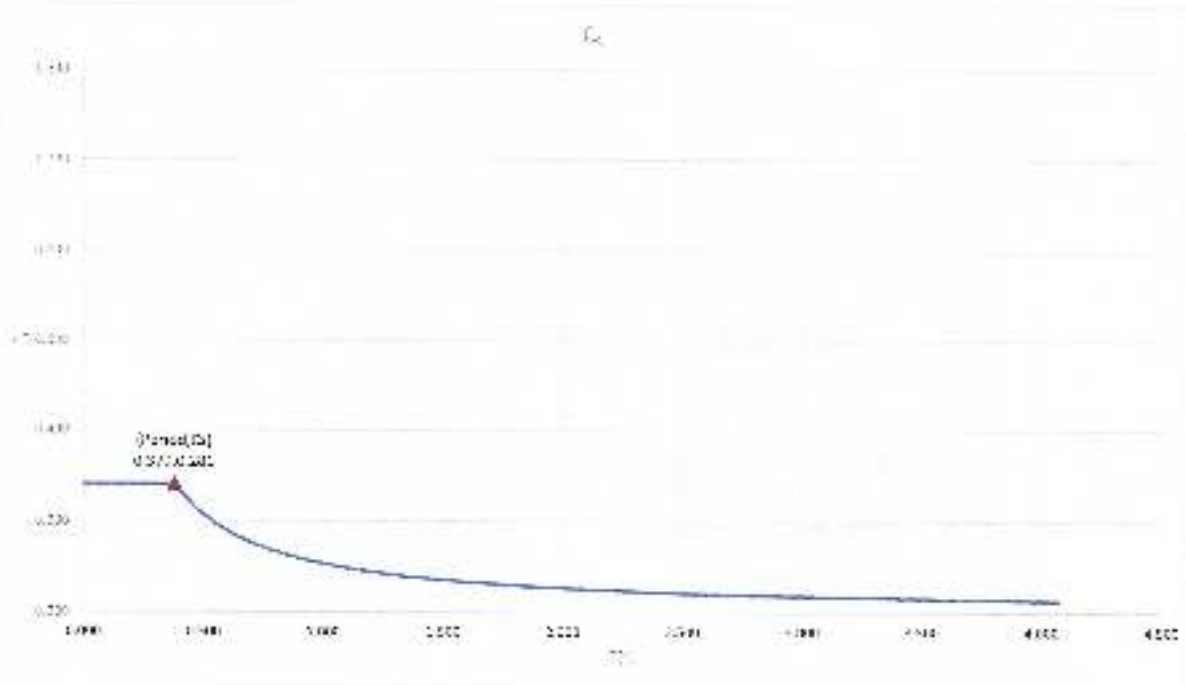
$W_1$	18.0	k
$W_2$	19.0	k

$T_p$	2.54	sec
$T_s$	0.91	sec
$k_p$	1.50	

$T_p^*$	0.252	
Seismic Shear, $V_{base}$	3.3	k
Wind Shear	15.6	k

ratio = 0.21

Wind Controls, No Seismic Analysis Required





<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W. Coloma Park Blvd Denver, CO 80220 Phone: (303) 999-1773 Fax: (303) 999-1776	<b>Job</b> Soike	<b>Page</b> 8 of 131
	<b>Project</b> U0142.2054.242	<b>Date</b> 17:04:43 10/24/24
	<b>Client</b> Raycap	<b>Designed by</b> mrine

## Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-F standard.

The following design criteria apply:

- Tower is located in Sandoval County, New Mexico
- Tower base elevation above sea level: 5521.00 ft.
- Basic wind speed of 104 mph.
- Risk Category II.
- Exposure Category C.
- Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- Topographic Category: 1
- Crest Height: 0.00 ft.
- Nominal ice thickness of 0.2500 in.
- Ice thickness is considered to increase with height.
- Ice density of 56pcf.
- A wind speed of 30 mph is used in combination with ice.
- Deflections calculated using a wind speed of 60 mph.
- Non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in pole design is 1.
- Local bending stresses due to climbing loads, feed line supports, and appearance mounts are not considered.

## Options

- |  |   |  |
|--|---|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Last</li> <li>Consider Moments - Horizontal</li> <li>Consider Moments - Diagonal</li> <li>Use Moment Magnifier - 1.0</li> <li>Use Code Snow Loads</li> <li>Use Code Safety Factors - Girts Escalate for</li> <li>Always Use Max Ice</li> <li>Kz to Exposure D Hurricane Region</li> <li>Include Belts to Member Capacity</li> <li>Leg Belts Are At End of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sides)</li> <li>SR Members Have Curves</li> <li>SR Members Are Concentric</li> <li>Distribute Leg Loads As Uniform</li> <li>Use Special Wind Profile</li> </ul> | <ul style="list-style-type: none"> <li>Assume Legs Curved</li> <li>Use Agrate Ring Taper Plate</li> <li>Use Clear Spans For Wind Area</li> <li>Use Clear Spans For K1-F</li> <li>Revanon Gaps To Initial Tension</li> <li>Dynes Mast Stability Checks</li> <li>Use Azimuth Dish Coefficients</li> <li>Project Wind Area of Appendages</li> <li>Alternative Append - EPA Calculation</li> <li>Assemble Taper Ann Area</li> <li>Add IBC 601W Combination</li> <li>Set Capacity Regions By Component</li> <li>Triangular Diamond Inner Bracing</li> <li>Use Feed Line Bundles As Cylinder</li> <li>Ignore K1-F For 90 Deg. Angle Legs</li> <li>Use AsC10 X-Brace by Rules</li> </ul> | <ul style="list-style-type: none"> <li>Calculate Buckling of Bracing Towers</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable Offset Girt At Foundation</li> <li>Consider Feed Line Tension</li> <li>Include Angle Block Shear Check</li> <li>Use TIA 222-H Bracing Resist Assumption</li> <li>Use TIA 222-H Tension Ice Assumption</li> <li><b>Dates</b></li> <li>Include Snow-Tension Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mount of Sockets</li> <li>Pole Without Lines Attachments</li> <li>Pole With Strapped Or No Appendages</li> <li>Outside and Inside Corner Radii Are Known</li> </ul> |
|--|---|--|

## Tapered Pole Section Geometry

Section	Alternate	Snow Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Round Radius	Pole Grade
	<i>f<sub>i</sub></i>	<i>f<sub>s</sub></i>	<i>f<sub>l</sub></i>		in	in	in	in	
I.1	75.00-25.00	50.00	4.25	18	31.000	30.750	0.1875	0.2500	A572-58 105 ksi
I.2	25.00-1.00	15.25		18	29.140	30.070	0.2500	1.0000	A572-58 (65 ksi)

<b>tnxTower</b> <b>Vector Structural Engineering</b> 651 W. Colono Park Blvd Chicago, IL 60636 Phone: (861) 990-1775 FAX: (861) 990-1776	Job	Spike	Page	3 of 131
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	Client	Raycap	Designed by	mrrle

### Tapered Pole Properties

Section	Top Dia. in	Area in <sup>2</sup>	$I$ in <sup>4</sup>	$r$ in	$I_x$ in <sup>4</sup>	$I_y$ in <sup>4</sup>	$J$ in <sup>4</sup>	$I_{xx}$ in <sup>4</sup>	$I_{yy}$ in <sup>4</sup>	$X$ in	$Y$ in
L1	21.2500	12.3860	677.8263	7.3881	10.5630	63.5383	1195.34-4	6.1947	3.5594		12.952
	31.9200	18.485	2175.4080	10.8157	15.5210	137.4033	4795.6405	9.0994	5.0830		22.174
L2	33.8050	25.2466	3520.6563	10.4907	15.7053	167.9401	3644.7089	11.6235	4.7561		19.14
	35.2572	27.6178	4325.7766	12.5338	17.9791	247.5346	4459.1149	13.8113	5.1291		22.919

Tower Elevation	Gusset Area (sq. ft.)	Gusset Thickness	Gusset Grade	Adapt. Factor $K_1$	Adapt. Factor $K_2$	Height (ft)	Double Angle Satch. Deb. Spacing Diagonals in	Double Angle Satch. Deb. Spacing Horizontal in	Double Angle Satch. Deb. Spacing Vertical in
ft	ft <sup>2</sup>	in							
L1 75.00-77.00									
L2 25.00-31.00									

### User Defined Loads

Description	Elevation ft	Offset from Centerline ft	Vertical Angle °	No. Ice	Height ft	$F_x$		$F_y$		$C_{ex}$
						lb	lb	lb	lb	
Concrete Loading @ 75 ft	75.00	0.00	0.0000	No Ice	1947.00	0.00	0.00	2670.00	90.64	
				Ice	516.00	0.00	0.00	353.00	142.89	
				Service	1342.00	0.00	0.00	895.00	106.48	
Concrete Loading @ 55 ft	55.00	0.00	0.0000	No Ice	1947.00	0.00	0.00	2670.00	93.31	
				Ice	516.00	0.00	0.00	353.00	147.99	
				Service	1347.00	0.00	0.00	895.00	109.73	
Concrete Loading @ 55 ft	55.00	0.00	0.0000	No Ice	1947.00	0.00	0.00	1557.00	53.90	
				Ice	516.00	0.00	0.00	254.00	105.88	
				Service	1342.00	0.00	0.00	508.00	62.28	
Concrete Loading @ 55 ft	55.00	0.00	0.0000	No Ice	1342.00	0.00	0.00	1523.00	51.79	
				Ice	516.00	0.00	0.00	251.00	109.67	
				Service	1347.00	0.00	0.00	505.00	61.51	
Concrete Loading @ 55 ft	55.00	0.00	0.0000	No Ice	1947.00	0.00	0.00	2576.00	90.04	
				Ice	516.00	0.00	0.00	351.00	142.92	
				Service	1342.00	0.00	0.00	84.00	105.91	
Concrete Loading @ 15 ft	15.00	0.00	0.0000	No Ice	1347.00	0.00	0.00	1576.00	93.92	
				Ice	516.00	0.00	0.00	351.00	149.09	
				Service	1342.00	0.00	0.00	84.00	110.48	

### Discrete Tower Loads

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 2 <sup>nd</sup> Calumet Park Blvd Chicago, IL 60670 Phone: (800) 960-1220 FAX: (800) 960-1226	Job	Spiko	Page 10 of 131
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Description	Face or Leg	Offset Type	Offset From Local Face	Allowance Adjustment	Placement		C.A. From		Weight
					X	Y	Z	Z	
(4) Generic Panel (Enclosed, 115 lbs)	A	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	115.00 115.00
(4) Generic Panel (Enclosed, 115 lbs)	B	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	115.00 115.00
(4) Generic Panel (Enclosed, 115 lbs)	C	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	115.00 115.00
(2) 10'-0" T-arm EPA - 5.7 ft <sup>2</sup> (61 lbs)	A	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	161.00 561.25
(2) 10'-0" T-arm EPA - 5.7 ft <sup>2</sup> (61 lbs)	B	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	161.00 561.25
(2) 10'-0" T-arm EPA - 5.7 ft <sup>2</sup> (61 lbs)	C	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	161.00 561.25
(4) Generic RRU (Enclosed, 75 lbs)	A	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	B	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	C	From Face	3.00 0.00 0.00	0.0000	70.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	75.00 75.00
***									
(4) Generic Panel (Enclosed, 113 lbs)	A	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	113.00 113.00
(4) Generic Panel (Enclosed, 113 lbs)	B	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	113.00 113.00
(4) Generic Panel (Enclosed, 113 lbs)	C	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	113.00 113.00
(2) 10'-0" T-arm EPA - 5.7 ft <sup>2</sup> (61 lbs)	A	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	161.00 561.25
(2) 10'-0" T-arm EPA - 5.7 ft <sup>2</sup> (61 lbs)	B	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	161.00 561.25
(2) 10'-0" T-arm EPA - 5.7 ft <sup>2</sup> (61 lbs)	C	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	161.00 561.25
(4) Generic RRU (Enclosed, 75 lbs)	A	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	B	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	75.00 75.00
(4) Generic RRU (Enclosed, 75 lbs)	C	From Face	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice	0.00 0.00	0.00 0.00	75.00 75.00
***									
(4) Generic Panel (Enclosed, 112 lbs)	A	From Face	3.00	0.0000	50.00	No Ice	0.00	0.00	112.00

<b>taxTower</b> <b>Vector Structural Engineering</b> 601 W. Galena Park Blvd League City, TX 77409 Phone: (281) 936-1773 FAX: (281) 993-1776	Job	Spike	Page 11 of 131
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	Client	Raycap	Designed by
			mritie

Description	Face or Leg	Offset Type	Offset Floor Level	Length Adjustment	Placement	Cl. Adj. Front	Cl. Adj. Side	Weight
				$\alpha$	$\beta$	$\beta^x$	$\beta^y$	lb
(5 lbs)			0.00		12' Ice	0.00	0.00	115.00
			0.00					
(4) Generic Panel (Enclosed, 115 lbs)	D	From Face	3.00	0.0000	50.00	No Ice	0.00	115.00
			0.00		12' Ice	0.00	0.00	115.00
			0.00					
(4) Generic Panel (Enclosed, 115 lbs)	C	From Face	3.00	0.0000	50.00	No Ice	0.00	115.00
			0.00		12' Ice	0.00	0.00	115.00
			0.00					
(2) 10'x7' 1-in. EPA = 5.7 lb'2 (15 lbs)	A	From Face	3.00	0.0000	50.00	No Ice	0.00	161.00
			0.00		12' Ice	0.00	0.00	361.36
			0.00					
(2) 10'x7' 1-in. EPA = 5.7 lb'2 (15 lbs)	H	From Face	3.00	0.0000	50.00	No Ice	0.00	161.00
			0.00		12' Ice	0.00	0.00	361.36
			0.00					
(2) 10'x7' 1-in. EPA = 5.7 lb'2 (15 lbs)	C	From Face	3.00	0.0000	50.00	No Ice	0.00	161.00
			0.00		12' Ice	0.00	0.00	361.36
			0.00					
(4) Generic RRU (Flat roof, 75 lbs)	A	From Face	3.00	0.0000	50.00	No Ice	0.00	75.00
			0.00		12' Ice	0.00	0.00	75.00
			0.00					
(4) Generic RRU (Flat roof, 75 lbs)	B	From Face	3.00	0.0000	50.00	No Ice	0.00	75.00
			0.00		12' Ice	0.00	0.00	75.00
			0.00					
(4) Generic RRU (Flat roof, 75 lbs)	C	From Face	3.00	0.0000	50.00	No Ice	0.00	75.00
			0.00		12' Ice	0.00	0.00	75.00
			0.00					

### Tower Pressures - No Ice

G<sub>w</sub> = 1.00

System Elevation	$z$	$A_{ref}$	$z_p$	$A_{ex}$	$K_{zt}$	$G_{z, s}$	$G_{z, e}$	$G_{z, p}$	Exp %	Calc. In. Press. $h'$	Calc. Out. Press. $h'$
$h'$	$h'$		$z_p'$	$h'$		$\beta^x$	$\beta^y$	$\beta^z$			
11.95.20-25.04	19.10	1.890	2'	109.355		0.300	109.355	109.355	100.00	0.000	0.000
						0.700	109.355	109.355	100.00	0.000	0.000
						0.700	109.355	109.355	100.00	0.000	0.000
12.25.04-1.00	12.77	0.850	15'	66.362		0.300	66.362	66.362	100.00	0.000	0.000
						0.700	66.362	66.362	100.00	0.000	0.000
						0.300	66.362	66.362	100.00	0.000	0.000

### Tower Pressure - With Ice

G<sub>w</sub> = 1.00

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd League City, TX 77505 Phone: (281) 936-1777 FAX: (281) 936-1776	Job	Spike	Page 12 of 13
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	Client	Raycap	Designed by
			mrie

Section Elevation	$z$	$K_z$	$g$	$z$	$A_x$	$F$	$A_z$	$A_y$	$A_{xy}$	Leg %	$C_{dA}$ in Face $\mu^2$	$C_{dA}$ Out Face $\mu^2$
$\beta$	$\beta$		$g$	$z$	$\beta$	$\mu$	$\beta$	$\beta$	$\beta$		$\mu^2$	$\mu^2$
L. 75.00-25.00	49.10	1.090	2	0.2900	111.523	A	0.000	111.523	111.523	100.00	0.000	0.000
						B	0.000	111.523		100.00	0.000	0.000
						C	0.000	111.523		100.00	0.000	0.000
L. 25.00-1.00	12.91	0.850	2	0.2273	67.493	A	0.000	67.493	67.493	100.00	0.000	0.000
						B	0.000	67.493		100.00	0.000	0.000
						C	0.000	67.493		100.00	0.000	0.000

### Tower Pressure - Service

$G_e = 1.00$

Section Elevation	$z$	$K_z$	$g$	$A_x$	$F$	$A_z$	$A_y$	$A_{xy}$	Leg %	$C_{dA}$ in Face $\mu^2$	$C_{dA}$ Out Face $\mu^2$
$\beta$	$\beta$		$g$	$\beta$	$\mu$	$\beta$	$\beta$	$\beta$		$\mu^2$	$\mu^2$
L. 75.00-25.00	49.10	1.090	2	109.533	A	0.000	109.533	109.533	100.00	0.000	0.000
					B	0.000	109.533		100.00	0.000	0.000
					C	0.000	109.533		100.00	0.000	0.000
L. 25.00-1.00	12.91	0.850	2	66.362	A	0.000	66.362	66.362	100.00	0.000	0.000
					B	0.000	66.362		100.00	0.000	0.000
					C	0.000	66.362		100.00	0.000	0.000

### Tower Forces - No Ice - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	$F$	$z$	$C_v$	$g$	$D_x$	$D_y$	$A_x$	$F$	$z$	Crit. Face
$\beta$	$\beta$	$\beta$	$\mu$	$z$	$g$	$g$	$\mu$	$\mu$	$\beta$	$\mu$	$g$	$\mu$
L. 75.00-25.00	0.00	2600.97	A	1	0.73	24	1	1	109.533	2151.37	43.05	C
			B	1	0.73		1	1	109.533			
			C	1	0.73		1	1	109.533			
L. 25.00-1.00	0.00	2444.77	A	1	0.73	19	1	1	66.362	1027.03	43.79	C
			B	1	0.73		1	1	66.362			
			C	1	0.73		1	1	66.362			
Sum Weight	0.00	5045.74					0.113		175908.37	3178.39		

### Tower Forces - No Ice - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	$F$	$z$	$C_v$	$g$	$D_x$	$D_y$	$A_x$	$F$	$z$	Crit. Face
$\beta$	$\beta$	$\beta$	$\mu$	$z$	$g$	$g$	$\mu$	$\mu$	$\beta$	$\mu$	$g$	$\mu$
L. 75.00-25.00	0.00	2600.97	A	1	0.73	24	1	1	109.533	2151.37	43.05	C
			B	1	0.73		1	1	109.533			
			C	1	0.73		1	1	109.533			
L. 25.00-1.00	0.00	2444.77	A	1	0.73	19	1	1	66.362	1027.03	43.79	C

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 651 W. Watson Park Blvd Denver, CO 80202 Phone: (303) 994-1775 FAX: (303) 994-1776	Job	Spike	Page 13 of 131
	Project	U0142 2054.242	Date 17:04:43 10/24/24
	Client	Raycap	Designed by mriine

Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	qx	Dx	Dy	Ax	F	v	Ctrl. Face
ft	lb	lb	c			psf			ft <sup>2</sup>	lb	psf	
Sum Weight:	0.00	5043.74	D C	1 1	0.73 0.73		1		OTM 113508.37 lb-ft	1178.70		

**Tower Forces - No Ice - Wind 60 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	qx	Dx	Dy	Ax	F	v	Ctrl. Face
ft	lb	lb	c			psf			ft <sup>2</sup>	lb	psf	
1.1 75.00-25.00	0.00	2600.97	A J C	1 1 1	0.73 0.73 0.73	24	1	1	109.355 109.355 109.355	2131.37	43.03	C
1.2 25.00-1.00	0.00	2442.77	A H C	1 1 1	0.73 0.73 0.73	19	1	1	66.362 66.362 66.362	1021.02	12.79	C
Sum Weight:	0.00	5043.74							OTM 113508.37 lb-ft	3178.39		

**Tower Forces - No Ice - Wind 90 To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	qx	Dx	Dy	Ax	F	v	Ctrl. Face
ft	lb	lb	c			psf			ft <sup>2</sup>	lb	psf	
1.1 55.00-25.00	0.00	2600.97	A B C	1 1 1	0.73 0.73 0.73	24	1	1	109.355 109.355 109.355	2131.37	43.03	C
1.2 25.00-1.00	0.00	2442.77	A B C	1 1 1	0.73 0.73 0.73	19	1	1	66.362 66.362 66.362	1021.02	12.79	C
Sum Weight:	0.00	5043.74							OTM 113508.37 lb-ft	3178.39		

**Tower Forces - With Ice - Wind Normal To Face**

Section Elevation	Add Weight	Self Weight	F a c e	e	Cx	qx	Dx	Dy	Ax	F	v	Ctrl. Face
ft	lb	lb	c			psf			ft <sup>2</sup>	lb	psf	
1.1 75.00-73.00	0.00	3020.55	A B C	1 1 1	1.0 1.0 1.0	2	1	1	11.521 11.521 11.521	300.17	6.10	C

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W. Collins Park Blvd Denver, CO 80202 Phone: (303) 998-1775 FAX: (303) 998-1776	Job	Page 14 of 131
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	Client	U0142.2054.242
	Raycap	Date 17:04:43 10/24/24
		Designed by mirie

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	q <sub>s</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>c</sub>	F	v	Corl Face
z	lb	lb	ft	ft	psf	psf			ft <sup>2</sup>	lb	psf	
L1 25.00-1.00	0.00	2666.54	A	1	1.2	2	1		67.271	142.40	5.93	C
			B	1	1.2		1		67.271			
			C	1	1.2		1		67.271			
Sum Weight	0.00	2666.54					OTM		16102.78 lb-ft	442.31		

**Tower Forces - With Ice - Wind 45 To Face**

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	q <sub>s</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>c</sub>	F	v	Corl Face
z	lb	lb	ft	ft	psf	psf			ft <sup>2</sup>	lb	psf	
L1 75.00-25.00	0.00	1020.56	A	1	1.2	2	1		111.523	300.11	6.00	C
			B	1	1.2		1		111.523			
			C	1	1.2		1		111.523			
L2 25.00-1.00	0.00	2666.54	A	1	1.2	2	1		67.271	142.40	5.93	C
			B	1	1.2		1		67.271			
			C	1	1.2		1		67.271			
Sum Weight	0.00	2666.54					OTM		16102.78 lb-ft	442.31		

**Tower Forces - With Ice - Wind 60 To Face**

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	q <sub>s</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>c</sub>	F	v	Corl Face
z	lb	lb	ft	ft	psf	psf			ft <sup>2</sup>	lb	psf	
L1 75.00-25.00	0.00	1020.56	A	1	1.2	2	1		111.523	300.11	6.00	C
			B	1	1.2		1		111.523			
			C	1	1.2		1		111.523			
L2 25.00-1.00	0.00	2666.54	A	1	1.2	2	1		67.271	142.40	5.93	C
			B	1	1.2		1		67.271			
			C	1	1.2		1		67.271			
Sum Weight	0.00	2666.54					OTM		16102.78 lb-ft	442.31		

**Tower Forces - With Ice - Wind 90 To Face**

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	q <sub>s</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>c</sub>	F	v	Corl Face
z	lb	lb	ft	ft	psf	psf			ft <sup>2</sup>	lb	psf	
L1 75.00-25.00	0.00	1020.56	A	1	1.2	2	1		111.523	300.11	6.00	C
			B	1	1.2		1		111.523			

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd. Denver, CO 80246 Phone: (801) 999-1775 FAX: (801) 999-1776	Job	Spike	Page 15 of 131
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	Client	Raycap	Designed by mrlite

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	g <sub>x</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>x</sub>	F	v	Ctrl. Face
<i>h</i>	<i>w</i>	<i>w</i>	<i>c</i>	<i>c</i>		<i>pdf</i>			<i>h'</i>	<i>w</i>	<i>pdf</i>	
L1 25.00-31.00	0.00	2650.54	A	1	1.2	2	1	1	11.563	149.49	5.95	C
			B	1	1.2				67.271			
			C	1	1.2				67.271			
Sum Weight:	0.00	3687.10					0.113		1302.78	142.51		

### Tower Forces - Service - Wind Normal To Face

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	g <sub>x</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>x</sub>	F	v	Ctrl. Face
<i>h</i>	<i>w</i>	<i>w</i>	<i>c</i>	<i>c</i>		<i>pdf</i>			<i>h'</i>	<i>w</i>	<i>pdf</i>	
L1 75.00-75.00	0.00	2900.97	A	1	0.73	7	1	1	109.355	608.56	12.17	C
			B	1	0.73				109.355			
			C	1	0.73				109.355			
L2 25.00-31.00	0.00	2444.77	A	1	0.73	5	1	1	66.367	793.54	12.11	C
			B	1	0.73				66.362			
			C	1	0.73				66.362			
Sum Weight:	0.00	5345.74					0.113		32678.46	499.21		

### Tower Forces - Service - Wind 45 To Face

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	g <sub>x</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>x</sub>	F	v	Ctrl. Face
<i>h</i>	<i>w</i>	<i>w</i>	<i>c</i>	<i>c</i>		<i>pdf</i>			<i>h'</i>	<i>w</i>	<i>pdf</i>	
L1 75.00-75.00	0.00	2600.97	A	1	0.73	7	1	1	109.355	508.65	12.17	C
			B	1	0.73				109.355			
			C	1	0.73				109.355			
L2 25.00-31.00	0.00	2444.77	A	1	0.73	5	1	1	66.367	293.56	12.11	C
			B	1	0.73				66.362			
			C	1	0.73				66.362			
Sum Weight:	0.00	5045.74					0.113		32678.56	899.21		

### Tower Forces - Service - Wind 60 To Face

Section Elevation	Add Weight	Self Weight	F <sub>x</sub>	F <sub>y</sub>	C <sub>x</sub>	g <sub>x</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>x</sub>	F	v	Ctrl. Face
<i>h</i>	<i>w</i>	<i>w</i>	<i>c</i>	<i>c</i>		<i>pdf</i>			<i>h'</i>	<i>w</i>	<i>pdf</i>	
L1	0.00	2600.97	A	1	0.73	7	1	1	109.355	508.65	12.17	C

<b>inxTower</b> <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd Denver, CO 80220 Phone: (303) 930-1775 Fax: (303) 930-1776	Job	Page 16 of 131
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	Spike	
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	Raycap	mirrie

Section Elevation	Add Weight	Self Weight	A	e	C <sub>x</sub>	a <sub>x</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>x</sub>	F	W	Cent. Face
ft	lb	lb	ft	ft		psf			ft	lb	psf	
75.00-75.00			A	1	0.77		1	1	109.355			
			C	1	0.77				109.355			
12.25.00-1.00	0.00	2445.77	A	1	0.73	7	1	1	66.362	290.56	12.11	C
			B	1	0.73				66.362			
			C	1	0.73				66.362			
Sum Weight:	0.00	2645.74						OTM	32573.95	899.21		
									5-C			

### Tower Forces - Service - Wind 90 To Face

Section Elevation	Add Weight	Self Weight	A	e	C <sub>x</sub>	a <sub>x</sub>	D <sub>x</sub>	D <sub>y</sub>	A <sub>x</sub>	F	W	Cent. Face
ft	lb	lb	ft	ft		psf			ft	lb	psf	
1.75.00-25.00	0.00	2645.97	A	1	0.73	7	1	1	109.355	608.67	12.17	C
			D	1	0.73				109.355			
			C	1	0.73				109.355			
17.25.00-1.00	0.00	2445.77	A	1	0.73	3	1	1	66.362	290.56	12.11	C
			B	1	0.73				66.362			
			C	1	0.73				66.362			
Sum Weight:	0.00	2645.74						OTM	32678.95	896.21		
									1-40			

### Discrete Appurtenance Pressures - No Ice G<sub>HI</sub> = 1.100

Description	Along Row	Weight	Offset	Offset	H	R	γ	C <sub>pe</sub> Front	C <sub>pe</sub> Side
	ft	lb	ft	ft	ft		psf	ft	ft
Generic Panel (Enclosed, 115 lbs)	500.0000	460.00	-3.39	-1.96	70.00	1.174	27	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.40	-1.96	70.00	1.174	27	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	3.07	70.00	1.174	27	0.00	0.00
12'-0" Trans EPA = 5.7 ft <sup>2</sup> (161 lbs)	300.0000	161.00	-3.39	-1.96	70.00	1.174	27	0.00	0.00
12'-0" Trans EPA = 5.7 ft <sup>2</sup> (151 lbs)	60.0000	322.00	3.39	-1.96	70.00	1.174	27	0.00	0.00
12'-0" Trans EPA = 5.7 ft <sup>2</sup> (151 lbs)	180.0000	161.00	0.00	3.92	70.00	1.174	27	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	400.0000	200.00	-3.39	-1.96	70.00	1.174	27	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	400.00	3.39	-1.96	70.00	1.174	27	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	200.00	0.00	3.00	70.00	1.174	27	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-3.46	-2.00	60.00	1.157	26	0.00	0.00
Generic Panel (Enclosed, 50 lbs)	50.0000	460.00	3.46	-2.00	60.00	1.157	26	0.00	0.00

<b>tuxTower</b> <b>Vector Structural Engineering</b> 601 W. Galena Park Blvd Denver, CO 80226 Phone: (303) 399-1775 Fax: (303) 396-1776	Job	Spike	Page 17 of 131
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	Client	Raycap	Designed by mnie

Description	Along Z-axis #	Weight #	Offset ft	Offset ft	e ft	$K_z$	$g_z$ pcf	Curtain Wind ft	Curtain Side ft <sup>2</sup>
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	4.08	60.00	1.157	25	0.00	0.00
10'-0" Term EPA = 5.7 R2 (151 lbs)	300.0000	322.00	-5.46	-2.00	60.00	1.197	26	0.00	0.00
10'-0" Term EPA = 5.7 R2 (151 lbs)	60.0000	322.00	5.46	-2.00	60.00	1.37	16	0.00	0.00
17'-0" Term EPA = 5.7 R2 (161 lbs)	180.0000	332.00	0.00	4.00	50.00	1.197	26	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.46	-2.00	60.00	1.185	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.46	-2.00	60.00	1.157	26	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	4.00	60.00	1.197	26	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-5.57	-2.00	50.00	1.094	25	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	5.57	2.00	50.00	1.094	25	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	4.08	50.00	1.094	25	0.00	0.00
10'-0" Term EPA = 5.7 R2 (161 lbs)	300.0000	322.00	-5.57	-2.00	50.00	1.094	25	0.00	0.00
10'-0" Term EPA = 5.7 R2 (151 lbs)	60.0000	322.00	5.57	-2.00	50.00	1.094	25	0.00	0.00
10'-0" Term EPA = 5.7 R2 (151 lbs)	180.0000	322.00	0.00	4.08	50.00	1.094	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-4.57	2.00	50.00	1.094	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	4.57	2.00	50.00	1.094	25	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	4.08	50.00	1.094	25	0.00	0.00
Sum Weight:		9758.00							

### Discrete Appurtenance Pressures - With Ice $G_n = 1.160$

Description	Along Z-axis #	Weight #	Offset ft	Offset ft	e ft	$K_z$	$g_z$ pcf	Curtain Wind ft	Curtain Side ft <sup>2</sup>	r ft
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-3.46	-1.96	70.00	1.174	2	0.00	0.00	0.2855
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.35	-1.96	50.00	1.174	2	0.00	0.00	0.2898
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	3.92	50.00	1.174	2	0.00	0.00	0.2895
17'-0" Term EPA = 5.7 R2 (161 lbs)	300.0000	754.52	3.29	-1.96	50.00	1.174	3	0.00	0.00	0.2695
10'-0" Term EPA = 5.7 R2 (161 lbs)	60.0000	754.52	3.39	-1.96	50.00	1.191	3	0.00	0.00	0.2695
10'-0" Term EPA = 5.7 R2 (151 lbs)	180.0000	754.52	0.00	3.92	50.00	1.174	2	0.00	0.00	0.2695
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.35	-1.96	50.00	1.174	2	0.00	0.00	0.2895
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.29	-1.96	50.00	1.174	2	0.00	0.00	0.2695
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	3.92	50.00	1.174	2	0.00	0.00	0.2695

<b>inxTower</b> <b>Vector Structural Engineering</b> 551 2 <sup>nd</sup> Galena Park Blvd Duane, TX 75026 Phone: (501) 993-1775 FAX: (501) 993-1776	Job	Page 18 of 131
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	Spike	
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	Raycap	mrlric

Description	Along x-axis "	Height ft	Offset ft	Offset ft	z ft	R <sub>z</sub>	q psf	C <sub>d</sub> - Front ft <sup>2</sup>	C <sub>d</sub> - Side ft <sup>2</sup>	A m
75 lbs) Generic Panel (Enclosed, 115 lbs)	300.0000	450.00	-3.46	-2.00	60.00	1.137	2	0.00	0.00	0.2653
Generic Panel (Enclosed, 115 lbs)	50.0000	460.00	3.46	-2.00	50.00	1.137	1	0.00	0.00	0.2654
Generic Panel (Enclosed, 115 lbs)	80.0000	460.00	0.00	-1.00	60.00	1.137	2	0.00	0.00	0.2654
10'-0" Term CPA - 5.7 602 (161 lbs)	300.0000	716.92	-3.46	-2.00	60.00	1.137	2	0.00	0.00	0.2653
17'-0" Term EPA - 5.7 802 (161 lbs)	50.0000	746.92	3.46	-2.00	50.00	1.137	1	0.00	0.00	0.2654
10'-0" Term EPA - 5.7 802 (161 lbs)	180.0000	746.92	0.00	-1.00	60.00	1.137	2	0.00	0.00	0.2654
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.46	-2.00	60.00	1.137	2	0.00	0.00	0.2653
Generic RRU (Enclosed, 75 lbs)	50.0000	300.00	3.46	-2.00	50.00	1.137	1	0.00	0.00	0.2653
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	-1.00	60.00	1.137	2	0.00	0.00	0.2654
Generic Panel (Enclosed, 115 lbs)	300.0000	560.00	-3.53	-2.00	50.00	1.094	2	0.00	0.00	0.2656
Generic Panel (Enclosed, 115 lbs)	50.0000	590.00	3.53	-2.00	50.00	1.094	1	0.00	0.00	0.2656
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	-1.00	50.00	1.094	2	0.00	0.00	0.2655
10'-0" Term EPA - 5.7 802 (161 lbs)	90.0000	739.24	3.53	-2.00	50.00	1.094	1	0.00	0.00	0.2655
10'-0" Term CPA - 5.7 602 (161 lbs)	60.0000	739.24	3.53	-2.00	50.00	1.094	2	0.00	0.00	0.2656
10'-0" Term EPA - 5.7 802 (161 lbs)	180.0000	739.24	0.00	-1.00	50.00	1.094	2	0.00	0.00	0.2656
Generic RRU (Enclosed, 75 lbs)	300.0000	90.00	-3.53	-2.00	50.00	1.094	1	0.00	0.00	0.2655
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.53	-2.00	50.00	1.094	2	0.00	0.00	0.2655
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	-1.00	50.00	1.094	2	0.00	0.00	0.2656
Sum Weight		3357.01								

### Discrete Appurtenance Pressures - Service $G_o = 1.00$

Description	Along x-axis "	Height ft	Offset ft	Offset ft	z ft	R <sub>z</sub>	q psf	C <sub>d</sub> - Front ft <sup>2</sup>	C <sub>d</sub> - Side ft <sup>2</sup>
Generic Panel (Enclosed, 115 lbs)	300.0000	450.00	-3.29	-1.96	70.00	1.174	5	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.29	-1.96	70.00	1.174	4	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	80.0000	460.00	0.00	-0.96	70.00	1.174	8	0.00	0.00
10'-0" Term CPA - 5.7 602 (161 lbs)	300.0000	322.00	-3.29	-1.96	70.00	1.174	6	0.00	0.00
17'-0" Term EPA - 5.7 802 (161 lbs)	50.0000	322.00	3.29	-1.96	70.00	1.174	4	0.00	0.00
10'-0" Term EPA - 5.7 802 (161 lbs)	180.0000	322.00	0.00	-0.96	70.00	1.174	8	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-3.29	-1.96	70.00	1.174	4	0.00	0.00

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 W. Galena Park Blvd Houston, TX 77030 Phone: (281) 990-1222 FAX: (281) 990-1226	Job	Spike	Page 19 of 131
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Description	Ending x-inches "	W-Shape in	Offset ft	Offset ft	Y ft	Z ft	q psf	C.A. Front ft <sup>2</sup>	C.A. Side ft <sup>2</sup>
75 lbs)									
Generic RRU (Enclosed, 75 lbs)	50.0000	300.00	1.09	-1.06	70.00	1.174	5	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	1.92	70.00	1.174	8	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	-3.46	2.00	60.00	1.137	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.78	-1.00	60.00	1.137	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	1.00	60.00	1.137	7	0.00	0.00
10'-0" T arm EPA = 5.7 RPS (161 lbs)	300.0000	322.00	-3.46	-2.00	60.00	1.137	7	0.00	0.00
10'-0" T arm EPA = 5.7 RPS (161 lbs)	60.0000	372.00	2.15	-2.00	60.00	1.137	7	0.00	0.00
10'-0" T arm EPA = 5.7 RPS (161 lbs)	180.0000	372.00	0.00	1.00	60.00	1.137	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	300.0000	300.00	-1.46	2.00	60.00	1.137	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	2.16	-2.00	60.00	1.137	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	0.00	60.00	1.137	7	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	300.0000	460.00	-4.23	-2.00	60.00	1.094	9	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	60.0000	460.00	3.73	-2.00	60.00	1.094	9	0.00	0.00
Generic Panel (Enclosed, 115 lbs)	180.0000	460.00	0.00	1.00	60.00	1.094	9	0.00	0.00
10'-0" T arm EPA = 5.7 RPS (161 lbs)	60.0000	372.00	2.52	-1.00	60.00	1.094	9	0.00	0.00
10'-0" T arm EPA = 5.7 RPS (161 lbs)	300.0000	322.00	1.65	2.00	60.00	1.094	7	0.00	0.00
10'-0" T arm EPA = 5.7 RPS (161 lbs)	180.0000	322.00	0.00	1.00	60.00	1.094	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	-3.52	-2.00	60.00	1.094	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	60.0000	300.00	3.52	2.00	60.00	1.094	7	0.00	0.00
Generic RRU (Enclosed, 75 lbs)	180.0000	300.00	0.00	1.00	60.00	1.094	7	0.00	0.00
Sum Weight		6750.00							

### Force Totals

Load Case	Vertical Forces lb	Sum of Forces X lb	Sum of Forces Z lb	Sum of Overturning Moments Mx lb-ft	Sum of Overturning Moments My lb-ft	Sum of Twisting Moments lb-ft
Leg Weight	5043.74					
Bracing Weight	0.00					
Local Member Self-Weight	5043.74			0.00	0.00	
Total Weight	10087.48			0.00	0.00	
Wind 0 deg - No Ice		0.00	-15620.39	-272255.32	0.00	0.00
Wind 30 deg - No Ice		8110.26	-14483.68	-270045.85	-156111.19	0.00
Wind 60 deg - No Ice		11252.25	-11752.39	-649059.74	-615050.74	0.00
Wind 90 deg - No Ice		11293.68	8500.20	-456135.19	-270045.85	0.00

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Load Case	Vertical Forces	Sum of Forces X	Sum of Forces Y	Sum of Drilling Moments, M <sub>z</sub>	Sum of Gravity Moments, M <sub>z</sub>	Sum of Torsion
	#	#	#	#-ft	#-ft	#-ft
Wind 90 deg - No Ice		16670.25	0.00	0.00	-972766.27	0.00
Wind 120 deg - No Ice		14393.68	8570.20	456733.19	-790047.85	0.00
Wind 135 deg - No Ice		11755.39	11755.39	243069.74	-643067.74	0.00
Wind 150 deg - No Ice		8570.20	14393.68	790047.85	-456733.19	0.00
Wind 180 deg - No Ice		0.00	16670.25	-42266.47	0.00	0.00
Wind 210 deg - No Ice		-8570.20	14393.68	750045.45	-455233.19	0.00
Wind 225 deg - No Ice		-11755.39	11755.39	643069.74	-643069.74	0.00
Wind 240 deg - No Ice		-14393.68	8570.20	456733.19	-790047.85	0.00
Wind 270 deg - No Ice		-16670.25	0.00	0.00	972766.27	0.00
Wind 300 deg - No Ice		-14393.68	-8570.20	-456733.19	-790047.85	0.00
Wind 315 deg - No Ice		-11755.39	-11755.39	-243069.74	-643069.74	0.00
Wind 330 deg - No Ice		-8570.20	-14393.68	-790047.85	-456733.19	0.00
Member Ice	641.26					
Total Weight Ice	7702.11			0.00	0.00	
Wind 0 deg - Ice		0.00	2322.57	-27508.78	0.00	0.00
Wind 30 deg - Ice		1161.28	2011.45	-11340.69	-53751.39	0.00
Wind 45 deg - Ice		1642.24	1642.24	-50158.08	-90158.08	0.00
Wind 60 deg - Ice		2011.45	-1161.28	-63751.39	-11340.69	0.00
Wind 90 deg - Ice		2322.57	0.00	0.00	-127300.78	0.00
Wind 120 deg - Ice		7011.26	1161.28	63751.39	-64206.1	0.00
Wind 135 deg - Ice		1642.24	1642.24	90158.08	-50158.08	0.00
Wind 150 deg - Ice		1161.28	2011.45	11340.69	-63751.39	0.00
Wind 180 deg - Ice		0.00	2322.57	127300.78	0.00	0.00
Wind 210 deg - Ice		-1161.28	2011.45	11340.69	63751.39	0.00
Wind 225 deg - Ice		-1642.24	1642.24	90158.08	50158.08	0.00
Wind 240 deg - Ice		-2011.45	1161.28	63751.39	11340.69	0.00
Wind 270 deg - Ice		-2322.57	0.00	0.00	127300.78	0.00
Wind 300 deg - Ice		-7011.26	-1161.28	-63751.39	11340.69	0.00
Wind 315 deg - Ice		-1642.24	-1642.24	-90158.08	50158.08	0.00
Wind 330 deg - Ice		-1161.28	-2011.45	-11340.69	63751.39	0.00
Total Weight	2105.74			0.00	0.00	
Wind 0 deg - Service		0.00	-5573.21	-297664.96	0.00	0.00
Wind 30 deg - Service		2686.61	-1261.94	-257958.62	-48952.48	0.00
Wind 45 deg - Service		3797.43	-3797.43	-210622.33	-210622.33	0.00
Wind 60 deg - Service		4653.24	-2586.61	-148917.48	-257958.62	0.00
Wind 90 deg - Service		5573.21	0.00	0.00	-297664.96	0.00
Wind 120 deg - Service		5573.21	2686.61	148917.48	-257958.62	0.00
Wind 135 deg - Service		3797.43	3797.43	210622.33	-210622.33	0.00
Wind 150 deg - Service		2586.61	4653.24	257958.62	-148917.48	0.00
Wind 180 deg - Service		0.00	5573.21	297664.96	0.00	0.00
Wind 210 deg - Service		-2686.61	4653.24	148917.48	257958.62	0.00
Wind 225 deg - Service		-3797.43	3797.43	210622.33	210622.33	0.00
Wind 240 deg - Service		-4653.24	2586.61	148917.48	257958.62	0.00
Wind 270 deg - Service		-5573.21	0.00	0.00	297664.96	0.00
Wind 300 deg - Service		-4653.24	-2686.61	-148917.48	257958.62	0.00
Wind 315 deg - Service		-3797.43	-3797.43	-210622.33	210622.33	0.00
Wind 330 deg - Service		-2686.61	-4653.24	-257958.62	148917.48	0.00

### Load Combinations

Comb No	Description
1	Dead Only
2	1.2 Dead + 1.0 Wind 0 deg - No Ice
3	0.9 Dead + 1.0 Wind 0 deg - No Ice
4	1.2 Dead + 1.0 Wind 90 deg - No Ice

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Comb. No.	Description
5	0.9 Dead+1.0 Wind 45 deg - No Ice
6	1.5 Dead+1.0 Wind 45 deg - No Ice
7	0.9 Dead+1.0 Wind 45 deg - No Ice
8	1.2 Dead+1.0 Wind 60 deg - No Ice
9	0.9 Dead+1.0 Wind 60 deg - No Ice
10	1.2 Dead+1.0 Wind 90 deg - No Ice
11	0.9 Dead+1.0 Wind 90 deg - No Ice
12	1.2 Dead+1.0 Wind 120 deg - No Ice
13	0.9 Dead+1.0 Wind 120 deg - No Ice
14	1.2 Dead+1.0 Wind 135 deg - No Ice
15	0.9 Dead+1.0 Wind 135 deg - No Ice
16	1.2 Dead+1.0 Wind 150 deg - No Ice
17	0.9 Dead+1.0 Wind 150 deg - No Ice
18	1.2 Dead+1.0 Wind 180 deg - No Ice
19	0.9 Dead+1.0 Wind 180 deg - No Ice
20	1.2 Dead+1.0 Wind 210 deg - No Ice
21	0.9 Dead+1.0 Wind 210 deg - No Ice
22	1.2 Dead+1.0 Wind 225 deg - No Ice
23	0.9 Dead+1.0 Wind 225 deg - No Ice
24	1.2 Dead+1.0 Wind 240 deg - No Ice
25	0.9 Dead+1.0 Wind 240 deg - No Ice
26	1.2 Dead+1.0 Wind 270 deg - No Ice
27	0.9 Dead+1.0 Wind 270 deg - No Ice
28	1.2 Dead+1.0 Wind 300 deg - No Ice
29	0.9 Dead+1.0 Wind 300 deg - No Ice
30	1.2 Dead+1.0 Wind 315 deg - No Ice
31	0.9 Dead+1.0 Wind 315 deg - No Ice
32	1.5 Dead+1.0 Wind 330 deg - No Ice
33	0.9 Dead+1.0 Wind 330 deg - No Ice
34	1.2 Dead+1.0 Ice
35	1.2 Dead+1.0 Wind 0 deg+1.0 Ice
36	1.2 Dead+1.0 Wind 30 deg+1.0 Ice
37	1.2 Dead+1.0 Wind 45 deg+1.0 Ice
38	1.2 Dead+1.0 Wind 60 deg+1.0 Ice
39	1.2 Dead+1.0 Wind 75 deg+1.0 Ice
40	1.2 Dead+1.0 Wind 90 deg+1.0 Ice
41	1.2 Dead+1.0 Wind 105 deg+1.0 Ice
42	1.2 Dead+1.0 Wind 120 deg+1.0 Ice
43	1.2 Dead+1.0 Wind 135 deg+1.0 Ice
44	1.2 Dead+1.0 Wind 150 deg+1.0 Ice
45	1.2 Dead+1.0 Wind 165 deg+1.0 Ice
46	1.2 Dead+1.0 Wind 180 deg+1.0 Ice
47	1.2 Dead+1.0 Wind 195 deg+1.0 Ice
48	1.2 Dead+1.0 Wind 210 deg+1.0 Ice
49	1.2 Dead+1.0 Wind 225 deg+1.0 Ice
50	1.2 Dead+1.0 Wind 240 deg+1.0 Ice
51	Dead+Wind 0 deg - Service
52	Dead+Wind 30 deg - Service
53	Dead+Wind 45 deg - Service
54	Dead+Wind 60 deg - Service
55	Dead+Wind 90 deg - Service
56	Dead+Wind 120 deg - Service
57	Dead+Wind 135 deg - Service
58	Dead+Wind 150 deg - Service
59	Dead+Wind 180 deg - Service
60	Dead+Wind 210 deg - Service
61	Dead+Wind 225 deg - Service
62	Dead+Wind 240 deg - Service
63	Dead+Wind 270 deg - Service
64	Dead+Wind 300 deg - Service
65	Dead+Wind 315 deg - Service
66	Dead+Wind 330 deg - Service

<b>tnxTower</b> Vector Structural Engineering 451 W. Gibson Park Blvd Denver, CO 80202 Phone: (303) 999-1775 FAX: (303) 999-1776	Job	Page 22 of 131
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	Spike	
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	Raycap	minnie

### Maximum Member Forces

Section No	Elevation ft	Connection Type	Condition	Max Load Comb	Dist	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
L1	75 - 25	Plate	Max. Tension	55	0.00	0.00	-0.00
			Max. Uniaxial Compression	14	-17726.73	0.00	0.00
			Max. Mx	16	-31330.45	448072.86	0.00
			Max. My	2	-21950.49	0.00	488072.86
			Max. Vy	10	16039.32	-488072.86	0.00
			Max. Vx	7	-16039.32	0.00	488072.86
L2	25 - 1	Plate	Max. Tension	16	0.00	0.00	0.00
			Max. Uniaxial Compression	1	0.00	0.00	0.00
			Max. Mx	10	-25231.17	-950122.58	0.00
			Max. My	15	-25231.17	0.00	-950122.58
			Max. Vy	10	16537.89	-950122.58	0.00
			Max. Vx	13	16537.89	0.00	950122.58
			Max. Tension	6	0.00	0.00	0.00

### Maximum Reactions

Location	Condition	Max Load Comb	Vertical lb	Horizontal X lb	Horizontal Y lb
Base	Max. Vert	27	26568.57	0.00	0.00
	Max. Hx	27	18942.16	16530.17	0.00
	Max. Hy	5	18942.16	0.00	16620.17
	Max. Mx	2	950122.58	0.00	16620.05
	Max. My	10	950122.58	-16620.05	0.00
	Max. Tension	15	0.00	-8310.17	14393.63
	Min. Vert	1	18932.16	0.00	16620.17
	Min. Hx	11	18932.16	-16620.17	0.00
	Min. Hy	15	18932.16	0.00	-16620.17
	Min. Mx	13	-950122.58	0.00	-16620.05
	Min. My	26	-950122.58	16620.05	0.00
	Min. Tension	20	-0.00	8310.17	-14393.63

### Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear lb	Shear lb	Overturning Moment lb-ft	Disturbing Moment lb-ft	Twist lb-ft
Dead Only	31325.77	0.00	0.00	0.00	0.00	0.00
1.2 Dead 1.0 Wind 0 deg - No Ice	25247.87	0.00	-16620.05	-950122.58	0.00	0.00
0.9 Dead 1.0 Wind 0 deg - No Ice	18922.16	0.00	-16620.17	-910136.59	0.00	0.00
1.2 Dead 1.0 Wind 30 deg - No Ice	25242.88	8310.17	14393.63	-822816.26	-47907.71	0.00
0.9 Dead 1.0 Wind 30 deg - No Ice	18932.16	8310.18	-14393.65	-814210.36	-479084.21	0.00

Load Combination	Vertical k	Shear k	Shear k	Overswing Moment M <sub>x</sub> k-ft	Overswing Moment M <sub>y</sub> k-ft	Torque k-ft
1.5 Dead+1.0 Wind 45 deg - No Ice	25242.88	11752.55	-11752.55	-671852.82	-671852.82	0.00
0.9 Dead-1.0 Wind 45 deg - No Ice	18952.16	11752.57	-11752.57	664800.16	-664800.16	0.00
1.2 Dead+1.0 Wind 60 deg - No Ice	25242.88	14395.63	-8100.17	-479071.71	822848.26	-0.00
0.9 Dead-1.0 Wind 60 deg - No Ice	18922.16	14495.66	-8500.18	470081.71	-814210.56	-0.00
1.2 Dead+1.0 Wind 90 deg - No Ice	25242.88	16620.05	0.00	0.00	-650122.99	0.00
0.9 Dead-1.0 Wind 90 deg - No Ice	18922.16	16620.17	0.00	0.00	-940136.50	0.00
1.2 Dead-1.0 Wind 120 deg - No Ice	25242.88	14495.63	8310.17	475071.71	-823548.26	0.00
0.9 Dead+1.0 Wind 120 deg - No Ice	18952.16	14495.65	8310.15	-470081.71	-814210.56	0.00
1.2 Dead+1.0 Wind 135 deg - No Ice	25242.88	11752.55	11752.55	671852.82	-671852.82	0.00
0.9 Dead-1.0 Wind 135 deg - No Ice	18922.16	11752.49	11752.37	-664800.16	-664800.16	0.00
1.2 Dead+1.0 Wind 150 deg - No Ice	25242.88	8310.17	14595.63	822848.26	-479071.71	0.00
0.9 Dead-1.0 Wind 150 deg - No Ice	18922.16	8310.15	-14995.65	-814210.56	-470081.71	-0.00
1.5 Dead+1.0 Wind 180 deg - No Ice	25242.88	0.00	16620.05	550122.99	0.00	0.00
0.9 Dead-1.0 Wind 180 deg - No Ice	18952.16	0.00	16620.17	-940136.50	0.00	0.00
1.2 Dead+1.0 Wind 210 deg - No Ice	25242.88	-8500.17	14395.53	879848.36	-475071.71	0.00
0.9 Dead+1.0 Wind 210 deg - No Ice	18952.16	8310.18	14995.65	-814210.56	-470081.71	0.00
1.2 Dead+1.0 Wind 225 deg - No Ice	25242.88	-11752.55	11752.35	671852.82	671852.82	0.00
0.9 Dead-1.0 Wind 225 deg - No Ice	18922.16	-11752.37	11752.47	-664800.16	664800.16	0.00
1.2 Dead+1.0 Wind 240 deg - No Ice	25242.88	-14495.64	8310.17	475071.71	822848.26	-0.00
0.9 Dead-1.0 Wind 240 deg - No Ice	18922.16	-14595.65	8310.18	-470081.71	-814210.56	0.00
1.2 Dead+1.0 Wind 270 deg - No Ice	25242.88	-16620.05	0.00	0.00	650122.99	0.00
0.9 Dead+1.0 Wind 270 deg - No Ice	18952.16	16620.17	-0.00	0.00	-940136.50	0.00
1.2 Dead+1.0 Wind 300 deg - No Ice	25242.88	-14395.63	-8100.17	-479071.71	822848.26	0.00
0.9 Dead-1.0 Wind 300 deg - No Ice	18922.16	-14495.66	-8500.18	470081.71	-814210.56	0.00
1.5 Dead+1.0 Wind 315 deg - No Ice	25242.88	11752.55	-11752.45	671852.82	671852.82	0.00
0.9 Dead-1.0 Wind 315 deg - No Ice	18952.16	-11752.57	-11752.37	-664800.16	-664800.16	0.00
1.2 Dead+1.0 Wind 330 deg - No Ice	25242.88	-8100.17	-14495.54	822848.26	479071.71	0.00
0.9 Dead+1.0 Wind 330 deg - No Ice	18922.16	-8500.18	-14595.55	-814210.56	-470081.71	-0.00
1.2 Dead+1.0 Ice	25268.51	0.00	0.00	0.00	0.00	0.00
1.2 Dead+1.0 Wind Coldeg+1.0 Ice	25268.51	0.00	252.28	-132590.55	0.00	0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice	25268.51	11609.64	2010.29	-115175.23	66495.20	0.00

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 651 W. Gardner Park Blvd Draper, UT 84020 Phone: (801) 999-1775 FAX: (801) 999-1776	Job	Spike	Page 21 of 131
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			Designed by mrrile

Load Combination	Vertical lb	Shear lb	Moment lb-ft	Displacement X-axis, in.	Displacement Moment, in.	Torque lb-ft
1.2 Dead+1.0 Wind 45 deg+1.0 Ice	26268.51	164.39	-151.39	-34038.55	-94033.55	0.00
1.2 Dead+1.0 Wind 60 deg+1.0 Ice	26268.51	200.29	-1760.61	-66495.40	-115173.23	-0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice	26268.51	2321.28	0.00	0.00	-132990.58	0.00
1.2 Dead+1.0 Wind 135 deg+1.0 Ice	26268.51	2000.29	1160.64	66495.40	-115173.23	0.00
1.2 Dead+1.0 Wind 135 deg-1.0 Ice	26268.51	164.39	161.39	94038.55	-54033.55	0.00
1.2 Dead+1.0 Wind 150 deg-1.0 Ice	26268.51	1150.61	2000.29	115173.23	-66495.40	-0.00
1.2 Dead+1.0 Wind 180 deg-1.0 Ice	26268.51	0.00	2321.28	132990.58	0.00	0.00
1.2 Dead+1.0 Wind 210 deg+1.0 Ice	26268.51	-1160.64	2000.29	-115173.23	66495.40	0.00
1.2 Dead+1.0 Wind 225 deg+1.0 Ice	26268.51	-1641.39	641.39	-94038.55	34038.55	0.00
1.2 Dead+1.0 Wind 240 deg+1.0 Ice	26268.51	-2000.29	1160.64	-66495.40	115173.23	-0.00
1.2 Dead+1.0 Wind 270 deg+1.0 Ice	26268.51	-2321.28	0.00	0.00	-132990.58	0.00
1.2 Dead+1.0 Wind 300 deg+1.0 Ice	26268.51	-2000.29	-1160.64	-66495.40	115173.23	0.00
1.2 Dead+1.0 Wind 315 deg+1.0 Ice	26268.51	-1641.39	-1641.39	-94038.55	94033.55	0.00
1.2 Dead+1.0 Wind 330 deg+1.0 Ice	26268.51	-1160.64	-2000.29	-115173.23	66495.40	-0.00
Dead+Wind 3 deg - Service	21035.73	0.00	-5772.71	-80821.42	0.00	0.00
Dead+Wind 60 deg - Service	21035.73	2586.37	-4632.93	-26692.40	-151107.24	0.00
Dead+Wind 15 deg - Service	21035.73	3799.11	-8799.11	-21794.24	-21794.24	0.00
Dead+Wind 50 deg - Service	21035.73	4632.93	2686.47	-151107.24	-26692.40	0.00
Dead+Wind 90 deg - Service	21035.73	5472.71	0.00	0.00	-308219.47	0.00
Dead+Wind 130 deg - Service	21035.73	4632.93	2686.47	151107.24	-26692.40	0.00
Dead+Wind 145 deg - Service	21035.73	3799.11	3799.11	21794.24	-21794.24	0.00
Dead+Wind 180 deg - Service	21035.73	2686.37	4632.93	26692.40	-151107.24	0.00
Dead+Wind 210 deg - Service	21035.73	0.00	5472.71	308219.47	0.00	0.00
Dead+Wind 225 deg - Service	21035.73	-2686.37	4632.93	-26692.40	151107.24	0.00
Dead+Wind 240 deg - Service	21035.73	-3799.11	3799.11	-21794.24	21794.24	0.00
Dead+Wind 270 deg - Service	21035.73	-4632.93	2686.37	-151107.24	26692.40	-0.00
Dead+Wind 300 deg - Service	21035.73	-5472.71	-0.00	0.00	-308219.47	0.00
Dead+Wind 315 deg - Service	21035.73	-4632.93	-2686.37	-151107.24	26692.40	0.00
Dead+Wind 330 deg - Service	21035.73	-3799.11	-3799.11	-21794.24	21794.24	0.00
Dead+Wind 330 deg - Service	21035.73	-2686.37	-4632.93	-26692.40	151107.24	0.00

### Solution Summary

Load Comb.	FX lb	Sum of Applied Forces			Sum of Reactions			% Error
		FX lb	FY lb	FZ lb	PX lb	PY lb	PZ lb	
1	0.00	-21035.74	0.00	0.00	21035.74	0.00	0.000%	
2	0.00	25242.88	-16620.39	0.00	25242.87	16620.39	0.001%	
3	0.00	-18532.16	-16620.39	0.00	18532.16	16620.37	0.001%	
4	2310.20	-15742.88	-14399.68	-8310.17	2310.20	15742.88	14399.68	0.000%
5	8310.20	-14972.16	-11392.68	-8310.18	8310.20	14972.16	11392.68	0.000%
6	11751.49	-25242.88	-11751.39	11751.35	25242.88	11751.35	0.000%	
7	11751.49	-18932.16	-11751.39	-11751.37	18932.16	11751.37	0.000%	
8	14399.68	-35242.88	-8310.17	-14399.63	35242.88	8310.17	0.000%	

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Level Count	Sum of Applied Forces				Sum of Reactions			% Error
	Px lb	Py lb	Pz lb	Mx lb	Rx lb	Ry lb	Rz lb	
9	4991.78	-13532.76	8310.20	-14993.65	18922.16	8710.18	0.000%	
10	6620.35	-17242.88	0.00	-16630.35	25212.57	0.00	0.001%	
11	6620.35	-18742.76	0.00	-16630.17	18922.76	0.00	0.001%	
12	14293.55	-25242.55	8310.20	-14499.65	25212.58	-8310.20	0.000%	
13	14293.55	-18912.16	8310.20	-14499.65	18922.76	-8310.20	0.000%	
14	11752.39	-25242.88	11752.39	-11752.35	25242.88	-11752.35	0.000%	
15	11752.39	-18922.16	11752.39	-11752.37	18922.16	-11752.37	0.000%	
16	8310.20	-25242.88	4399.68	-8310.17	25242.88	-14499.68	0.000%	
17	8310.20	-18922.16	4399.68	-8310.18	18922.16	-14499.68	0.000%	
18	0.00	-25242.88	16620.35	0.00	25242.87	-16620.35	0.001%	
19	0.00	-18922.16	16620.35	0.00	18922.16	-16620.17	0.001%	
20	-8310.20	-25242.88	14499.68	4310.17	25242.88	-14499.68	0.000%	
21	-4310.20	-8922.76	14499.68	8310.18	18922.16	-1392.65	0.000%	
22	-11752.39	-25242.88	11752.39	-11752.33	25242.88	-11752.35	0.000%	
23	-11752.39	-18922.16	11752.39	-11752.37	18922.16	-11752.37	0.000%	
24	-14293.55	-25242.88	8310.20	14499.68	25242.88	-8310.17	0.000%	
25	-14293.55	-18922.16	8310.20	14499.68	18922.16	-8310.18	0.000%	
26	-16630.35	25242.88	0.00	16620.35	25242.87	0.00	0.001%	
27	-16630.35	-18922.16	0.00	16620.17	18922.16	0.00	0.001%	
28	-14499.68	-25242.88	-4310.20	14293.55	25242.88	8310.17	0.000%	
29	-14499.68	-18922.16	-4310.20	14293.55	18922.16	8310.18	0.000%	
30	-11752.39	-25242.88	-11752.35	11752.35	25242.88	11752.35	0.000%	
31	-11752.39	-18922.16	-11752.35	11752.37	18922.16	11752.37	0.000%	
32	-8310.20	-25242.88	-14499.68	8310.17	25242.88	14499.68	0.000%	
33	-8310.20	-18922.16	-14499.68	8310.18	18922.16	14499.68	0.000%	
34	0.00	-26268.51	0.00	0.00	26268.51	0.00	0.000%	
35	0.00	-26268.51	2321.25	0.00	26268.51	2321.25	0.000%	
36	1641.39	-26268.51	-2311.35	-1641.39	26268.51	2010.29	0.000%	
37	1641.39	26268.51	-1641.39	-1641.39	26268.51	1641.39	0.000%	
38	2010.29	26268.51	-1161.25	-2010.29	26268.51	1161.25	0.000%	
39	2321.25	-26268.51	0.00	2321.25	26268.51	0.00	0.000%	
40	2010.29	-26268.51	1161.25	-2010.29	26268.51	-1161.25	0.000%	
41	1641.39	-26268.51	1641.39	-1641.39	26268.51	-1641.39	0.000%	
42	1161.25	-26268.51	2010.29	1161.25	26268.51	-2010.29	0.000%	
43	0.00	-26268.51	2321.25	0.00	26268.51	2321.25	0.000%	
44	-1161.25	-26268.51	2010.29	1161.25	26268.51	-2010.29	0.000%	
45	-1641.39	-26268.51	1641.39	-1641.39	26268.51	-1641.39	0.000%	
46	-2010.29	-26268.51	1161.25	-2010.29	26268.51	-1161.25	0.000%	
47	2321.25	-26268.51	0.00	2321.25	26268.51	0.00	0.000%	
48	-2010.29	-26268.51	1161.25	-2010.29	26268.51	-1161.25	0.000%	
49	-1641.39	-26268.51	1641.39	-1641.39	26268.51	-1641.39	0.000%	
50	-1161.25	-26268.51	2010.29	1161.25	26268.51	-2010.29	0.000%	
51	0.00	-21035.74	-4653.93	0.00	21035.74	4653.93	0.000%	
52	2685.61	-21035.74	-4653.93	-2685.61	21035.74	4653.93	0.000%	
53	4799.44	-21035.74	-4799.44	4799.44	21035.74	4799.44	0.000%	
54	4653.93	-21035.74	-2685.61	-4653.93	21035.74	2685.61	0.000%	
55	5372.21	-21035.74	0.00	-5372.21	21035.74	0.00	0.000%	
56	4653.93	-21035.74	2685.61	-4653.93	21035.74	-2685.61	0.000%	
57	4799.44	-21035.74	4799.44	-4799.44	21035.74	-4799.44	0.000%	
58	2685.61	-21035.74	4653.93	-2685.61	21035.74	-4653.93	0.000%	
59	0.00	-21035.74	5372.21	0.00	21035.74	5372.21	0.000%	
60	-2685.61	-21035.74	4653.93	2685.61	21035.74	-4653.93	0.000%	
61	-4799.44	-21035.74	4799.44	-4799.44	21035.74	-4799.44	0.000%	
62	-4653.93	-21035.74	2685.61	4653.93	21035.74	-2685.61	0.000%	
63	-5372.21	-21035.74	0.00	5372.21	21035.74	0.00	0.000%	
64	-4653.93	-21035.74	-2685.61	4653.93	21035.74	2685.61	0.000%	
65	-4799.44	-21035.74	-4799.44	4799.44	21035.74	-4799.44	0.000%	
66	-2685.61	-21035.74	-4653.93	2685.61	21035.74	4653.93	0.000%	

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**Non-Linear Convergence Results**

Load Combination	Converged?	Number of Cycles	Displacement Tolerances	Force Tolerances
1	Yes	6	0.0000001	0.0000001
2	Yes	10	0.0000001	0.0000001
3	Yes	10	0.0000001	0.0000001
4	Yes	11	0.0000001	0.0000001
5	Yes	11	0.0000001	0.0000001
6	Yes	11	0.0000001	0.0000001
7	Yes	11	0.0000001	0.0000001
8	Yes	11	0.0000001	0.0000001
9	Yes	11	0.0000001	0.0000001
10	Yes	10	0.0000001	0.0000001
11	Yes	10	0.0000001	0.0000001
12	Yes	11	0.0000001	0.0000001
13	Yes	11	0.0000001	0.0000001
14	Yes	11	0.0000001	0.0000001
15	Yes	11	0.0000001	0.0000001
16	Yes	11	0.0000001	0.0000001
17	Yes	11	0.0000001	0.0000001
18	Yes	10	0.0000001	0.0000001
19	Yes	10	0.0000001	0.0000001
20	Yes	11	0.0000001	0.0000001
21	Yes	11	0.0000001	0.0000001
22	Yes	11	0.0000001	0.0000001
23	Yes	11	0.0000001	0.0000001
24	Yes	11	0.0000001	0.0000001
25	Yes	11	0.0000001	0.0000001
26	Yes	10	0.0000001	0.0000001
27	Yes	10	0.0000001	0.0000001
28	Yes	11	0.0000001	0.0000001
29	Yes	11	0.0000001	0.0000001
30	Yes	11	0.0000001	0.0000001
31	Yes	11	0.0000001	0.0000001
32	Yes	11	0.0000001	0.0000001
33	Yes	11	0.0000001	0.0000001
34	Yes	6	0.0000001	0.0000001
35	Yes	4	0.0000001	0.0000001
36	Yes	4	0.0000001	0.0000001
37	Yes	8	0.0000001	0.0000001
38	Yes	8	0.0000001	0.0000001
39	Yes	8	0.0000001	0.0000001
40	Yes	8	0.0000001	0.0000001
41	Yes	8	0.0000001	0.0000001
42	Yes	8	0.0000001	0.0000001
43	Yes	8	0.0000001	0.0000001
44	Yes	8	0.0000001	0.0000001
45	Yes	8	0.0000001	0.0000001
46	Yes	8	0.0000001	0.0000001
47	Yes	8	0.0000001	0.0000001
48	Yes	8	0.0000001	0.0000001
49	Yes	8	0.0000001	0.0000001
50	Yes	8	0.0000001	0.0000001
51	Yes	9	0.0000001	0.0000001
52	Yes	9	0.0000001	0.0000001
53	Yes	9	0.0000001	0.0000001
54	Yes	9	0.0000001	0.0000001
55	Yes	9	0.0000001	0.0000001
56	Yes	9	0.0000001	0.0000001
57	Yes	9	0.0000001	0.0000001

<b>inxTower</b> Vector Structural Engineering 951 W. Gateway Park Blvd Cooper, UT 84629 Phone: (971) 936-1775 FAX: (971) 936-1776	Job	Spike	Page 27 of 121
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53	Yes	9	0.0000001	0.0005807
59	Yes	9	0.0000001	0.0007126
60	Yes	9	0.0000001	0.0002687
61	Yes	9	0.0000001	0.0005202
67	Yes	9	0.0000001	0.0005807
68	Yes	9	0.0000001	0.0007126
64	Yes	9	0.0000001	0.0002687
65	Yes	9	0.0000001	0.0005202
66	Yes	9	0.0000001	0.0005807

### Maximum Tower Deflections - Service Wind

Section No	Elevation ft	Max. Deflection in	Gen. Load Comb.	Tilt °	Tors. °
L1	75 - 25	19.110	59	1.0415	0.0000
L2	29.25 - 1	1.680	59	0.9258	0.0000

### Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Approximate	Gen. Load Comb.	Deflection in	Tilt °	Tors. °	Radius of Curvature ft
75.00	Concealment Loading @ 75 ft	59	10.110	1.0418	0.0000	21715
70.00	(4) Generic Panel (Underside, 115 lbs)	59	3.995	0.9966	0.0000	21715
65.00	Concealment Loading @ 65 ft	59	7.900	0.9506	0.0000	10857
60.00	(4) Generic Panel (Underside, 115 lbs)	59	6.859	0.9040	0.0000	7238
55.00	Concealment Loading @ 55 ft	59	3.807	0.8379	0.0000	5428
50.00	(4) Generic Panel (Underside, 115 lbs)	59	4.837	0.7796	0.0000	3412
45.00	Concealment Loading @ 45 ft	59	3.922	0.7422	0.0000	3615

### Maximum Tower Deflections - Design Wind

Section No	Elevation ft	Max. Deflection in	Gen. Load Comb.	Tilt °	Tors. °
L1	75 - 25	31.137	5	1.2047	0.0000
L2	29.25 - 1	3.175	5	1.6194	0.0000

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Approximate	Gen. Load Comb.	Deflection in	Tilt °	Tors. °	Radius of Curvature ft
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Elevation	Description	Grav. Load Comb.	Deflection	T <sub>11</sub>	T <sub>12</sub>	Ratio of Characteristic
$\beta$			in	"	"	$\beta$
75.00	Concealment Loading @ 25 ft	18	21.127	3.2047	0.0000	7094
70.00	(4) Generic Panel (Enclosed, 112 lbs)	18	27.587	3.0660	0.0000	7094
65.00	Concealment Loading @ 55 ft	18	25.330	2.7749	0.0000	2545
60.00	(4) Generic Panel (Enclosed, 112 lbs)	18	21.017	2.7787	0.0000	2564
55.00	Concealment Loading @ 55 ft	18	17.852	2.0251	0.0000	1772
50.00	(4) Generic Panel (Enclosed, 112 lbs)	18	14.877	2.4613	0.0000	1417
45.00	Concealment Loading @ 45 ft	18	12.075	2.3850	0.0000	1190

### Compression Checks

### Pole Design Data

Section No.	Elevation	Size	L	L <sub>c</sub>	K <sub>1</sub>	A	P <sub>c</sub>	σ <sub>p</sub>	Ratio
	$\beta$		ft	ft		in <sup>2</sup>	lb	lb	$\frac{P_c}{\sigma_p}$
L1	75 - 72.5921	1P10 75x71x0.1875	50.00	3.00	3.00	3.6655	-1771.91	740820.00	0.02
	72.5921 - 70.1843					3.9447	-1776.69	757277.00	0.02
	70.1843 - 67.7765					4.2241	-5749.67	772621.00	0.07
	67.7765 - 65.3687					4.5035	-5476.57	785971.00	0.07
	65.3687 - 62.9609					4.7822	-7872.49	806318.00	0.10
	62.9609 - 60.5531					4.0656	-8708.50	823665.00	0.10
	60.5531 - 58.1453					4.3447	-12088.90	849012.00	0.14
	58.1453 - 55.7375					4.6237	-12183.70	853359.00	0.14
	55.7375 - 53.3297					4.9030	-14623.00	871705.00	0.17
	53.3297 - 50.9219					5.1824	-14787.50	888052.00	0.17
	50.9219 - 48.5141					5.4617	-18828.10	904400.00	0.21
	48.5141 - 46.1063					5.7407	-19000.00	907750.00	0.21
	46.1063 - 43.6985					6.0197	-20422.50	917095.00	0.22
	43.6985 - 41.2907					6.2987	-20505.50	923440.00	0.22
	41.2907 - 38.8829					6.5776	-20700.70	940787.00	0.23
	38.8829 - 36.4751					6.8570	-20901.70	960134.00	0.27
	36.4751 - 34.0673					7.1364	-21106.10	1002180.00	0.27
	34.0673 - 31.6595					7.4158	-21313.80	1018830.00	0.27
	31.6595 - 29.2517					7.6952	-21520.70	1025170.00	0.27

<b>inxTower</b>  <b>Vector Structural Engineering</b> 651 E. Galena Park Blvd Denver, CO 80236 Phone: (303) 599-1775 FAX: (303) 599-1776	Job	Spike	Page 29 of 151
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Section No.	Elevation $\mu$	Size	$F_x$	$F_y$	$R_{\text{req}}$	$F_x$	$F_y$	$W_{\text{req}}$	$R_{\text{ratio}}$
			$\mu$	$\mu$		$\mu'$	$\mu'$	$\mu'$	
L2	19.25	TP35 035x09.5463x0.57	28.33	0.00	0.0	15.1887	-9530.96	1064070.00	0.019
	19.25 - 25					14.9042	-12559.20	1599500.00	0.019
	25 - 25.7368					14.6996	-22488.40	1469880.00	0.015
	23.7368 -					14.2951	-22581.80	1521260.00	0.015
	22.4757								
	22.4757 -					14.4905	-22725.60	1433700.00	0.016
	21.3105								
	21.2105 -					14.6850	-22870.60	1444700.00	0.016
	19.947								
	19.947 -					14.4814	-23025.00	1455360.00	0.016
	18.6847								
	18.6847 -					15.0759	-23170.60	1467000.00	0.016
	17.4211								
	17.4211 -					15.3725	-23325.50	1478430.00	0.016
	16.1579								
	16.1579 -					15.4678	-23477.70	1489570.00	0.016
	14.8947								
	14.8947 -					15.0633	-23631.00	1500300.00	0.016
	13.6316								
	13.6316 -					15.4587	-23785.70	1511730.00	0.016
12.3684									
12.3684 -	15.0512	-23940.50	1521700.00	0.016					
11.1053									
11.1053 -	15.2495	-24095.60	1532600.00	0.016					
9.84211									
9.84211 -	15.4451	-24255.50	1547000.00	0.016					
8.57895									
8.57895 -	15.6405	-24416.30	1555470.00	0.016					
7.31579									
7.31579 -	15.4360	-24575.50	1567800.00	0.016					
6.05263									
6.05263 -	17.0314	-24735.70	1581340.00	0.016					
4.78947									
4.78947 -	17.3269	-24897.70	1592700.00	0.016					
3.52632									
3.52632 -	17.4223	-25060.90	1604210.00	0.016					
2.26316									
2.26316 -	17.6178	-25221.00	1615840.00	0.016					

### Pole Bending Design Data

Section No.	Elevation $\mu$	Size	$F_x$	$F_y$	$R_{\text{req}}$	$F_x$	$F_y$	$R_{\text{ratio}}$			
			$\mu$	$\mu$		$\mu'$	$\mu'$				
L1	75 - 72.591	TP30 75x11x0.1875	6755.77	252586.67	0.017	0.00	392385.67	0.000			
	72.591 -					23752.08	-407259.17	0.027	0.00	407259.17	0.000
	70.1842										
	70.1842 -					17475.31	-422501.67	0.031	0.00	422501.67	0.000
	67.7763										
	67.7763 -					29477.07	-437751.00	0.007	0.00	437751.00	0.000
	65.3684										
	65.3684 -					46388.41	-452981.67	0.005	0.00	452981.67	0.000
	62.9605										
	62.9605 -					55543.25	-468214.17	0.040	0.00	468214.17	0.000

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Station No.	Elevation $\bar{h}$	Size	$M_x$ $M_y$	$\#M_x$ $\#M_y$	Ratio $M_x/M_y$	$M_z$ $M_y$	$\#M_z$ $\#M_y$	Ratio $M_z/M_y$
	50.1525 - 48.1447		48133.00	-48765.00	0.175	0.00	48376.00	0.000
	58.1547 - 55.7268		105051.57	-94426.57	0.210	0.00	49476.57	0.000
	55.7268 - 53.3289		130146.57	-51551.57	0.257	0.00	51551.57	0.000
	53.3289 - 50.9211		162130.87	557051.57	0.306	0.00	591051.57	0.000
	50.9211 - 48.5132		193385.82	509000.00	0.354	0.00	54700.00	0.000
	48.5132 - 45.1053		224613.57	563028.22	0.399	0.00	569028.22	0.000
	46.1053 - 43.6974		259456.57	572791.17	0.448	0.00	579291.17	0.000
	43.6974 - 41.2895		297057.50	582295.00	0.497	0.00	591955.00	0.000
	41.2895 - 38.8816		335000.00	51518.11	0.544	0.00	611518.11	0.000
	38.8816 - 36.4737		373036.57	527791.57	0.591	0.00	62791.57	0.000
	36.4737 - 34.0658		41269.00	544107.50	0.638	0.00	64107.50	0.000
	34.0658 - 31.6579		44964.17	590457.00	0.681	0.00	66457.00	0.000
	31.6579 - 29.2500		48901.17	509454.17	0.731	0.00	67634.17	0.000
1.2	29.25 - 29	T993.055x29.5163x0.23	214523.22	507982.50	0.746	0.00	70582.50	0.000
	29 - 24.7986		311555.82	1029525.00	0.904	0.00	1029525.00	0.000
	24.7986 - 22.3908		375529.17	1043211.00	0.953	0.00	1044741.00	0.000
	22.3908 - 20.0157		397410.00	1058000.00	0.958	0.00	1054000.00	0.000
	20.0157 - 17.6315		417921.57	1073308.33	0.976	0.00	1072308.33	0.000
	17.6315 - 15.2474		438161.17	1086665.00	0.988	0.00	1086665.00	0.000
	15.2474 - 12.8632		45906.57	1101066.57	0.995	0.00	1101066.57	0.000
	12.8632 - 10.4791		679610.00	113208.22	0.999	0.00	113308.22	0.000
	10.4791 - 8.0950		70272.50	115000.00	0.999	0.00	115000.00	0.000
	8.0950 - 5.7109		72691.00	1144575.00	0.999	0.00	1144525.00	0.000
	5.7109 - 3.3268		741021.50	1159091.57	0.940	0.00	1159091.57	0.000
	3.3268 - 0.9427		76748.17	1172708.33	0.950	0.00	1172708.33	0.000
	0.9427 - 1.4586		78500.00	1185150.00	0.952	0.00	1185150.00	0.000
	1.4586 - 1.9745		80380.00	120661.57	0.668	0.00	120661.57	0.000
	1.9745 - 2.4904		42489.17	1217758.33	0.677	0.00	1217758.33	0.000
	2.4904 - 3.0063		445523.00	1232316.57	0.686	0.00	1232316.57	0.000
	3.0063 - 3.5222		46652.57	1247108.33	0.695	0.00	1247108.33	0.000
	3.5222 - 4.0381		48729.57	126248.55	0.705	0.00	126211.55	0.000
	4.0381 - 4.5540		50820.33	127891.57	0.711	0.00	127891.57	0.000

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 671 W. Galena Park Blvd Draper, UT 84020 Phone: (801) 998-1775 FAX: (801) 999-1776	Job	Spike	Page 31 of 131
	Project	U0142.2054.242	Date 17.04.43 10/24/24
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Section No	Elevation $\beta$	Size	$M_x$ lb-ft	$\phi M_x$ lb-ft	Ratio $\frac{M_x}{\phi M_x}$	$M_y$ lb-ft	$\phi M_y$ lb-ft	Ratio $\frac{M_y}{\phi M_y}$
	3.52042							
	3.52032		295165.67	1291875.00	0.719	0.00	1251875.00	0.000
	2.263.6							
	2.263.6 -		290111.67	1306791.67	0.727	0.00	1306791.67	0.000

### Pole Shear Design Data

Section No	Elevation $\beta$	Size	Actual $V_x$ lb	$\phi V_x$ lb	Ratio $\frac{V_x}{\phi V_x}$	Actual $V_y$ lb	$\phi V_y$ lb	Ratio $\frac{V_y}{\phi V_y}$
L1	75 - 72.5921	1Pau70x2.2x11.18x2	2822.91	232799.00	0.012	0.00	114278.22	0.000
	72.5921		2956.70	227183.00	0.013	0.00	132760.00	0.000
	70.1549							
	70.1547 -		5274.97	255087.00	0.014	0.00	451645.00	0.000
	67.7163							
	67.7163 -		3176.52	260951.00	0.011	0.00	112633.22	0.000
	65.2784							
	65.2784 -		7574.65	241895.00	0.032	0.00	499175.00	0.000
	62.8405							
	62.8405 -		7425.58	240799.00	0.032	0.00	510231.00	0.000
	60.4026							
	60.4026 -		8234.22	251764.00	0.033	0.00	541218.34	0.000
	58.1447							
	58.1447 -		8330.12	256608.00	0.032	0.00	552129.00	0.000
	55.7068							
	55.7068 -		12579.60	261312.00	0.048	0.00	673475.00	0.000
	53.2689							
	53.2689 -		12670.00	256115.00	0.048	0.00	590133.22	0.000
	50.8311							
	50.8311 -		12346.70	271370.00	0.048	0.00	617215.00	0.000
	48.3932							
	48.3932 -		13025.50	276224.00	0.047	0.00	597260.00	0.000
	46.1053							
	46.1053 -		15561.00	281128.00	0.056	0.00	602678.34	0.000
	43.6674							
	43.6674 -		15731.50	286032.00	0.055	0.00	586003.00	0.000
	41.2295							
	41.2295 -		15798.80	280936.00	0.054	0.00	577325.00	0.000
	38.7916							
	38.7916 -		15563.00	275810.00	0.051	0.00	723853.22	0.000
	36.4737							
	36.4737 -		15924.40	280744.00	0.059	0.00	753385.00	0.000
	34.1058							
	34.1058 -		15983.00	285618.00	0.052	0.00	783319.34	0.000
	31.6679							
	31.6679 -		16049.80	290552.00	0.052	0.00	803657.34	0.000
	29.25							
	29.25 - 25		2175.24	315208.00	0.022	0.00	854366.67	0.000
L2	29.25 - 25	TP35075x20 3487x0.25	3028.32	115318.00	0.022	0.00	1106775.00	0.000
	25 - 25.0068		16316.90	427949.00	0.038	0.00	1131941.67	0.000
	23.7368 -		16241.50	426379.00	0.038	0.00	1144256.67	0.000
	22.4737 -							
	22.4737 -		16266.00	425899.00	0.038	0.00	1161754.22	0.000
	21.2105							
	21.2105 -		16300.50	424329.00	0.038	0.00	1130350.00	0.000
	19.9474							

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<b>Project</b>	U0142.2054.242	<b>Date</b> 17:04:43 10/24/24
<b>Client</b>	Raycap	<b>Designed by</b> miria

Section No.	Elevation $\bar{h}$	Slab	Actual $F_c$ $\bar{h}$	$\phi F_c$ $\bar{h}$	Ratio $\frac{F_c}{\phi F_c}$	Actual $F_s$ $\bar{h}$	$\phi F_s$ $\bar{h}$	Ratio $\frac{F_s}{\phi F_s}$
	19.9474 - 12.6843		6914.60	43655.00	0.057	0.00	19917.67	0.000
	18.5842 - 13.1211		6218.60	44010.00	0.057	0.00	21803.53	0.000
	17.1211 - 16.1579		7657.30	44350.00	0.057	0.00	73761.67	0.000
	16.1579 - 14.8947		7935.00	44690.00	0.057	0.00	72590.00	0.000
	14.8947 - 13.6316		16499.40	45030.00	0.035	0.00	127528.53	0.000
	13.6316 - 12.3684		16722.80	45380.00	0.036	0.00	179513.53	0.000
	12.3684 - 11.1053		16456.00	45730.00	0.035	0.00	131451.57	0.000
	11.1053 - 9.8421		16775.10	46080.00	0.036	0.00	103451.57	0.000
	9.8421 - 8.5789		16902.10	46430.00	0.036	0.00	135476.57	0.000
	8.5789 - 7.3157		16773.00	46780.00	0.035	0.00	192463.53	0.000
	7.3157 - 6.0525		16947.80	47130.00	0.035	0.00	139468.53	0.000
	6.0525 - 4.7894		16970.50	47480.00	0.035	0.00	147300.00	0.000
	4.7894 - 3.5262		16981.10	47830.00	0.035	0.00	173511.57	0.000
	3.5262 - 2.2631		16922.70	48180.00	0.035	0.00	149675.00	0.000
	2.2631 - 1.0000		16928.20	48480.00	0.034	0.00	147766.57	0.000

**Pole Interaction Design Data**

Section No.	Elevation $\bar{h}$	Ratio $\frac{F_c}{\phi F_c}$	Ratio $\frac{F_s}{\phi F_c}$	Ratio $\frac{F_c}{\phi F_c}$	Ratio $\frac{F_s}{\phi F_c}$	Ratio $\frac{F_s}{\phi F_s}$	Coord. Strength Ratio	Min. Strength Ratio	Comments
21	78.92592	0.002	0.017	0.000	0.015	0.000	0.019	1.000	✓
	92.591 - 90.1812	0.000	0.054	0.000	0.015	0.000	0.050	1.000	✓
	70.1843 - 67.7767	0.007	0.051	0.000	0.014	0.000	0.058	1.000	✓
	63.7768 - 61.3684	0.007	0.067	0.000	0.014	0.000	0.075	1.000	✓
	62.3684 - 60.9605	0.010	0.105	0.000	0.032	0.000	0.111	1.000	✓
	62.9605 - 60.5525	0.010	0.140	0.000	0.032	0.000	0.151	1.000	✓
	60.5525 - 59.1447	0.018	0.178	0.000	0.033	0.000	0.191	1.000	✓
	58.1447 - 57.7368	0.014	0.210	0.000	0.032	0.000	0.226	1.000	✓
	55.7368	0.017	0.257	0.000	0.048	0.000	0.276	1.000	✓

<b>tnxTower</b>  <b>Vector Structural Engineering</b> 651 W. Graines Park Blvd Dayton, OH 45424 Phone: (601) 999-1775 FAX: (601) 999-1776	Job	Spike	Page 33 of 101
	Project	U0142.2054.242	Date 17:04:43 10/24/24
	Client	Raycap	Designed by mrio

Section No.	Elevation ft	Ratio $P_x$ of $P_x$	Ratio $M_x$ of $M_x$	Ratio $M_y$ of $M_y$	Ratio $P_y$ of $P_y$	Ratio $T_z$ of $T_z$	Comb. Stress Ratio	Allow. Stress Ratio	Control
	53.3289						✓	1.000	✓
	54.9249 - 56.9211	0.017	0.300	0.000	0.048	0.000	0.325	1.000	✓
	50.9211 - 48.5135	0.021	0.354	0.000	0.048	0.000	0.377	1.000	✓
	48.5132 - 46.1053	0.021	0.399	0.000	0.047	0.000	0.422	1.000	✓
	46.1054 - 43.6974	0.023	0.445	0.000	0.050	0.000	0.475	1.000	✓
	43.6971 - 41.2895	0.025	0.499	0.000	0.055	0.000	0.524	1.000	✓
	41.2895 - 38.8816	0.021	0.546	0.000	0.051	0.000	0.577	1.000	✓
	38.8816 - 36.4737	0.021	0.594	0.000	0.054	0.000	0.618	1.000	✓
	36.4737 - 34.0658	0.021	0.638	0.000	0.050	0.000	0.662	1.000	✓
	34.0658 - 31.6579	0.021	0.681	0.000	0.052	0.000	0.704	1.000	✓
	31.6579 - 29.25	0.021	0.721	0.000	0.052	0.000	0.715	1.000	✓
	29.25 - 29	0.000	0.746	0.000	0.050	0.000	0.755	1.000	✓
1.2	29.25 - 25	0.009	0.930	0.000	0.022	0.000	0.919	1.000	✓
	25 - 23.7500	0.010	0.954	0.000	0.055	0.000	0.970	1.000	✓
	23.7500 - 22.4725	0.010	0.965	0.000	0.055	0.000	0.987	1.000	✓
	22.4725 - 21.2100	0.010	0.970	0.000	0.058	0.000	0.994	1.000	✓
	21.2100 - 19.9475	0.010	0.968	0.000	0.058	0.000	0.996	1.000	✓
	19.9474 - 18.6842	0.010	0.970	0.000	0.057	0.000	0.916	1.000	✓
	18.6842 - 17.4211	0.010	0.969	0.000	0.057	0.000	0.920	1.000	✓
	17.4211 - 16.1579	0.010	0.960	0.000	0.057	0.000	0.937	1.000	✓
	16.1579 - 14.8947	0.010	0.950	0.000	0.057	0.000	0.947	1.000	✓
	14.8947 - 13.6316	0.010	0.940	0.000	0.056	0.000	0.957	1.000	✓
	13.6316 - 12.3684	0.010	0.950	0.000	0.056	0.000	0.957	1.000	✓
	12.3684 - 11.1053	0.010	0.959	0.000	0.056	0.000	0.970	1.000	✓
	11.1053 - 9.84211	0.010	0.968	0.000	0.056	0.000	0.983	1.000	✓
	9.84211 - 8.57895	0.010	0.977	0.000	0.056	0.000	0.994	1.000	✓
	8.57895 -	0.010	0.986	0.000	0.055	0.000	0.999	1.000	✓

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Project	U0142.2054.242	Date 17:04:43 10/24/24
Client	Raycap	Designed by mririe

Member No.	Member #	Node #	Node #	Node #	Node #	Node #	Node #	Elem Stress Ratio	Elem Stress Ratio	Criteria
	751376									
	751379 - 605843	0.06	0.503	0.000	0.035	0.000	0.000	0.711	1.000	✓
	605263 - 478917	0.016	0.303	0.000	0.045	0.000	0.000	0.739	1.000	✓
	478842 - 492042	0.008	0.717	0.000	0.037	0.000	0.000	0.755	1.000	✓
	492032 - 326919	0.016	0.719	0.000	0.035	0.000	0.000	0.736	1.000	✓
	326916 - 1	0.016	0.727	0.000	0.034	0.000	0.000	0.744	1.000	✓

**Section Capacity Table**

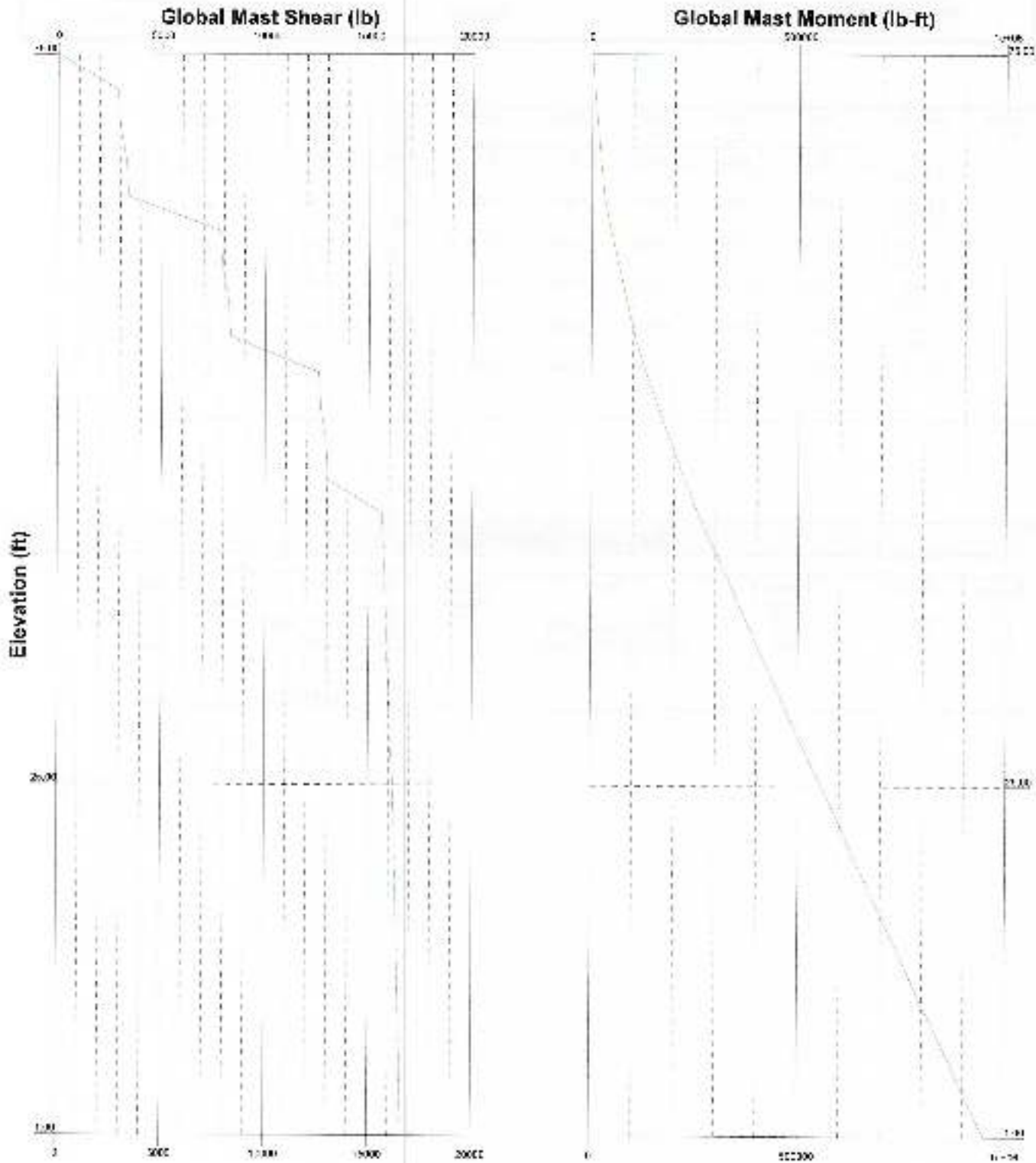
Section No.	Element #	Component Type	Size	Critical Element	P (k)	$\phi P_n$ (k)	% Capacity	Pass/Fail
1.1	75-25	Pile	1P50.73x27.40.1573	1	-21740.40	109150.00	74.3	Pass
1.2	25-1	Pile	TP45.055x29.5465x0.25	5	-28781.10	1613640.00	74.4	Pass
<b>Summary:</b>								
Pile (LL)							74.4	Pass
<b>RATING =</b>							<b>74.5</b>	<b>Pass</b>

Vx

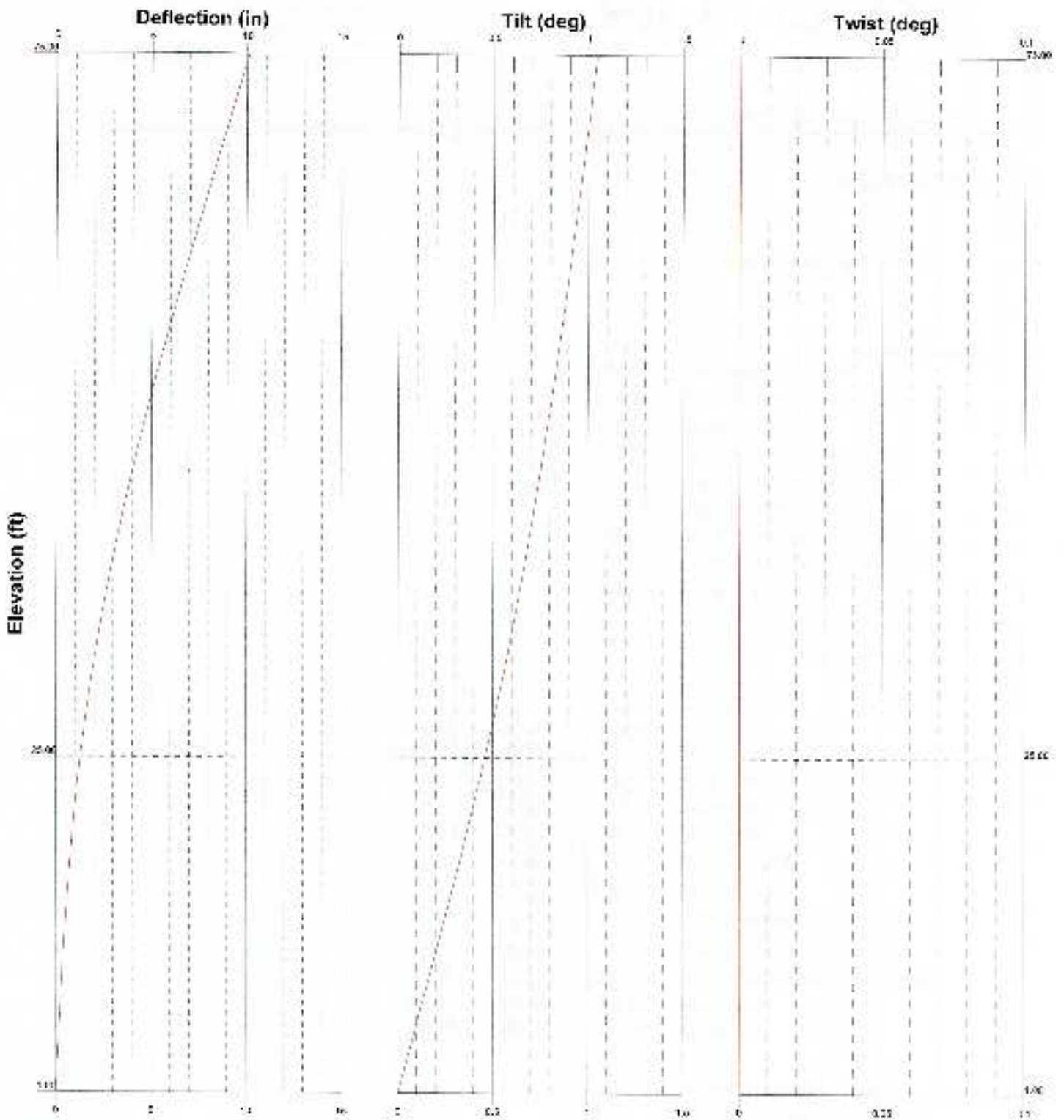
Vz

Mx

Mz



<b>Vector Structural Engineering</b>		<b>Spoke</b>	
651 W Calera Park Blvd		ProJd 00142.2054.242	
Draper, UT 84020		Proj: TIA-222-H	Drawn: MTC
Phone: (801) 950-1775		Proj: TIA-222-H	Scale: NTS
FAX: (801) 580-1776		Proj: TIA-222-H	Drawn: E. J.



<b>Vector Structural Engineering</b>		<b>Spike</b>	
651 W Galena Park Blvd Draper, UT 84020 Phone: (801) 943-1775 FAX: (801) 940-1775		Project: 00142.2054.242	
Drawn by: mmm	Checked by: mmm	Date: 10/25/24	Scale: 1/8" = 1'-0"
Project: TIA-222-H	Date: 10/25/24	Drawn by: mmm	Checked by: mmm



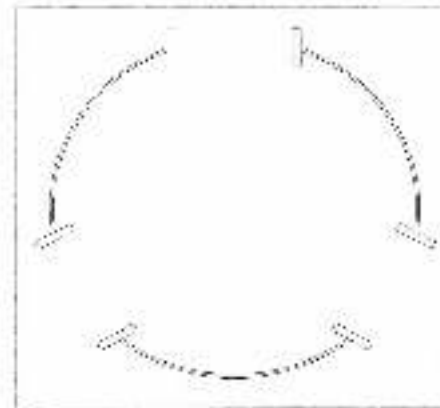
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PROJECT: NM01-148 SPIKE

**Port Design:**

Label: Ports at 70 ft A.G.L.

Geometry Input

Elevation of Port, AGL	70.00	ft
Pole Diameter	21.975	in
Pole Thickness	0.1875	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	11.0	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	3/8	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	3	

	Port 1	Port 2	Port 3
Azimuth (°)	0	120	240
Height (in)	12	12	12
Width (in)	8	8	8
Depth (in)	2.5	2.5	2.5
Thickness (in)	0.5	0.5	0.5
Projection (in)	0.5	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	2.5	2.5	2.5
Pole Area Removed (in <sup>2</sup> )	1.54	1.54	1.54
Dist. From Center to Reinf. (in)	10.2375	10.2375	10.2375
Area Check	79.9%	79.9%	79.9%
MOI Check	85.0%	85.0%	85.0%
Individual Port Weights (lbs)	14	14	14
Reduction in Pole Weight (lbs)	16		
Total Port Weight (lbs)	27		



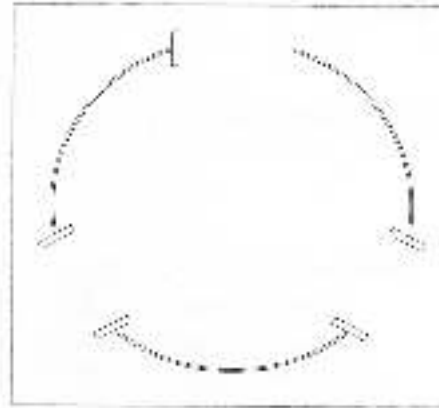
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PROJECT: NM01 148 SPIKE

## Port Design:

Label: Ports at 60 ft A.G.L.



### Geometry Input

Elevation of Port, AGL	60.00	ft
Pole Diameter	23.925	in
Pole Thickness	0.1875	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	11.0	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	3/8	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	3	

	Port 1	Port 2	Port 3
Azimuth (°)	0	120	240
Height (in)	12	12	12
Width (in)	8	8	8
Depth (in)	2.5	2.5	2.5
Thickness (in)	0.5	0.5	0.5
Projection (in)	0.5	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	2.5	2.5	2.5
Pole Area Removed (in <sup>2</sup> )	1.53	1.53	1.53
Dist. From Center to Reinf. (in)	11.2125	11.2125	11.2125
Area Check	79.6%	79.6%	79.6%
MOI Check	84.2%	84.2%	84.2%
Individual Port Weights (lbs)	14	14	14
Reduction in Pole Weight (lbs)	16		
Total Port Weight (lbs)	27		



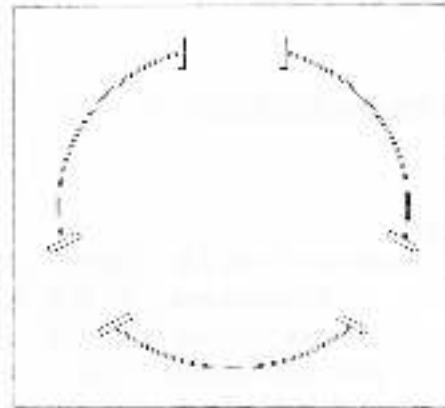
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PROJECT: NM01-148 SPIKE

## Port Design:

Label: Ports at 50 ft A.G.L.



### Geometry Input

Elevation of Port, AGL	50.00	ft
Pole Diameter	25.875	in
Pole Thickness	0.1875	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	11.0	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	3/8	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	3	

	Port 1	Port 2	Port 3
Azimuth (°)	0	120	240
Height (in)	12	12	12
Width (in)	8	8	8
Depth (in)	2.5	2.5	2.5
Thickness (in)	0.5	0.5	0.5
Projection (in)	0.5	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	2.5	2.5	2.5
Pole Area Removed (in <sup>2</sup> )	1.53	1.53	1.53
Dist. From Center to Reinf. (in)	12.1875	12.1875	12.1875
Area Check	79.3%	79.3%	79.3%
MOI Check	83.6%	83.6%	83.6%
Individual Port Weights (lbs)	14	14	14
Reduction in Pole Weight (lbs)	16		
Total Port Weight (lbs)	27		



JOB NO.: U0142.2054.242

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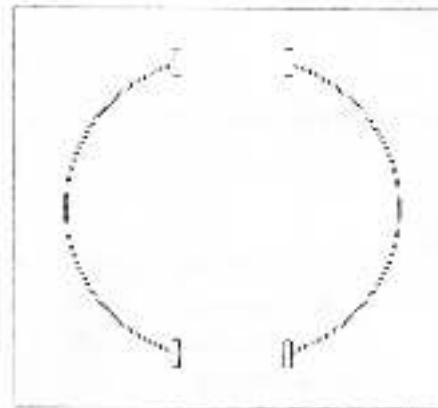
PROJECT: NM01-148 SPIKE

## Port Design:

Label: Ports at 7 ft A.G.L.

### Geometry Input

Elevation of Port, AGI	7.00	ft
Pole Diameter	33.885	in
Pole Thickness	0.25	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	14.5	k/in
Weld Filler Strength	70	ksi
Required Fillet Weld	1/2	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	2	



	Port 1	Port 2
Azimuth (°)	0	180
Height (in)	24	24
Width (in)	12	12
Depth (in)	3	3
Thickness (in)	0.75	0.75
Projection (in)	0.5	0.5
Reinforcing Area (in <sup>2</sup> )	4.5	4.5
Pole Area Removed (in <sup>2</sup> )	3.07	3.07
Dist. From Center to Reinf. (in)	15.9425	15.9425
Area Check	88.6%	88.6%
MOI Check	93.5%	93.5%
Individual Port Weights (lbs)	45	45
Reduction in Pole Weight (lbs)	42	
Total Port Weight (lbs)	50	



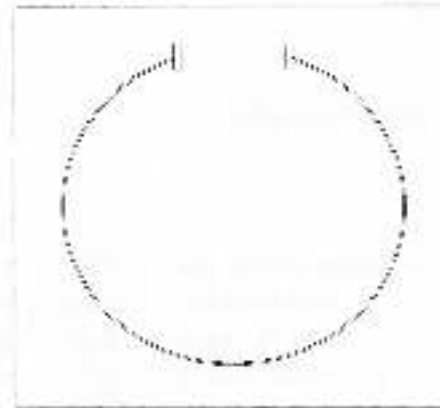
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PROJECT: NM01-148 SPIKE

## Port Design:

Label: Ports at 3 ft A.G.L.



### Geometry Input

Elevation of Port, AGL	3.00	ft
Pole Diameter	34.665	in
Pole Thickness	0.25	in
Pole Yield Strength	65	ksi
Pole Unit Tensile Strength	14.6	k/in
Weld Filler Strength:	70	ksi
Required Fillet Weld:	1/2	in
Reinforcing Rim Yield Strength	50	ksi
# of Ports	1	

	Port 1
Azimuth (°)	0
Height (in)	24
Width (in)	12
Depth (in)	3
Thickness (in)	0.75
Projection (in)	0.5
Reinforcing Area (in <sup>2</sup> )	4.5
Pole Area Removed (in <sup>2</sup> )	3.06
Dist. From Center to Reinf. (in)	16.3325
Area Check	88.5%
MOI Check	93.3%
Individual Port Weights (lbs)	46
Reduction in Pole Weight (lbs)	23
Total Port Weight (lbs)	23



JOB NO.: 110112.2054.242

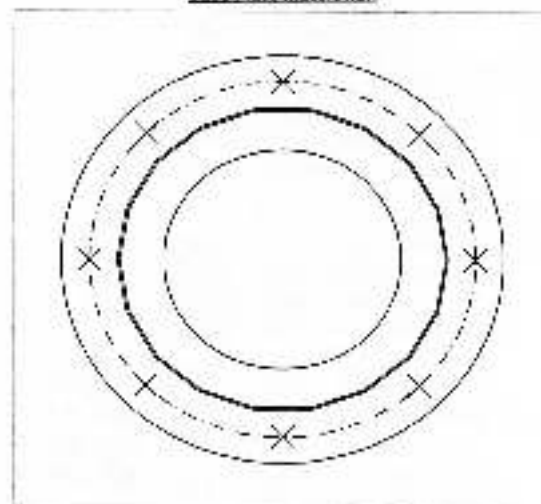
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PROJECT: AM01-148 SPIKE

### Monopole Baseplate & Anchorage Design per TIA-222-H Annex Q & IIA-222-H Section 4.9.9

Quantity	Symbol	Value	Units
Number of sides		18	
Flat O.D.	$D_p$	35.06	in
Plate wall thickness	$t_p$	0.25	in
Plate yield strength	$F_y$	65	ksi
Bore Radius		1	in
Base plate fillet or weld size		0.25	in
Anchor diameter	$d$	2.25	in
Number of anchors	$n$	8	
Anchor grade		A615-75	
Base plate thickness	$t_b$	2.25	in
Base plate yield strength	$F_y$	53	ksi
Anchor hole diameter		2.625	in
Slotted to outside edge?		No	
Hat washer diameter	$c$		
Eye-bolt hole diameter		2.625	
Eye-bolt circle		30.5	in
Bolt end diameter	$D_b$	41.5	in
Plate O.D.	$D_p$	47.5	in
Plate I.D.		25.5	in

Base Plate Illustration



LRFD Loads	Symbol	Value	Units	
			Wind	Seismic
Axial down	$R_{ax}$	26.27	k	3.00 k
Axial up	$R_{ax}$	0	k	3.00 k
Shear	$V_x$	16.53	k	3.00 k
Moment	$M_x$	953.14	k-ft	3.00 k-ft
Member min. capacity	$\phi V_n$	152	k-ft	

Fit Check

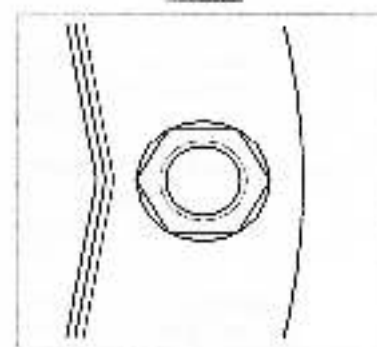


Plate stress ratio		46.8%	OK
Anchor rod girth		55.0%	OK
Min. number of sides		18	OK 6 minimum
Min. number of anchors		8	OK 8 minimum
Max. anchor rod to plate distance		3.1"	OK 18.5" maximum
Min. anchor diameter		2.25"	OK 0.75" minimum
Max. anchor rod spacing		16.3"	NG 18.5" maximum
Min. anchor rod spacing		15.88"	OK 6.75" minimum
Min. base plate thickness		2.25"	OK 2" minimum
Min. inside diameter		25.5"	OK 13.52" minimum
Max. inside diameter		25.5"	OK 31.125" maximum

Note: when number of anchors is less than minimum and when maximum anchor rod spacing is exceeded, adjustments are made to the effective plate width calculations as if requirements of TIA-222-H Annex Q were met.

Check	Dist.	Result
Washer vs weld	0.5333	OK
Washer vs DD	0.8125	OK
Washer covers hole	0.5	OK



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PROJECT: NM01-146 SPIKE

## Anchorage Embedment Design

(per ACI 318-19)

Vertical Bar Size:	#8
# of Vertical Bars:	22
Concrete Compressive Strength (psi):	4000
Pier Diameter (ft):	5.5
Pier Depth (ft):	20
Top of Pier Elevation (in):	6
Concrete Volume (yd <sup>3</sup> ):	19.0
Side Concrete Cover (in):	4
Top Concrete Cover (in):	2
Horizontal Tie Size:	#4
Bot. Circle Diameter (in):	41.5
# of Anchor Rods:	8
Anchor Rod Diameter (in):	2.25
$\psi_t$ (bar location factor):	1.0
$\psi_e$ (epoxy coating factor):	1.0
$\psi_s$ (bar size factor):	1.0
$\lambda$ (concrete type factor):	1.0
Vertical Bar Diameter (in):	1.0
Horizontal Tie Diameter (in):	0.500
Buffer (in):	4.25
Req'd Lap Length (in):	37.0
Min. Req'd Embedment Depth (in):	48.2

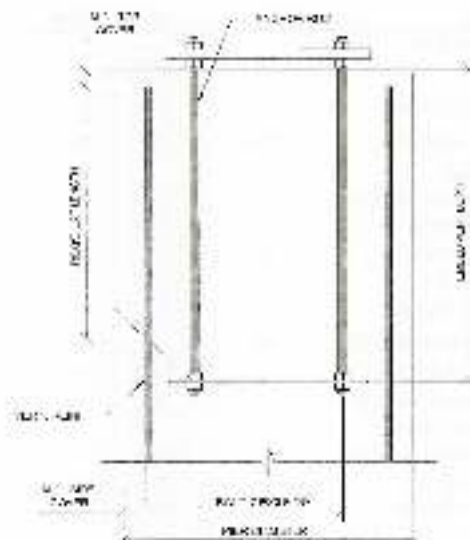
Table 25.4.2.4

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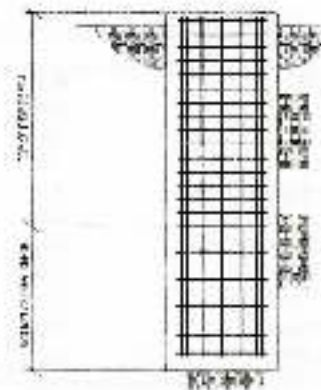
Table 25.4.2.4

in (Section 25.4.2.3)



## Transverse Reinforcement Design

Seismic Design Category:	C
Apply Seismic Detailing?	No
Site Class:	C
Type of Transverse Reinforcement:	Spiral
Transverse $f_y$ (ksi):	80
Seismic Hooks Required?	No
Tie Size OK?	Yes
Spacing at Top of Pier (in):	12
Spacing at Bottom of Pier (in):	12
Total Pier Length (ft):	20.5
Top Pier Length (ft):	20.5
Bottom Pier Length (ft):	0





JOB NO.: U0142.2054.242

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Project: NM01-148 SPIKE

**Drilled Pier Design:****Applied Loads:**

Max. shear, V:	22.2	k
Max. moment, M:	1,286.9	k-ft
Max. downl. $P_{down}$ :	35.0	k
Max. uplift, $P_{up}$ :	0.0	k

Design methodology:	LRFD
Maximum foundation rating:	100%

**Pier Properties:**

Pier shape:	Round
Pier diameter, b:	5.5 ft
Min. pier diameter, b <sub>min</sub> (opt):	3.0 ft
c:	5.5
Top of pier elevation:	0.5 ft
Pier depth, d:	20 ft
Min. pier depth, d <sub>min</sub> (opt):	0.0 ft

Volume of concrete:	487	ft <sup>3</sup>
Volume of concrete:	15.0	yd <sup>3</sup>
Weight of concrete:	73.1	k

**Soil Properties & Analysis:**

Allow. bearing pressure:	55,600	psf
Gross or net?	Net	
1/3 increase for short term loads?	No	
Skin friction (down):	0	psf
Skin friction (uplift):	0	psf
Top length to ignore:	2.75	ft
1/3 increase for short term loads?	No	
Combine skin friction w/ end bearing?	No	
Bearing capacity:	1,058.0	k
Uplift capacity:	65.8	k

F.S.: 1

F.S.: 1

F.S.: 1

**Results:**

Bearing capacity OK.  
 Uplift capacity OK.

Lateral analysis in LPile



JOB NO.: L0149 2024 242

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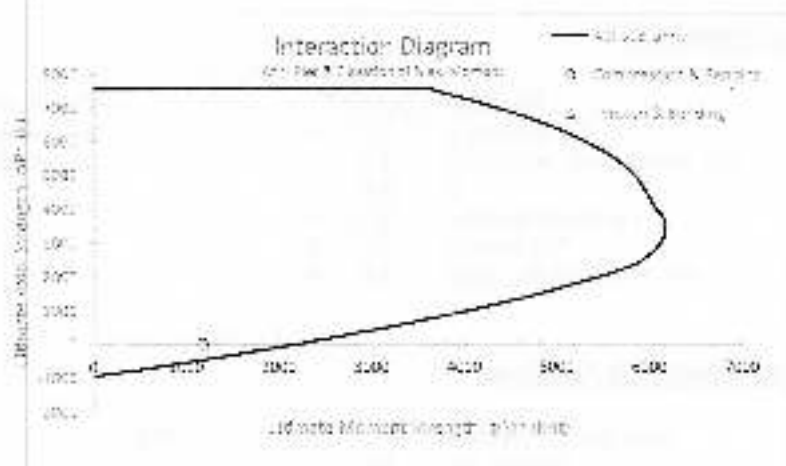
PROJECT: NMC -145 Splice

**Drilled Pier Reinforcement:****Design Requirements:**

Max. Moment, $M$ (k-ft)	950.1	Max. Down, $P_{\text{down}}$ (k)	23.3	Required Foundation UC Limit	100%
Max. Shear, $V$ (k)	16.6	Max. Uplift, $P_{\text{up}}$ (k)	0.0	$M_n/M_u$ (k-ft) (k-ft)	1183.7
Height of $V$ (ft)	13.535	Flexibility for $P$ (ft)	0	(Uplift is negative for comparison w/ Interaction Diagram)	
		Concrete Self-weight (k)	47.7	(0.145 acf)	

**Pier Properties:**

Code Reference	ACI 318-19
Pier Diameter (ft)	3.5
Top of Pier Elevation (ft)	6
Pier Depth (ft)	20
Vertical Bar Size	#8
Bar Diameter (in)	1
Bar Area (in <sup>2</sup> )	0.79
Seismic Design Category	C
# of Vertical Bars	22
Vert. Yield Strength (ksi)	50000
Horizontal Reinf. Type	Spiral
Horizontal Reinf. Size	#4
Horizontal Reinf. Diameter (in)	0.5
Spiral Concrete Cover (in)	4
Vert. Edge Distance (in)	4.5
Conc. Comp. Strength, $f_c$ (ksi)	4300
Angle Between Bars, $\theta$ (radians)	0.263
Area of Steel (in <sup>2</sup> )	17.4
Gross Column Area (in <sup>2</sup> )	3921.2
Min. Reinforcement Ratio	0.53%
$\rho_s$	0.95
Concrete Yield Strain, $\epsilon_y$ (in/in)	0.003
$\beta_1$ (k)	1.0818
$\alpha$	0.75
$\gamma$ Factor	0.80
$\phi_P$ (pure compression, k)	0.75
$E_s$ (ksi)	29000
Max. Steel Strain, $\epsilon_s$ (in/in)	0.002065
Number of Verticals in top row	7

**Axial & Bending Checks:**

Steel/Concrete Ratio: 0.51% &gt; Min. Reinf. Ratio

Compression &amp; Bending

 @  $V$  Pier     @ Max.  $M$ 

$\phi P_n$ (k)	13.7	52.5
$\phi M_n$ (k-ft)	2222.8	2310.2
UC	50.1%	51.1%

UC	50.1%	51.1%
----	-------	-------

OK, Adequate

$$(\phi P_n)^2 + (M_u)^2 \leq (\phi P_n)^2 + (M_u)^2$$

Tension &amp; Bending

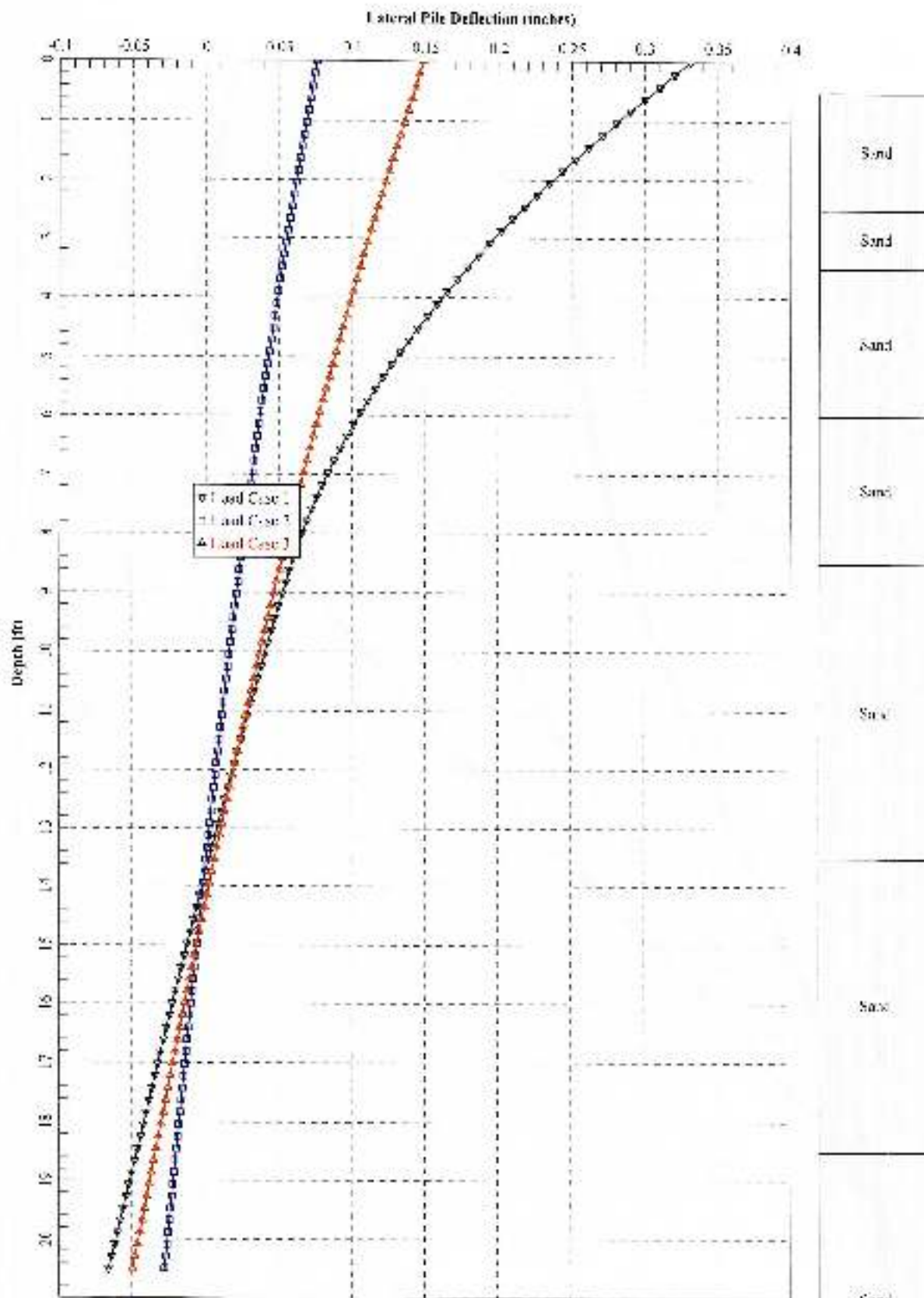
 @  $V$  Pier     @ Max.  $M$ 

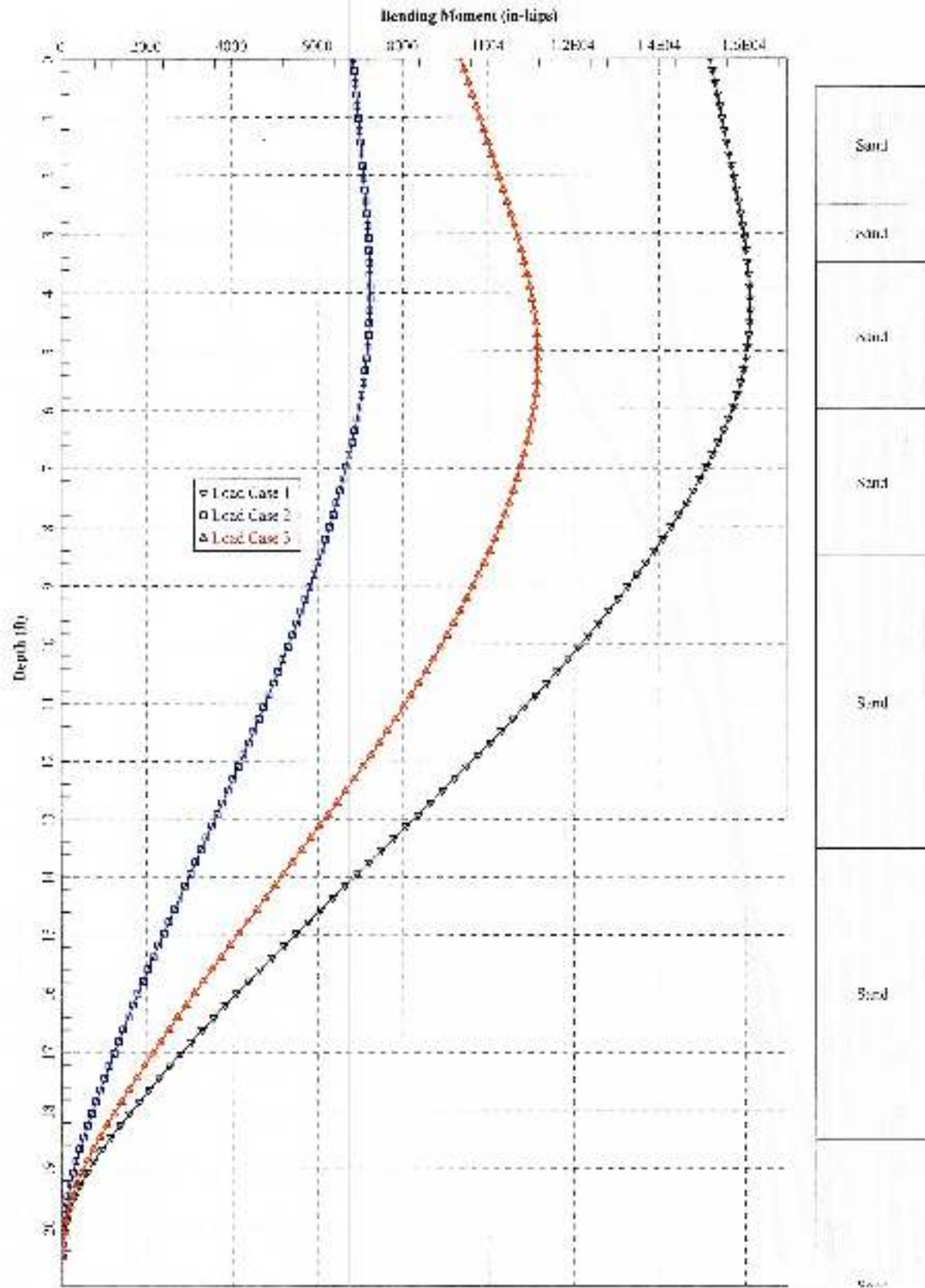
$\phi P_n$ (k)	0.0	42.8
$\phi M_n$ (k-ft)	2182.5	2270.1
UC	54.1%	52.0%

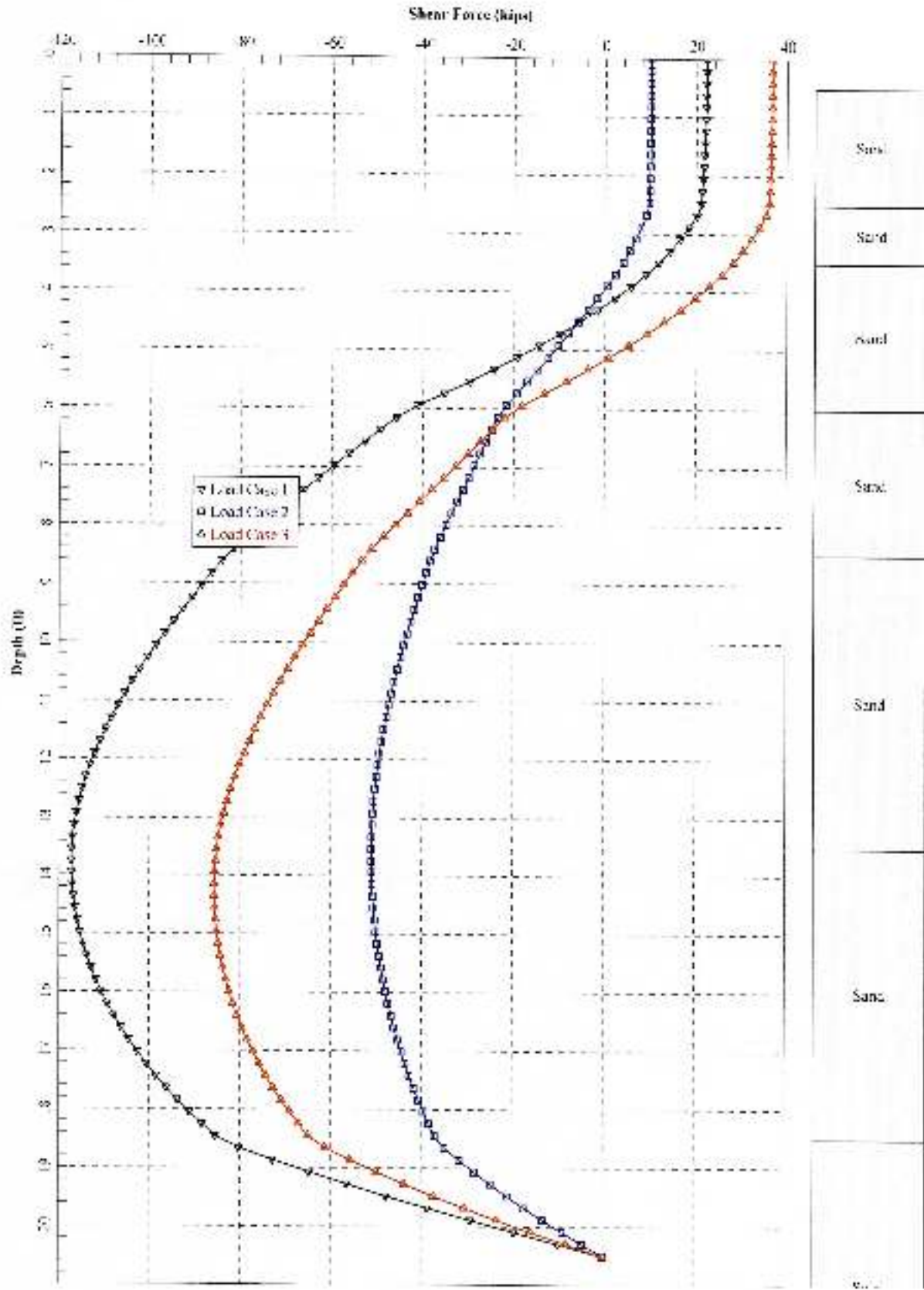
UC	54.1%	52.0%
----	-------	-------

OK, Adequate

$$(\phi P_n)^2 + (M_u)^2 \leq (\phi P_n)^2 + (M_u)^2$$







UNITED STATES DEPARTMENT OF COMMERCE  
 Analysis of Individual Files under Title 19, U.S.C.  
 Suspected of Violating Section 337 of the Tariff Act  
 I 188-273 (a) (b) (c) (d)  
 U.S. Trade Policy

Title Case # 1736 (a) (b) (c) (d)

NAI  
 457

Case Number or Priority Number: 188-273

Title Case # 1736 (a) (b) (c) (d) (e) (f) (g) (h) (i) (j) (k) (l) (m) (n) (o) (p) (q) (r) (s) (t) (u) (v) (w) (x) (y) (z)

Senior Structural Engineer, U.S.

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Files used for analysis

File # File Location  
 188-273 (a) (b) (c) (d) (e) (f) (g) (h) (i) (j) (k) (l) (m) (n) (o) (p) (q) (r) (s) (t) (u) (v) (w) (x) (y) (z)

Name of Input Data File:  
 188-273 (a) (b) (c) (d) (e) (f) (g) (h) (i) (j) (k) (l) (m) (n) (o) (p) (q) (r) (s) (t) (u) (v) (w) (x) (y) (z)

Name of Output Report File:  
 188-273 (a) (b) (c) (d) (e) (f) (g) (h) (i) (j) (k) (l) (m) (n) (o) (p) (q) (r) (s) (t) (u) (v) (w) (x) (y) (z)

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Date and Time of Analysis

Date: October 14, 1974

Time: 11:21:42

Program Title

UNITED STATES DEPARTMENT OF COMMERCE

Job Number: 188-273 (a) (b) (c) (d)

Class: GROUP

Program: 188-273

Description:

Program Details and Settings

Computational Options:  
 - Use unformatted data to compute the cross-section analysis  
 engineering units used for Data Input and Output Files  
 - Use the following system for file names, text, output:

- Analysis Input Options:
- Maximum number of iterations allowed: 100
  - Maximum number of iterations for convergence: 100,000.00
  - Maximum allowable deflection: 100,000.00
  - Maximum of pile increments: 100

Loading Type and Number of Cycles of Loading:  
 - Static Loading condition

- Use of pile cap flexibility factors for design of pile caps
- Analysis using varying overburden (method of slices, etc.)
- Axial stresses in pile loads are accurate
- Loading by lateral loads, moments acting on pile cap, etc.
- Input of shear resistance at the pile tip is not required
- Input of moment resistance at the pile tip is not required
- Specification of pile head (flexural) stiffness is not required
- Non-linear analysis of pile cap is not required
- Modeling analysis of pile cap is not required

Other Options:

- Where piles are located within a level defined by grade.
- Where pile head deflection, bending moment, shear force, and axial stress are required for full length of pile.
- Where treatment (lead) spacing of output is required.
- Where results are computed and reported in a convenient table.
- Where results are printed on paper.

Pile Structural Analysis and Capacity

Number of pile sections analyzed: 1  
 Total length of pile: 24.000 ft  
 Depth of ground surface below pile cap: 2.000 ft

Pile diameter used for pile cap design is 12.000 ft.

Cap loads are computed using pile flexibilities interpolated with cap size. The length of the pile is a function of the pile diameter as shown below.

Level	Layer Below	Pile
No.	Height	Thickness
	feet	feet
1	2.000	12.000
2	22.000	12.000

Layer Structural Properties for Pile Analysis

Pile Section No. 1:

Section 1 is a circular pile with a constant diameter of 12.000 ft.  
 Length of section: 24.0000 ft  
 Shaft diameter: 12.0000 ft

Clear capacity of section: 1.000 ft

Ground Slope and Pile Axial Angles

Ground slope angle: 0.200 degrees  
 0.200 radians  
 Pile axial angle: 0.000 degrees  
 0.000 radians

Soil and Pile Layering Data

The soil profile is made of three layers.

Layer 1 is sand, properties by Davis et al., 1974

Distance from top of pile to top of layer: 2.0000 ft  
 Distance from top of pile to bottom of layer: 2.0000 ft  
 Thickness of soil in layer of layer: 0.0000 ft  
 Density of soil in layer of layer: 120.0000 lb/ft<sup>3</sup>  
 Friction angle of soil in layer of layer: 30.0000 deg  
 Surcharge at top of layer: 1.0000 psf  
 Surcharge at bottom of layer: 1.0000 psf

NOTE: default values for soil properties will be computed for this layer.

Layer 2 is sand, properties by Davis et al., 1974

Distance from top of pile to top of layer: 2.0000 ft  
 Distance from top of pile to bottom of layer: 2.0000 ft  
 Effective soil weight at top of layer: 115.0000 pcf  
 Effective soil weight at bottom of layer: 115.0000 pcf  
 Friction angle of soil in layer: 30.0000 deg  
 Density of soil in layer of layer: 120.0000 lb/ft<sup>3</sup>  
 Surcharge at top of layer: 1.0000 psf  
 Surcharge at bottom of layer: 1.0000 psf

NOTE: default values for soil properties will be computed for this layer.

Layer 3 is sand, properties by Davis et al., 1974



NOTE: default values for saggrade 2 will be computed for this layer.

Layer 11 to 15, soil properties by Fines et al., 1984

- Thickness from top of pile to top of layer = 35.22000 ft
- Thickness from top of pile to bottom of layer = 41.22000 ft
- Relative unit weight at top of layer = 120.22000 pcf
- Relative unit weight at bottom of layer = 120.22000 pcf
- Friction angle at top of layer = 40.22000 deg.
- Friction angle at bottom of layer = 40.22000 deg.
- Saggrade 2 at top of layer = 2.0000 pcf
- Saggrade 2 at bottom of layer = 2.0000 pcf

NOTE: default values for saggrade 2 will be computed for this layer.

Layer 16 to 20, soil properties by Fines et al., 1984

- Thickness from top of pile to top of layer = 27.00000 ft
- Thickness from top of pile to bottom of layer = 28.00000 ft
- Relative unit weight at top of layer = 118.00000 pcf
- Relative unit weight at bottom of layer = 118.00000 pcf
- Friction angle at top of layer = 45.00000 deg.
- Friction angle at bottom of layer = 45.00000 deg.
- Saggrade 2 at top of layer = 2.0000 pcf
- Saggrade 2 at bottom of layer = 2.0000 pcf

NOTE: default values for saggrade 2 will be computed for this layer.

Layer 21 to 25, soil properties by Fines et al., 1984

- Thickness from top of pile to top of layer = 48.00000 ft
- Thickness from top of pile to bottom of layer = 53.00000 ft
- Relative unit weight at top of layer = 118.00000 pcf
- Relative unit weight at bottom of layer = 118.00000 pcf
- Friction angle at top of layer = 45.00000 deg.
- Friction angle at bottom of layer = 45.00000 deg.
- Saggrade 2 at top of layer = 2.0000 pcf
- Saggrade 2 at bottom of layer = 2.0000 pcf

NOTE: default values for saggrade 2 will be computed for this layer.

Characteristics of the ground soil layer extends over an 8' radius (8' dia. tip)

Summary of Final Soil Properties

Layer	Soil Type	Layer	Thickness	Angle of
-------	-----------	-------	-----------	----------

Layer No.	Soil Type	Unit Wt. pcf	Friction Ang. deg.	Friction Coef.	Phi (deg)
1	SSM	7.000	118.0000	10.000	118.000
2	SSM, at SL1	7.000	118.0000	10.000	118.000
3	SSM	7.000	118.0000	10.000	118.000
4	SSM, at SL1	7.000	118.0000	10.000	118.000
5	SSM	8.000	118.0000	10.000	118.000
6	SSM, at SL1	8.000	118.0000	10.000	118.000
7	SSM	8.000	118.0000	10.000	118.000
8	SSM, at SL1	8.000	118.0000	10.000	118.000
9	SSM	10.000	118.0000	10.000	118.000
10	SSM, at SL1	10.000	118.0000	10.000	118.000
11	SSM	10.000	118.0000	10.000	118.000
12	SSM, at SL1	10.000	118.0000	10.000	118.000
13	SSM	10.000	118.0000	10.000	118.000
14	SSM, at SL1	10.000	118.0000	10.000	118.000
15	SSM	10.000	118.0000	10.000	118.000
16	SSM, at SL1	10.000	118.0000	10.000	118.000
17	SSM	10.000	118.0000	10.000	118.000
18	SSM, at SL1	10.000	118.0000	10.000	118.000
19	SSM	10.000	118.0000	10.000	118.000
20	SSM, at SL1	10.000	118.0000	10.000	118.000
21	SSM	10.000	118.0000	10.000	118.000
22	SSM, at SL1	10.000	118.0000	10.000	118.000
23	SSM	10.000	118.0000	10.000	118.000
24	SSM, at SL1	10.000	118.0000	10.000	118.000
25	SSM	10.000	118.0000	10.000	118.000

Soil Loading Data

NOTE: loading criteria were used when computing q values for all analyses.

Final Head Loading and Phi Values at a Point Load

Number of loads applied = 2

Load Case	Location	Capacity	Final Factor
1	1	2	Force, lbs

Node	Element	Material	Area	Length	Volume	Weight	Center of Gravity
1	2	1	0.0000	10.0000	0.0000	0.0000	5.0000
2	3	1	0.0000	10.0000	0.0000	0.0000	15.0000
3	4	1	0.0000	10.0000	0.0000	0.0000	25.0000

p = wind force applied normal to pile shaft  
 q = wind pressure applied to pile face  
 r = lateral deflection normal to pile axis  
 s = pile slope relative to original pile shaft angle  
 u = horizontal deflection applied to pile head  
 v = vertical deflection applied to pile head  
 w = pile length  
 x = horizontal distance from pile base to point of interest  
 y = vertical distance from pile base to point of interest  
 z = distance from pile base to point of interest

**Material Properties: Modulus of Elasticity and Axial Stiffness**

Modulus of Elasticity values were determined from allowed loading conditions.

Number of Pile Sections Analyzed = 1

Pile Section No. 1:

**Dimensions and Properties of Pile Section 1 (ft)**

Length of Section	=	25.0000	ft
Shaft Diameter	=	25.0000	in
Concrete Cover Thickness (to face of reinforcement)	=	1.5000	in
Radius of Reinforcing Bars	=	0.5000	in
Yield Stress of Reinforcing Bars	=	60000	psi
Modulus of Elasticity of Reinforcing Bars	=	29000000	psi
Area of Steel	=	2.0000	sq ft
Area of Reinforcing Steel	=	27.8700	sq ft
Area Ratio of Steel Reinforcement	=	0.0718	
Modulus of Elasticity of Concrete	=	4.0300	psi
Area of Concrete Aggregate Core	=	2.0000	sq ft
Area of Steel Applied to Aggregate Core	=	0.0000	sq ft
Offset of Center of Reinforcing Bars from Center of Core	=	0.0000	ft

**Node Structural Dependencies:**

Node 1: Initial structural dependency	=	0.0000	lb
Node 2: Initial structural dependency	=	0.0000	lb
Node 3: Initial structural dependency	=	0.0000	lb

**Node Loading and Restraints and Restraints: Load Case Combinations:**

Case	Node 1	Node 2	Node 3	Node 4	Node 5
1	0.0000	0.0000	0.0000	0.0000	0.0000
2	0.0000	0.0000	0.0000	0.0000	0.0000
3	0.0000	0.0000	0.0000	0.0000	0.0000
4	0.0000	0.0000	0.0000	0.0000	0.0000
5	0.0000	0.0000	0.0000	0.0000	0.0000
6	0.0000	0.0000	0.0000	0.0000	0.0000
7	0.0000	0.0000	0.0000	0.0000	0.0000
8	0.0000	0.0000	0.0000	0.0000	0.0000
9	0.0000	0.0000	0.0000	0.0000	0.0000
10	0.0000	0.0000	0.0000	0.0000	0.0000
11	0.0000	0.0000	0.0000	0.0000	0.0000
12	0.0000	0.0000	0.0000	0.0000	0.0000
13	0.0000	0.0000	0.0000	0.0000	0.0000
14	0.0000	0.0000	0.0000	0.0000	0.0000
15	0.0000	0.0000	0.0000	0.0000	0.0000
16	0.0000	0.0000	0.0000	0.0000	0.0000
17	0.0000	0.0000	0.0000	0.0000	0.0000
18	0.0000	0.0000	0.0000	0.0000	0.0000
19	0.0000	0.0000	0.0000	0.0000	0.0000
20	0.0000	0.0000	0.0000	0.0000	0.0000
21	0.0000	0.0000	0.0000	0.0000	0.0000
22	0.0000	0.0000	0.0000	0.0000	0.0000

Note: The positions of the above restraints were determined by UTM.

Minimum spacing between reinforcement bars = 1.5000 ft = 18.0000 in.

Value of axial spacing to maximum aggregate size = 0.00

**Concrete Properties:**

Compressive Strength of Concrete	=	4000	psi
Modulus of Elasticity of Concrete	=	4.0300	psi
Modulus of Rigidity of Concrete	=	1570000	psi
Compressive Strain at Peak Stress	=	0.0020	
Modulus of Elasticity of Concrete	=	4.0300	psi





1.0235022	27121	0396071	17 557212	1.000120	-0.004604	1.000120	7702770	10.120818	0.001702	-0.017085
1.0235023	27122	0416292	17 574222	1.000121	-0.004711	1.000121	7702771	10.120818	0.001702	-0.017085
1.0235024	27123	0436413	17 591232	1.000121	-0.004820	1.000121	7702772	10.120818	0.001702	-0.017085
1.0235025	27124	0456534	17 608242	1.000122	-0.004930	1.000122	7702773	10.120818	0.001702	-0.017085
1.0235026	27125	0476655	17 625252	1.000122	-0.005040	1.000122	7702774	10.120818	0.001702	-0.017085
1.0235027	27126	0496776	17 642262	1.000123	-0.005150	1.000123	7702775	10.120818	0.001702	-0.017085
1.0235028	27127	0516897	17 659272	1.000123	-0.005260	1.000123	7702776	10.120818	0.001702	-0.017085
1.0235029	27128	0537018	17 676282	1.000124	-0.005370	1.000124	7702777	10.120818	0.001702	-0.017085
1.0235030	27129	0557139	17 693292	1.000124	-0.005480	1.000124	7702778	10.120818	0.001702	-0.017085
1.0235031	27130	0577260	17 710302	1.000125	-0.005590	1.000125	7702779	10.120818	0.001702	-0.017085
1.0235032	27131	0597381	17 727312	1.000125	-0.005700	1.000125	7702780	10.120818	0.001702	-0.017085
1.0235033	27132	0617502	17 744322	1.000126	-0.005810	1.000126	7702781	10.120818	0.001702	-0.017085
1.0235034	27133	0637623	17 761332	1.000126	-0.005920	1.000126	7702782	10.120818	0.001702	-0.017085
1.0235035	27134	0657744	17 778342	1.000127	-0.006030	1.000127	7702783	10.120818	0.001702	-0.017085
1.0235036	27135	0677865	17 795352	1.000127	-0.006140	1.000127	7702784	10.120818	0.001702	-0.017085
1.0235037	27136	0697986	17 812362	1.000128	-0.006250	1.000128	7702785	10.120818	0.001702	-0.017085
1.0235038	27137	0718107	17 829372	1.000128	-0.006360	1.000128	7702786	10.120818	0.001702	-0.017085
1.0235039	27138	0738228	17 846382	1.000129	-0.006470	1.000129	7702787	10.120818	0.001702	-0.017085
1.0235040	27139	0758349	17 863392	1.000129	-0.006580	1.000129	7702788	10.120818	0.001702	-0.017085
1.0235041	27140	0778470	17 880402	1.000130	-0.006690	1.000130	7702789	10.120818	0.001702	-0.017085
1.0235042	27141	0798591	17 897412	1.000130	-0.006800	1.000130	7702790	10.120818	0.001702	-0.017085
1.0235043	27142	0818712	17 914422	1.000131	-0.006910	1.000131	7702791	10.120818	0.001702	-0.017085
1.0235044	27143	0838833	17 931432	1.000131	-0.007020	1.000131	7702792	10.120818	0.001702	-0.017085
1.0235045	27144	0858954	17 948442	1.000132	-0.007130	1.000132	7702793	10.120818	0.001702	-0.017085
1.0235046	27145	0879075	17 965452	1.000132	-0.007240	1.000132	7702794	10.120818	0.001702	-0.017085
1.0235047	27146	0899196	17 982462	1.000133	-0.007350	1.000133	7702795	10.120818	0.001702	-0.017085
1.0235048	27147	0919317	17 999472	1.000133	-0.007460	1.000133	7702796	10.120818	0.001702	-0.017085
1.0235049	27148	0939438	18 016482	1.000134	-0.007570	1.000134	7702797	10.120818	0.001702	-0.017085
1.0235050	27149	0959559	18 033492	1.000134	-0.007680	1.000134	7702798	10.120818	0.001702	-0.017085
1.0235051	27150	0979680	18 050502	1.000135	-0.007790	1.000135	7702799	10.120818	0.001702	-0.017085
1.0235052	27151	0999801	18 067512	1.000135	-0.007900	1.000135	7702800	10.120818	0.001702	-0.017085
1.0235053	27152	1019922	18 084522	1.000136	-0.008010	1.000136	7702801	10.120818	0.001702	-0.017085
1.0235054	27153	1040043	18 101532	1.000136	-0.008120	1.000136	7702802	10.120818	0.001702	-0.017085
1.0235055	27154	1060164	18 118542	1.000137	-0.008230	1.000137	7702803	10.120818	0.001702	-0.017085
1.0235056	27155	1080285	18 135552	1.000137	-0.008340	1.000137	7702804	10.120818	0.001702	-0.017085
1.0235057	27156	1100406	18 152562	1.000138	-0.008450	1.000138	7702805	10.120818	0.001702	-0.017085
1.0235058	27157	1120527	18 169572	1.000138	-0.008560	1.000138	7702806	10.120818	0.001702	-0.017085
1.0235059	27158	1140648	18 186582	1.000139	-0.008670	1.000139	7702807	10.120818	0.001702	-0.017085
1.0235060	27159	1160769	18 203592	1.000139	-0.008780	1.000139	7702808	10.120818	0.001702	-0.017085
1.0235061	27160	1180890	18 220602	1.000140	-0.008890	1.000140	7702809	10.120818	0.001702	-0.017085
1.0235062	27161	1201011	18 237612	1.000140	-0.009000	1.000140	7702810	10.120818	0.001702	-0.017085
1.0235063	27162	1221132	18 254622	1.000141	-0.009110	1.000141	7702811	10.120818	0.001702	-0.017085
1.0235064	27163	1241253	18 271632	1.000141	-0.009220	1.000141	7702812	10.120818	0.001702	-0.017085
1.0235065	27164	1261374	18 288642	1.000142	-0.009330	1.000142	7702813	10.120818	0.001702	-0.017085
1.0235066	27165	1281495	18 305652	1.000142	-0.009440	1.000142	7702814	10.120818	0.001702	-0.017085
1.0235067	27166	1301616	18 322662	1.000143	-0.009550	1.000143	7702815	10.120818	0.001702	-0.017085
1.0235068	27167	1321737	18 339672	1.000143	-0.009660	1.000143	7702816	10.120818	0.001702	-0.017085
1.0235069	27168	1341858	18 356682	1.000144	-0.009770	1.000144	7702817	10.120818	0.001702	-0.017085
1.0235070	27169	1361979	18 373692	1.000144	-0.009880	1.000144	7702818	10.120818	0.001702	-0.017085
1.0235071	27170	1382100	18 390702	1.000145	-0.009990	1.000145	7702819	10.120818	0.001702	-0.017085
1.0235072	27171	1402221	18 407712	1.000145	-0.010100	1.000145	7702820	10.120818	0.001702	-0.017085
1.0235073	27172	1422342	18 424722	1.000146	-0.010210	1.000146	7702821	10.120818	0.001702	-0.017085
1.0235074	27173	1442463	18 441732	1.000146	-0.010320	1.000146	7702822	10.120818	0.001702	-0.017085
1.0235075	27174	1462584	18 458742	1.000147	-0.010430	1.000147	7702823	10.120818	0.001702	-0.017085
1.0235076	27175	1482705	18 475752	1.000147	-0.010540	1.000147	7702824	10.120818	0.001702	-0.017085
1.0235077	27176	1502826	18 492762	1.000148	-0.010650	1.000148	7702825	10.120818	0.001702	-0.017085
1.0235078	27177	1522947	18 509772	1.000148	-0.010760	1.000148	7702826	10.120818	0.001702	-0.017085
1.0235079	27178	1543068	18 526782	1.000149	-0.010870	1.000149	7702827	10.120818	0.001702	-0.017085
1.0235080	27179	1563189	18 543792	1.000149	-0.010980	1.000149	7702828	10.120818	0.001702	-0.017085
1.0235081	27180	1583310	18 560802	1.000150	-0.011090	1.000150	7702829	10.120818	0.001702	-0.017085
1.0235082	27181	1603431	18 577812	1.000150	-0.011200	1.000150	7702830	10.120818	0.001702	-0.017085
1.0235083	27182	1623552	18 594822	1.000151	-0.011310	1.000151	7702831	10.120818	0.001702	-0.017085
1.0235084	27183	1643673	18 611832	1.000151	-0.011420	1.000151	7702832	10.120818	0.001702	-0.017085
1.0235085	27184	1663794	18 628842	1.000152	-0.011530	1.000152	7702833	10.120818	0.001702	-0.017085
1.0235086	27185	1683915	18 645852	1.000152	-0.011640	1.000152	7702834	10.120818	0.001702	-0.017085
1.0235087	27186	1704036	18 662862	1.000153	-0.011750	1.000153	7702835	10.120818	0.001702	-0.017085
1.0235088	27187	1724157	18 679872	1.000153	-0.011860	1.000153	7702836	10.120818	0.001702	-0.017085
1.0235089	27188	1744278	18 696882	1.000154	-0.011970	1.000154	7702837	10.120818	0.001702	-0.017085
1.0235090	27189	1764399	18 713892	1.000154	-0.012080	1.000154	7702838	10.120818	0.001702	-0.017085
1.0235091	27190	1784520	18 730902	1.000155	-0.012190	1.000155	7702839	10.120818	0.001702	-0.017085
1.0235092	27191	1804641	18 747912	1.000155	-0.012300	1.000155	7702840	10.120818	0.001702	-0.017085
1.0235093	27192	1824762	18 764922	1.000156	-0.012410	1.000156	7702841	10.120818	0.001702	-0.017085
1.0235094	27193	1844883	18 781932	1.000156	-0.012520	1.000156	7702842	10.120818	0.001702	-0.017085
1.0235095	27194	1865004	18 798942	1.000157	-0.012630	1.000157	7702843	10.120818	0.001702	-0.017085
1.0235096	27195	1885125	18 815952	1.000157	-0.012740	1.000157	7702844	10.120818	0.001702	-0.017085
1.0235097	27196	1905246	18 832962	1.000158	-0.012850	1.000158	7702845	10.120818	0.001702	-0.017085
1.0235098	27197	1925367	18 850972	1.000158	-0.012960	1.000158	7702846	10.120818	0.001702	-0.017085
1.0235099	27198	1945488	18 867982	1.000159	-0.013070	1.000159	7702847	10.120818	0.001702	-0.017085
1.0235100	27199	1965609	18 884992	1.000159	-0.013180	1.000159	7702848	10.120818	0.001702	-0.017085
1.0235101	27200	1985730	18 902002	1.000160	-0.013290	1.000160	7702849	10.120818	0.001702	-0.017085
1.0235102	27201	2005851	18 919012	1.000160	-0.013400	1.000160	7702850	10.120818	0.001702	-0.017085
1.0235103	27202	2025972	18 936022	1.000161	-0.013510	1.000161	7702851	10.120818	0.001702	-0.017085
1.0235104	27203	2046093	18 953032	1.000161	-0.013620	1.000161	7702852	10.120818	0.001702	-0.017085
1.0235105	27204	2066214	18 970042	1.000162	-0.013730	1.000162	7702853	10.120818	0.001702	-0.017085
1.0235106	27205	2086335								





4.020642	2737	22276439	11.035324	1.961101	-4.034631
4.020643	-20.020623 CV	2713	18770931	1.961114	-4.034741
4.020644	2713	18770931	11.035325	1.961127	-4.034851
4.020645	2713	18770931	11.035326	1.961140	-4.034961
4.020646	2713	18770931	11.035327	1.961153	-4.035071
4.020647	2713	18770931	11.035328	1.961166	-4.035181
4.020648	2713	18770931	11.035329	1.961179	-4.035291
4.020649	2713	18770931	11.035330	1.961192	-4.035401
4.020650	2713	18770931	11.035331	1.961205	-4.035511
4.020651	2713	18770931	11.035332	1.961218	-4.035621
4.020652	2713	18770931	11.035333	1.961231	-4.035731
4.020653	2713	18770931	11.035334	1.961244	-4.035841
4.020654	2713	18770931	11.035335	1.961257	-4.035951
4.020655	2713	18770931	11.035336	1.961270	-4.036061
4.020656	2713	18770931	11.035337	1.961283	-4.036171
4.020657	2713	18770931	11.035338	1.961296	-4.036281
4.020658	2713	18770931	11.035339	1.961309	-4.036391
4.020659	2713	18770931	11.035340	1.961322	-4.036501
4.020660	2713	18770931	11.035341	1.961335	-4.036611
4.020661	2713	18770931	11.035342	1.961348	-4.036721
4.020662	2713	18770931	11.035343	1.961361	-4.036831
4.020663	2713	18770931	11.035344	1.961374	-4.036941
4.020664	2713	18770931	11.035345	1.961387	-4.037051
4.020665	2713	18770931	11.035346	1.961400	-4.037161
4.020666	2713	18770931	11.035347	1.961413	-4.037271
4.020667	2713	18770931	11.035348	1.961426	-4.037381
4.020668	2713	18770931	11.035349	1.961439	-4.037491
4.020669	2713	18770931	11.035350	1.961452	-4.037601
4.020670	2713	18770931	11.035351	1.961465	-4.037711
4.020671	2713	18770931	11.035352	1.961478	-4.037821
4.020672	2713	18770931	11.035353	1.961491	-4.037931
4.020673	2713	18770931	11.035354	1.961504	-4.038041
4.020674	2713	18770931	11.035355	1.961517	-4.038151
4.020675	2713	18770931	11.035356	1.961530	-4.038261
4.020676	2713	18770931	11.035357	1.961543	-4.038371
4.020677	2713	18770931	11.035358	1.961556	-4.038481
4.020678	2713	18770931	11.035359	1.961569	-4.038591
4.020679	2713	18770931	11.035360	1.961582	-4.038701
4.020680	2713	18770931	11.035361	1.961595	-4.038811
4.020681	2713	18770931	11.035362	1.961608	-4.038921
4.020682	2713	18770931	11.035363	1.961621	-4.039031
4.020683	2713	18770931	11.035364	1.961634	-4.039141
4.020684	2713	18770931	11.035365	1.961647	-4.039251
4.020685	2713	18770931	11.035366	1.961660	-4.039361
4.020686	2713	18770931	11.035367	1.961673	-4.039471
4.020687	2713	18770931	11.035368	1.961686	-4.039581
4.020688	2713	18770931	11.035369	1.961699	-4.039691
4.020689	2713	18770931	11.035370	1.961712	-4.039801
4.020690	2713	18770931	11.035371	1.961725	-4.039911
4.020691	2713	18770931	11.035372	1.961738	-4.040021
4.020692	2713	18770931	11.035373	1.961751	-4.040131
4.020693	2713	18770931	11.035374	1.961764	-4.040241
4.020694	2713	18770931	11.035375	1.961777	-4.040351
4.020695	2713	18770931	11.035376	1.961790	-4.040461
4.020696	2713	18770931	11.035377	1.961803	-4.040571
4.020697	2713	18770931	11.035378	1.961816	-4.040681
4.020698	2713	18770931	11.035379	1.961829	-4.040791
4.020699	2713	18770931	11.035380	1.961842	-4.040901
4.020700	2713	18770931	11.035381	1.961855	-4.041011
4.020701	2713	18770931	11.035382	1.961868	-4.041121
4.020702	2713	18770931	11.035383	1.961881	-4.041231
4.020703	2713	18770931	11.035384	1.961894	-4.041341
4.020704	2713	18770931	11.035385	1.961907	-4.041451
4.020705	2713	18770931	11.035386	1.961920	-4.041561
4.020706	2713	18770931	11.035387	1.961933	-4.041671
4.020707	2713	18770931	11.035388	1.961946	-4.041781
4.020708	2713	18770931	11.035389	1.961959	-4.041891
4.020709	2713	18770931	11.035390	1.961972	-4.042001
4.020710	2713	18770931	11.035391	1.961985	-4.042111
4.020711	2713	18770931	11.035392	1.961998	-4.042221
4.020712	2713	18770931	11.035393	1.962011	-4.042331
4.020713	2713	18770931	11.035394	1.962024	-4.042441
4.020714	2713	18770931	11.035395	1.962037	-4.042551
4.020715	2713	18770931	11.035396	1.962050	-4.042661
4.020716	2713	18770931	11.035397	1.962063	-4.042771
4.020717	2713	18770931	11.035398	1.962076	-4.042881
4.020718	2713	18770931	11.035399	1.962089	-4.042991
4.020719	2713	18770931	11.035400	1.962102	-4.043101
4.020720	2713	18770931	11.035401	1.962115	-4.043211
4.020721	2713	18770931	11.035402	1.962128	-4.043321
4.020722	2713	18770931	11.035403	1.962141	-4.043431
4.020723	2713	18770931	11.035404	1.962154	-4.043541
4.020724	2713	18770931	11.035405	1.962167	-4.043651
4.020725	2713	18770931	11.035406	1.962180	-4.043761
4.020726	2713	18770931	11.035407	1.962193	-4.043871
4.020727	2713	18770931	11.035408	1.962206	-4.043981
4.020728	2713	18770931	11.035409	1.962219	-4.044091
4.020729	2713	18770931	11.035410	1.962232	-4.044201
4.020730	2713	18770931	11.035411	1.962245	-4.044311
4.020731	2713	18770931	11.035412	1.962258	-4.044421
4.020732	2713	18770931	11.035413	1.962271	-4.044531
4.020733	2713	18770931	11.035414	1.962284	-4.044641
4.020734	2713	18770931	11.035415	1.962297	-4.044751
4.020735	2713	18770931	11.035416	1.962310	-4.044861
4.020736	2713	18770931	11.035417	1.962323	-4.044971
4.020737	2713	18770931	11.035418	1.962336	-4.045081
4.020738	2713	18770931	11.035419	1.962349	-4.045191
4.020739	2713	18770931	11.035420	1.962362	-4.045301
4.020740	2713	18770931	11.035421	1.962375	-4.045411
4.020741	2713	18770931	11.035422	1.962388	-4.045521
4.020742	2713	18770931	11.035423	1.962401	-4.045631
4.020743	2713	18770931	11.035424	1.962414	-4.045741
4.020744	2713	18770931	11.035425	1.962427	-4.045851
4.020745	2713	18770931	11.035426	1.962440	-4.045961
4.020746	2713	18770931	11.035427	1.962453	-4.046071
4.020747	2713	18770931	11.035428	1.962466	-4.046181
4.020748	2713	18770931	11.035429	1.962479	-4.046291
4.020749	2713	18770931	11.035430	1.962492	-4.046401
4.020750	2713	18770931	11.035431	1.962505	-4.046511
4.020751	2713	18770931	11.035432	1.962518	-4.046621
4.020752	2713	18770931	11.035433	1.962531	-4.046731
4.020753	2713	18770931	11.035434	1.962544	-4.046841
4.020754	2713	18770931	11.035435	1.962557	-4.046951
4.020755	2713	18770931	11.035436	1.962570	-4.047061
4.020756	2713	18770931	11.035437	1.962583	-4.047171
4.020757	2713	18770931	11.035438	1.962596	-4.047281
4.020758	2713	18770931	11.035439	1.962609	-4.047391
4.020759	2713	18770931	11.035440	1.962622	-4.047501
4.020760	2713	18770931	11.035441	1.962635	-4.047611
4.020761	2713	18770931	11.035442	1.962648	-4.047721
4.020762	2713	18770931	11.035443	1.962661	-4.047831
4.020763	2713	18770931	11.035444	1.962674	-4.047941
4.020764	2713	18770931	11.035445	1.962687	-4.048051
4.020765	2713	18770931	11.035446	1.962700	-4.048161
4.020766	2713	18770931	11.035447	1.962713	-4.048271
4.020767	2713	18770931	11.035448	1.962726	-4.048381
4.020768	2713	18770931	11.035449	1.962739	-4.048491
4.020769	2713	18770931	11.035450	1.962752	-4.048601
4.020770	2713	18770931	11.035451	1.962765	-4.048711
4.020771	2713	18770931	11.035452	1.962778	-4.048821
4.020772	2713	18770931	11.035453	1.962791	-4.048931
4.020773	2713	18770931	11.035454	1.962804	-4.049041
4.020774	2713	18770931	11.035455	1.962817	-4.049151
4.020775	2713	18770931	11.035456	1.962830	-4.049261
4.020776	2713	18770931	11.035457	1.962843	-4.049371
4.020777	2713	18770931	11.035458	1.962856	-4.049481
4.020778	2713	18770931	11.035459	1.962869	-4.049591
4.020779	2713	18770931	11.035460	1.962882	-4.049701
4.020780	2713	18770931	11.035461	1.962895	-4.049811
4.020781	2713	18770931	11.035462	1.962908	-4.049921
4.020782	2713	18770931	11.035463	1.962921	-4.050031
4.020783	2713	18770931	11.035464	1.962934	-4.050141
4.020784	2713	18770931	11.035465	1.962947	-4.050251
4.020785	2713	18770931	11.035466	1.962960	-4.050361
4.020786	2713	18770931	11.035467	1.962973	-4.050471
4.020787	2713	18770931	11.035468	1.962986	-4.050581
4.020788	2713	18770931	11.035469	1.962999	-4.050691
4.020789	2713	18770931	11.035470	1.963012	-4.050801
4.020790	2713	18770931	11.035471	1.963025	-4.050911
4.020791	2713	18770931	11.035472	1.963038	-4.051021
4.020792	2713	18770931	11.035473	1.963051	-4.051131
4.020793	2713	18770931	11.035474	1.963064	-4.051241
4.020794	2713	18770931	11.035475	1.963077	-4.051351
4.020795	2713	18770931	11.035476	1.963090</	







1	0.25	2993.	4,777,999	10491.	44275293.
2	0.25	2993.	15,462,799	10491.	44255109.
3	0.25	2993.	21,147,599	10491.	43771293.
4	0.44	2912.	10,747,599	10721.	22201279.
5	0.44	2912.	10,746,759	10721.	22222471.
6	0.44	2912.	10,746,759	10721.	22200469.

Layering correction equivalent widths of soil layers (mm)

Layer No.	Top of Layer (mm)	Bottom of Layer (mm)	Soil Profile	Soil Type	Layer Thickness (mm)	Layer Correction Factor	Layer Correction Multiplier	Layer Correction Value
1	0.000	0.00	101	10	0.00	0.00	0.00	0.00
2	0.000	1.0742	101	10	1.0742	0.00	0.00	0.00
3	0.000	2.1483	101	10	2.1483	0.00	0.00	0.00
4	0.000	3.2224	101	10	3.2224	0.00	0.00	0.00
5	0.000	4.2965	101	10	4.2965	0.00	0.00	0.00
6	0.000	5.3706	101	10	5.3706	0.00	0.00	0.00
7	0.000	6.4447	101	10	6.4447	0.00	0.00	0.00
8	0.000	7.5188	101	10	7.5188	0.00	0.00	0.00
9	0.000	8.5929	101	10	8.5929	0.00	0.00	0.00
10	0.000	9.6670	101	10	9.6670	0.00	0.00	0.00
11	0.000	10.7411	101	10	10.7411	0.00	0.00	0.00
12	0.000	11.8152	101	10	11.8152	0.00	0.00	0.00
13	0.000	12.8893	101	10	12.8893	0.00	0.00	0.00
14	0.000	13.9634	101	10	13.9634	0.00	0.00	0.00
15	0.000	15.0375	101	10	15.0375	0.00	0.00	0.00

Note: The  $\int_{z_1}^{z_2} \gamma dz$  integral of layer  $n$  equals the sum of the  $\int_{z_1}^{z_2} \gamma dz$  integrals for layer  $n$ . Layering correction equivalent widths are computed only for soil layers with both shear modulus and shear capacity parameters for peak lateral load transfer. These soil types are soil and stiff clay, rock/landfill sand, and concrete (soil only).

Computed values of pile loading and deflection for lateral loading for load case (Table 1)

Pile-head conditions are fixed and hammer loading (Type 1)

Depth (m)	Soil Stiffness (kN/m³)	Soil Capacity (kN/m²)	Soil Modulus (kPa)	Soil Capacity (kN/m²)	Soil Modulus (kPa)	Soil Capacity (kN/m²)	Soil Modulus (kPa)	Soil Capacity (kN/m²)	Soil Modulus (kPa)
0.00	2.00	2.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	4.00	4.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	6.00	6.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	8.00	8.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	10.00	10.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	12.00	12.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	14.00	14.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	16.00	16.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	18.00	18.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	20.00	20.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	22.00	22.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	24.00	24.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	26.00	26.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	28.00	28.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	30.00	30.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	32.00	32.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	34.00	34.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	36.00	36.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	38.00	38.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	40.00	40.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	42.00	42.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	44.00	44.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	46.00	46.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	48.00	48.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	50.00	50.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	52.00	52.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	54.00	54.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	56.00	56.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	58.00	58.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	60.00	60.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	62.00	62.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	64.00	64.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	66.00	66.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	68.00	68.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	70.00	70.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	72.00	72.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	74.00	74.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	76.00	76.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	78.00	78.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	80.00	80.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	82.00	82.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	84.00	84.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	86.00	86.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	88.00	88.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	90.00	90.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	92.00	92.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	94.00	94.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	96.00	96.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	98.00	98.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		
0.00	100.00	100.000	1.00E+07	20100	-0.0010	0.00	1.00E+11		



17,116	-1,047.0	132,044	-13,764	-1,705.00	2.00	4,330.12
20,149	1,844	4.00				
27,000	-1,200.0	1,100.75	-1,170	-1,520.00	2.00	4,330.12
30,107	1,844	4.00				
37,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
40,107	1,844	4.00				
47,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
50,107	1,844	4.00				
57,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
60,107	1,844	4.00				
67,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
70,107	1,844	4.00				
77,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
80,107	1,844	4.00				
87,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
90,107	1,844	4.00				
97,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
100,107	1,844	4.00				
107,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
110,107	1,844	4.00				
117,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
120,107	1,844	4.00				
127,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
130,107	1,844	4.00				
137,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
140,107	1,844	4.00				
147,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
150,107	1,844	4.00				
157,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
160,107	1,844	4.00				
167,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
170,107	1,844	4.00				
177,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
180,107	1,844	4.00				
187,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
190,107	1,844	4.00				
197,000	-1,200.0	1,100.50	-1,170	-1,520.00	2.00	4,330.12
200,107	1,844	4.00				

17,116	-1,047.0	132,044	-13,764	-1,705.00	0.00	1,122,942
20,149	1,844	4.00				
27,000	-1,200.0	1,100.75	-1,170	-1,520.00	0.00	1,122,942
30,107	1,844	4.00				
37,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
40,107	1,844	4.00				
47,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
50,107	1,844	4.00				
57,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
60,107	1,844	4.00				
67,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
70,107	1,844	4.00				
77,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
80,107	1,844	4.00				
87,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
90,107	1,844	4.00				
97,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
100,107	1,844	4.00				
107,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
110,107	1,844	4.00				
117,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
120,107	1,844	4.00				
127,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
130,107	1,844	4.00				
137,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
140,107	1,844	4.00				
147,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
150,107	1,844	4.00				
157,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
160,107	1,844	4.00				
167,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
170,107	1,844	4.00				
177,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
180,107	1,844	4.00				
187,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
190,107	1,844	4.00				
197,000	-1,200.0	1,100.50	-1,170	-1,520.00	0.00	1,122,942
200,107	1,844	4.00				

\* This analysis assumed all residential property would be sold at the same time. Monthly values of total residential property owned and existing in years are computed with the following assumptions: (1) only one unit per lot; (2) only existing residential stock; (3) no new residential stock; (4) no new units built; (5) the replacement cost of existing residential stock is the replacement cost of new stock developed by the city.

Major summary for use case No. 1:

Present residential	=	4,460,942 units
Proposed replacement	=	4,330,142 units
Net residential units	=	130,800 units
Net residential units	=	11,750 units
Present residential units	=	2,450,000 units (with units)
Proposed residential units	=	2,450,000 units (with units)
Net residential units	=	0
Net residential units	=	0

Net residential units for use case No. 1:

Present residential units	=	4,460,942 units
Proposed replacement units	=	4,330,142 units
Net residential units	=	130,800 units

Age	Age	Age	Age	Age	Age	Age
1	2	3	4	5	6	7









75.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
76.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
77.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
78.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
79.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
80.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
81.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
82.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
83.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
84.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
85.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
86.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
87.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
88.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
89.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
90.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
91.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
92.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
93.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
94.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
95.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
96.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
97.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
98.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
99.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12
100.0000	2.00000	200000	-4000	-4.00E+02	0.75	4.10E+12

This analysis computed pile response using nonlinear earth resistance only. Existing values of total stress due to soil weight and existing porewater are computed only to provide facilities as input to the code. The actual stresses in concrete and steel, as well as associated steel cap to be transferred from the cap to the pile, are not included in the output of loading server developed in this site.

**Output Summary for Load Case No. 1:**

Pile head deflection	4.10E+12
Computed slope at pile head	4.10E+12
Soil reaction bending moment	4.10E+12
Soil reaction shear force	4.10E+12
Head of reaction bending moment	4.10E+12
Head of reaction shear force	4.10E+12
Index of iteration	1
Index of soil resistance points	1

**Summary of Pile Head Response for Selected Load Cases**

**Table A.1: Summary of Pile Head Loading Conditions**

Load Case 1: Load 1 = Dead, 2 = Live, and Load 3 = Wind, 4 = Seismic  
 Load Case 2: Load 1 = Dead, 2 = Live, and Load 3 = Wind, 4 = Seismic  
 Load Case 3: Load 1 = Dead, 2 = Live, and Load 3 = Wind, 4 = Seismic  
 Load Case 4: Load 1 = Pile Reflection, 2 = Soil, and Load 3 = Wind, 4 = Seismic  
 Load Case 5: Load 1 = Pile Reflection, 2 = Soil, and Load 3 = Wind, 4 = Seismic

Load Case	Source	Load Type	Pile Head	Value	Unit	Reference
1	Dead	1	1	1.00E+02	lb	ASCE 7-05
2	Live	2	2	1.00E+02	lb	ASCE 7-05
3	Wind	3	3	1.00E+02	lb	ASCE 7-05
4	Seismic	4	4	1.00E+02	lb	ASCE 7-05

Two-way ANOVA statistics: 1. 11/20/2011 11:09 AM  
 Two-way ANOVA statistics: 2. 11/20/2011 11:09 AM

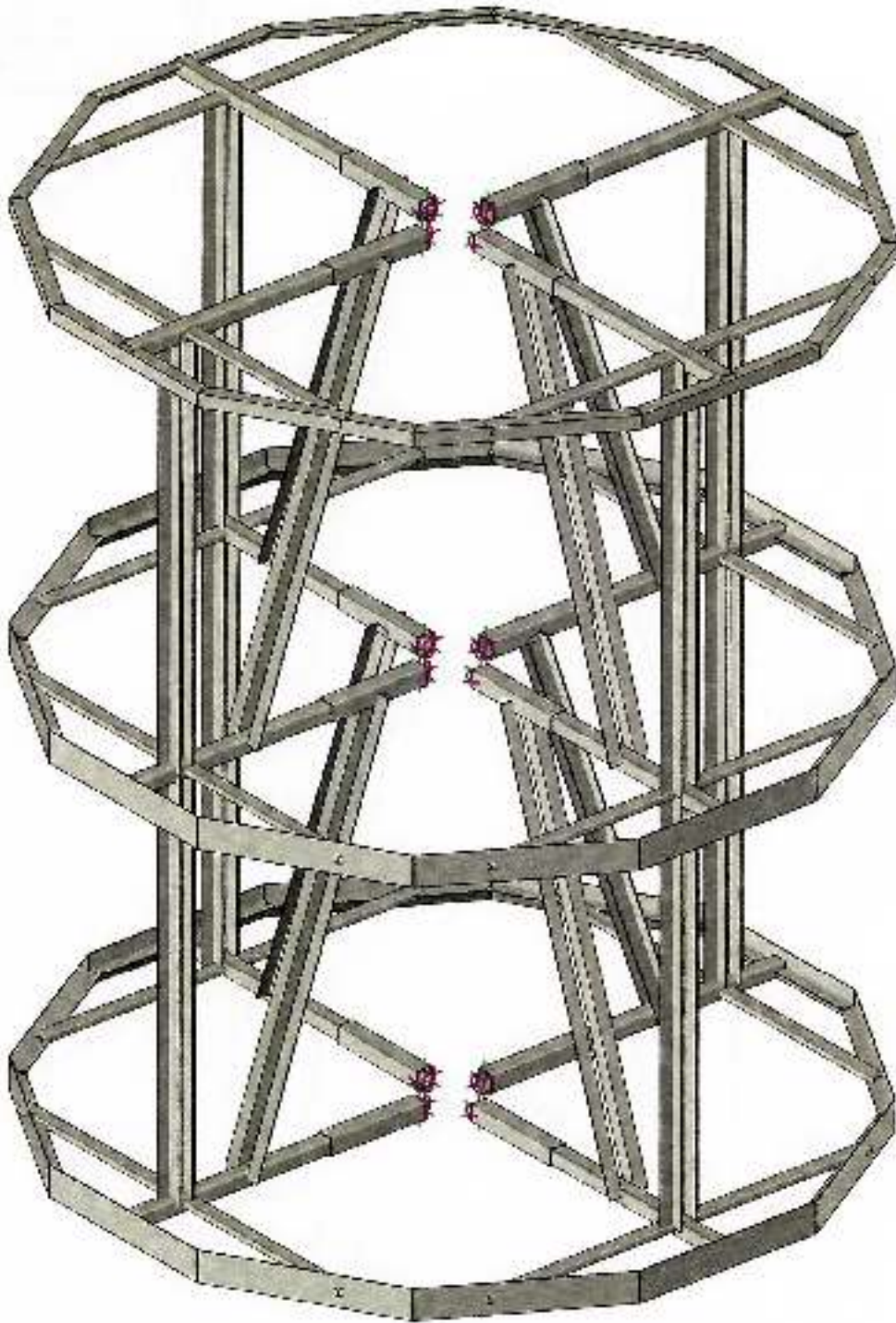
Summary of Hunting Package

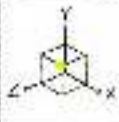
The following summary was generated for the

11/20/2011 11:09 AM

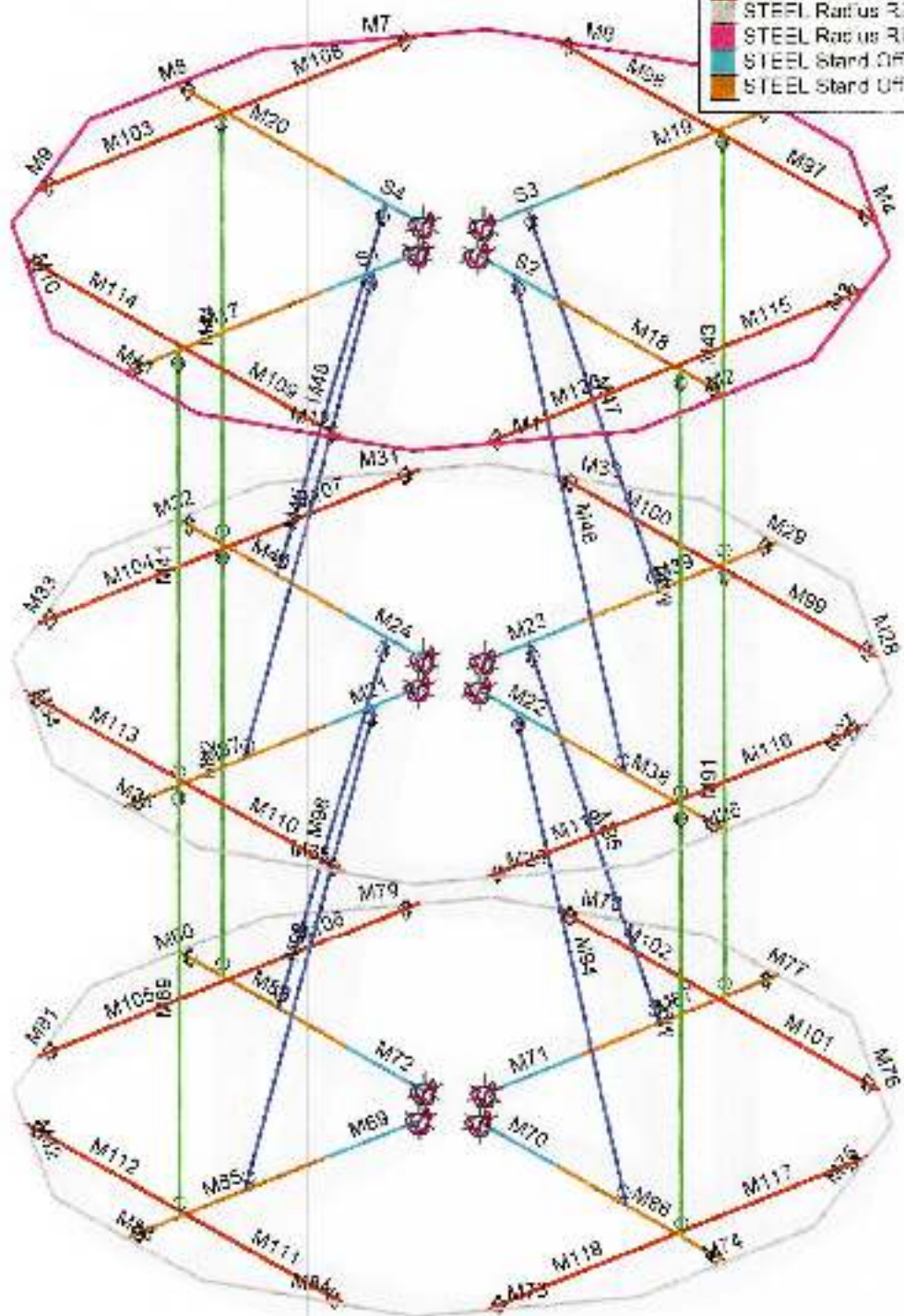
is from values for detector angle to either smaller than 20 degrees or higher than 70 degrees and no value of 0 has been specified for a null level defined using the same criteria. Program will assume an interval of 10 units for 0, but the detector angle is not 0 for every 10 units. Please check your input data for correctness.

The analysis order normally





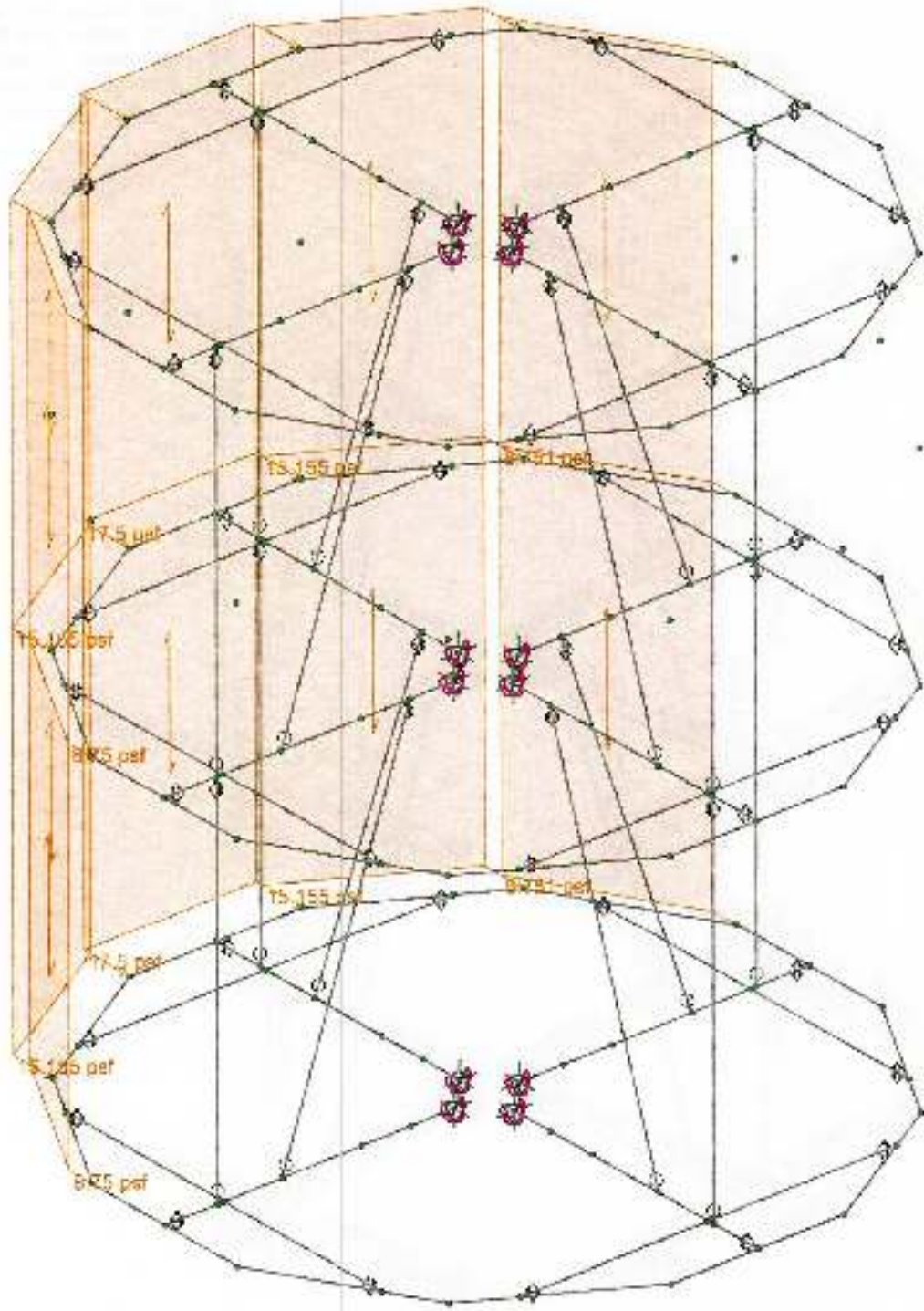
- Section Sets
- FRP Kicker Brace
  - FRP Vertical Brace
  - STEEL Outrigger Weldment
  - STEEL Radius Ring Assembly
  - STEEL Radius Ring Assembly Top
  - STEEL Stand Off Arm
  - STEEL Stand Off Arm Inner



Vector SF

SK-2  
Oct. 24, 2024 at 10:53 AM  
NM1-148 Spke Concealmen

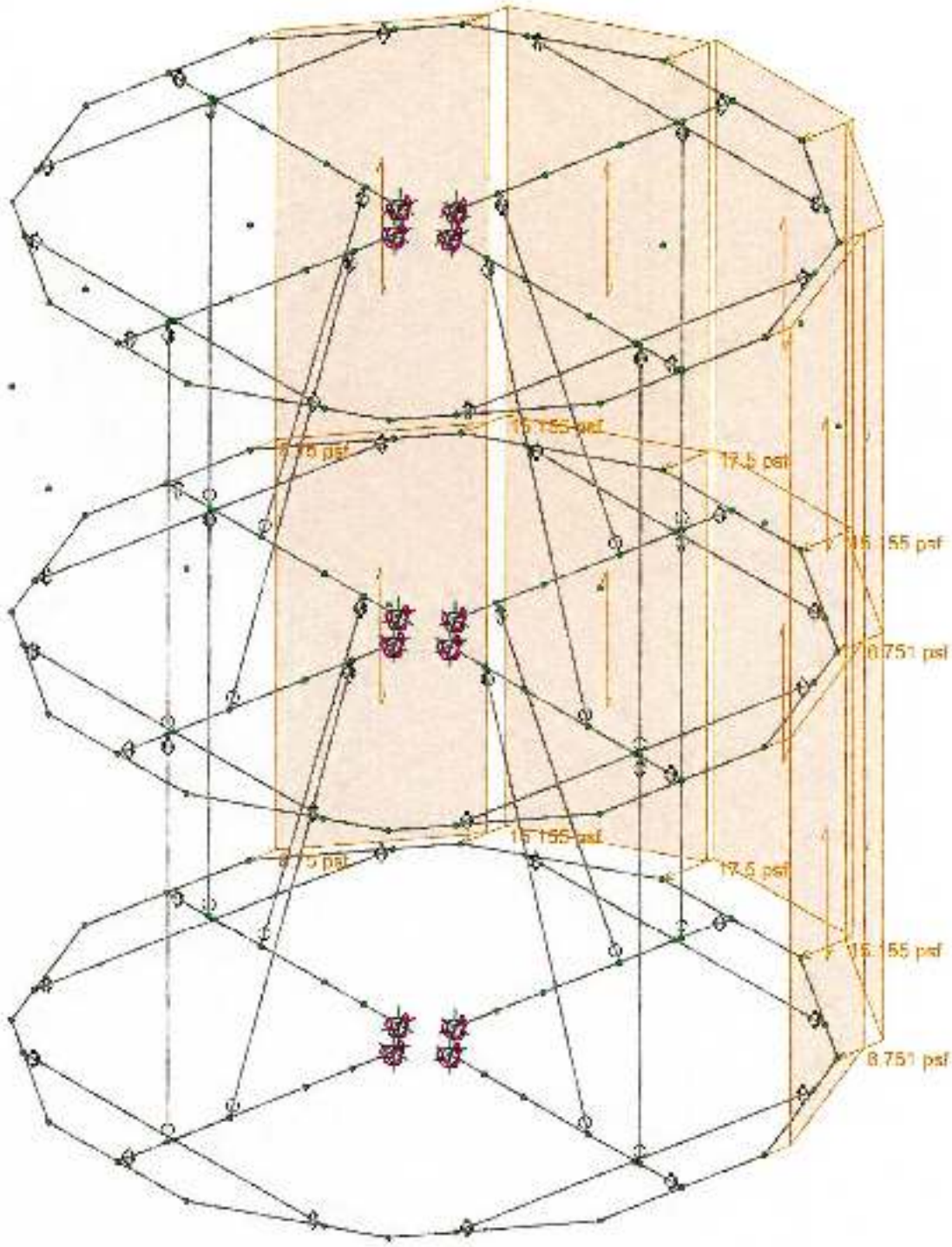
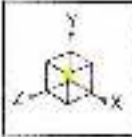




1 nets: H, C, O, N, X

	Vector SF

SK 4
Ort 24, 2024 at 10:53 AM
NMI: 146 Spko Corosalmen...



Loads: BLC 3, WLZ

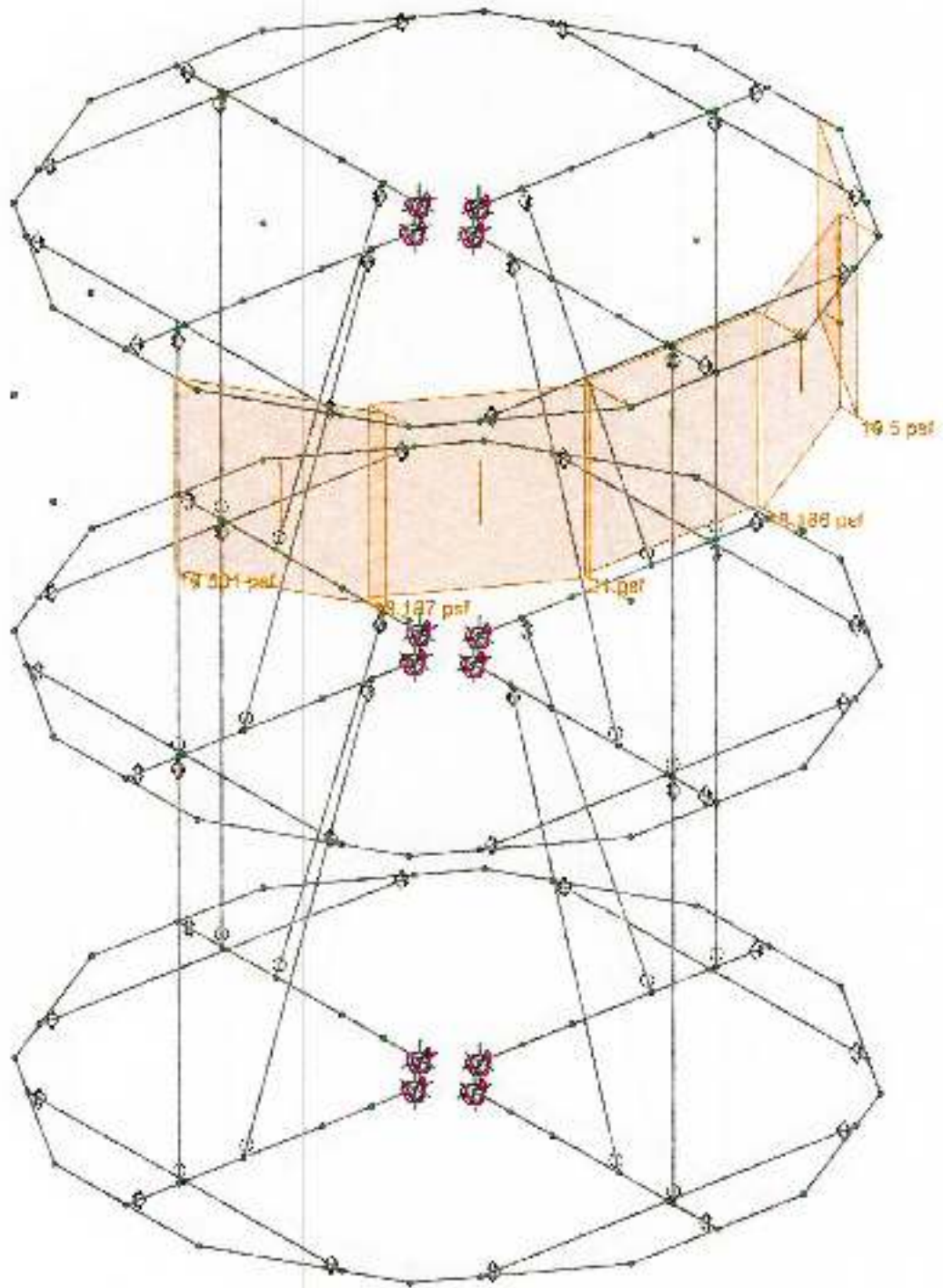


Vector SE

SK-5

Oct 24, 2024 at 10:53 AM

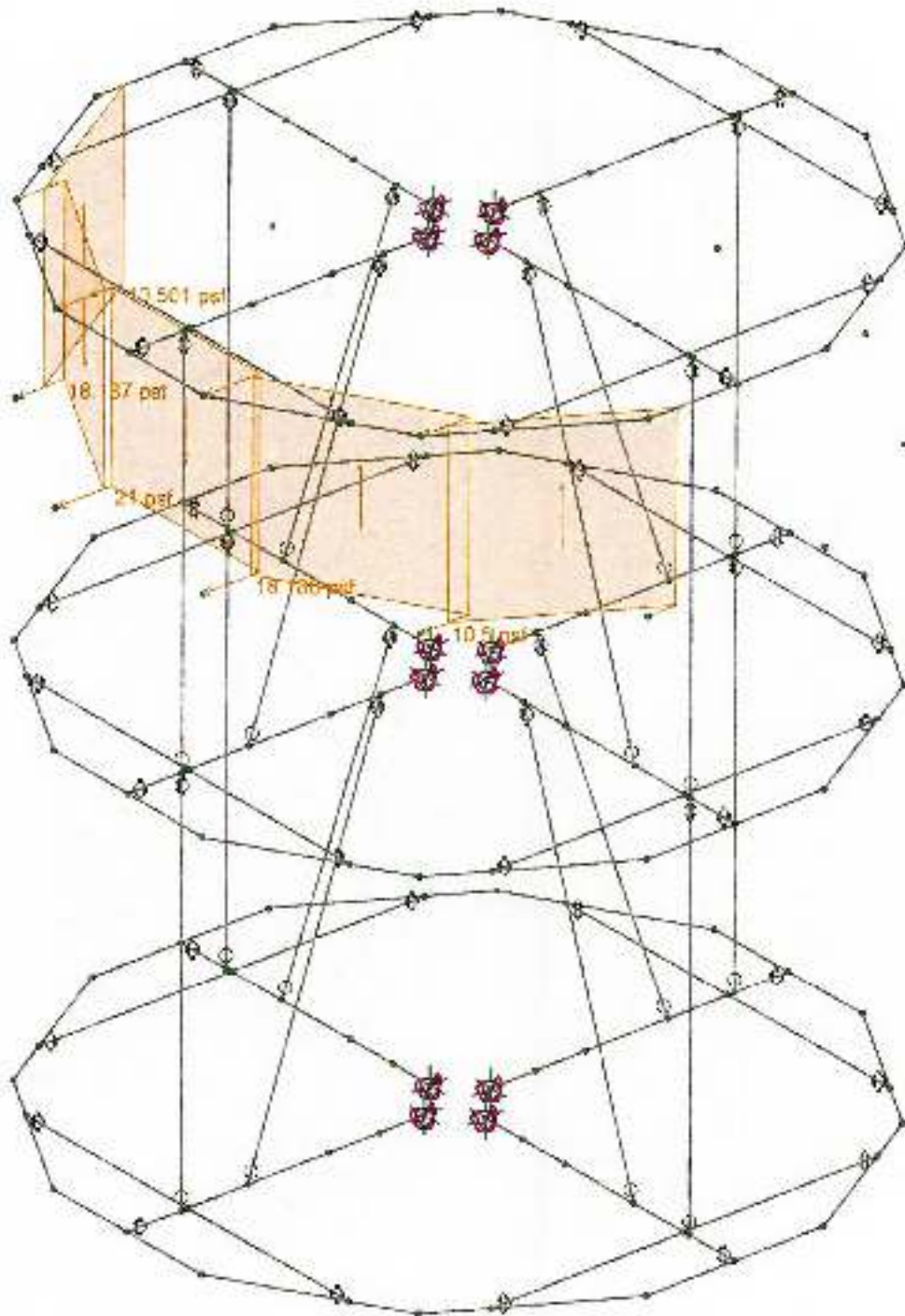
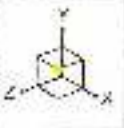
NM1-148 Spike Concreme1...



Loads: BLC 4 - W\_X Inside

	Vector SE

SK 6
Oct 24 2024 at 10:54 AM
NM1-148 Spike Concealmer...



Loads: RI C 5, WI Z Ins de

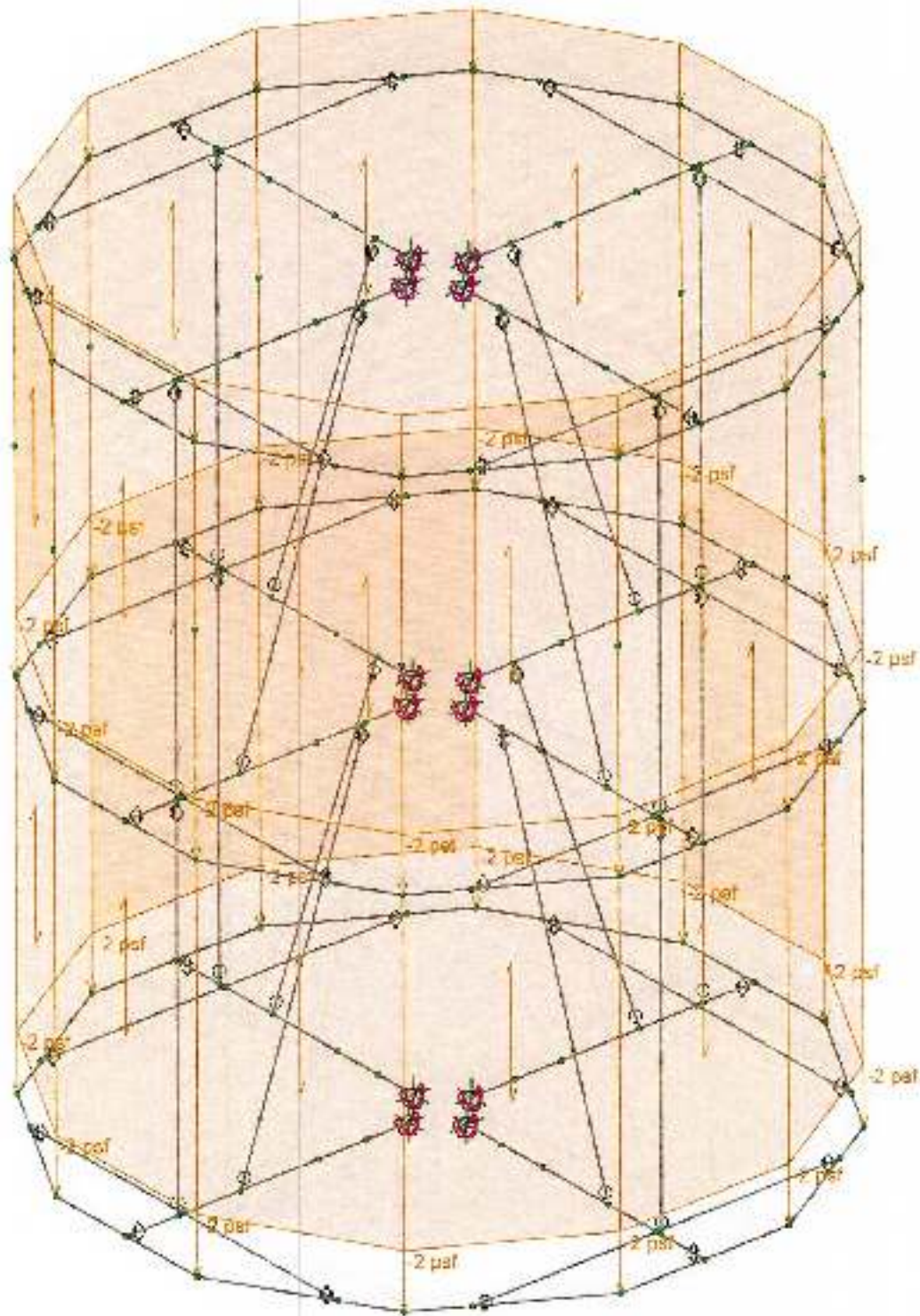


Vector SF

SK-7

Oct 24, 2024 at 10:54 AM

NM1-14d Spike Concealmen...



Loads: BLC 8, Panels

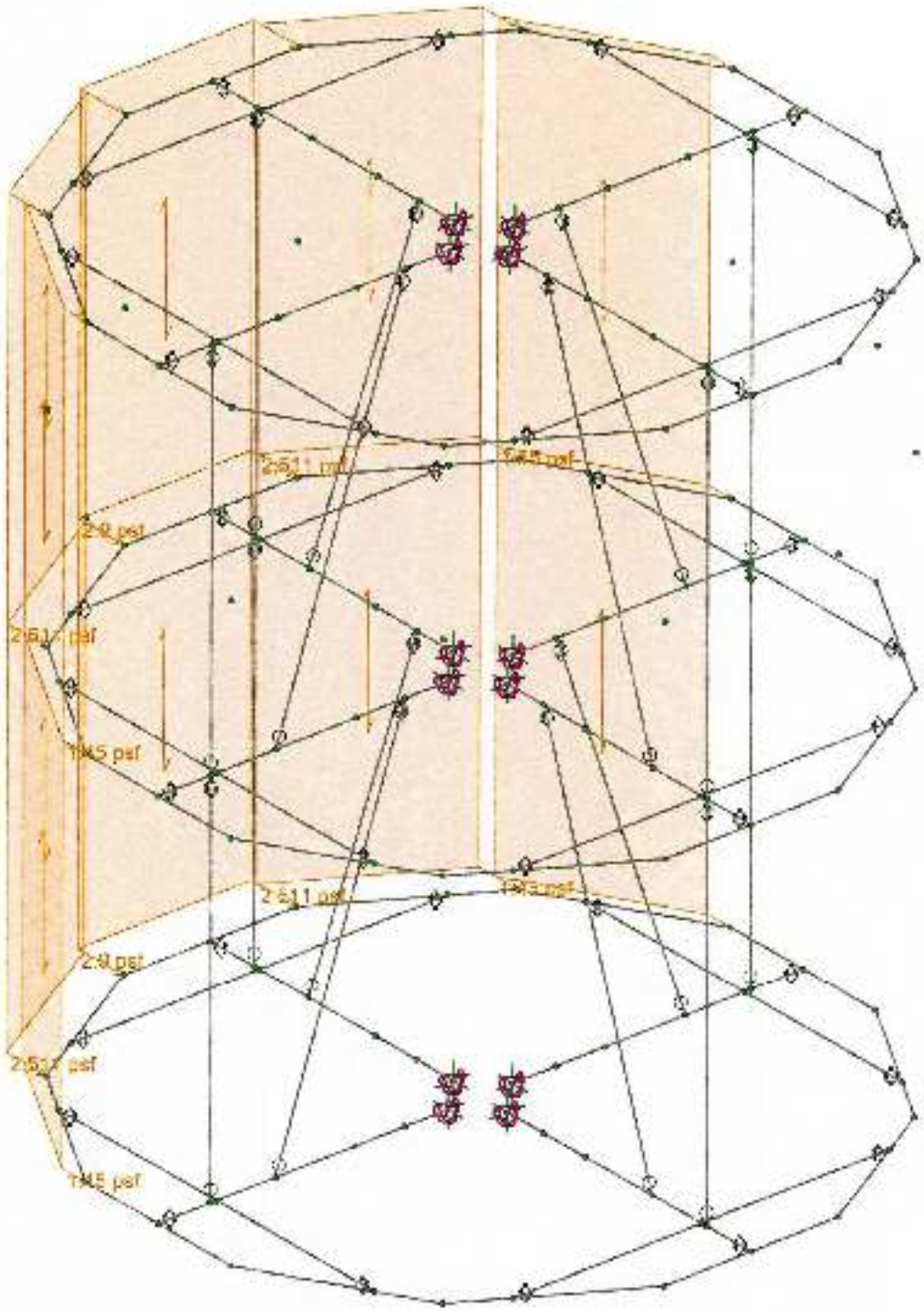
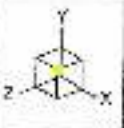


Vector SE

SK-8

Oct 24, 2024 at 10:54 AM

NM1-145 Soke Coroaalmen...



Load: DLC 8 W: X km

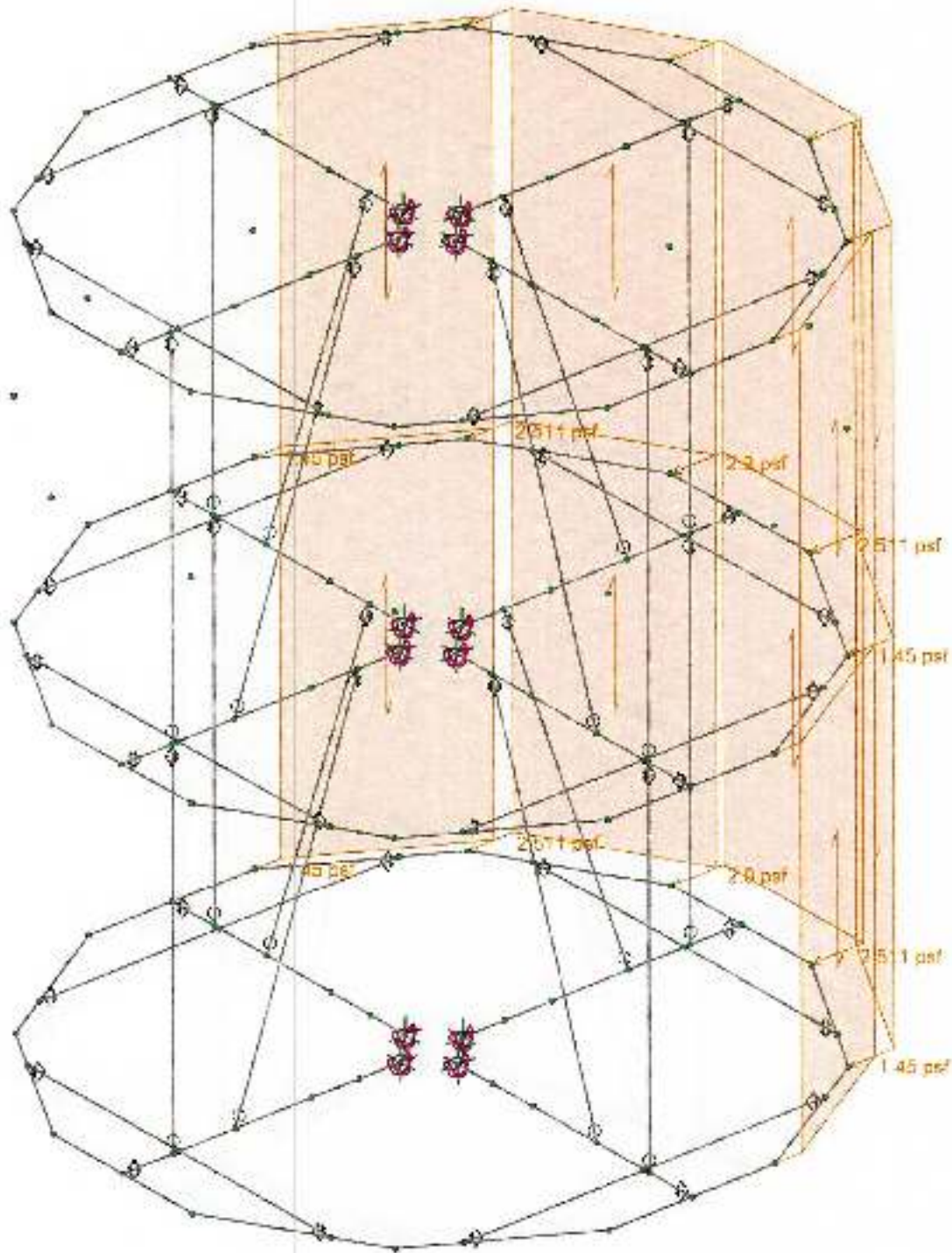


Vector BE

SK-9

Oct 24, 2024 at 10:54 AM

NM-145 Spoke Corralmen

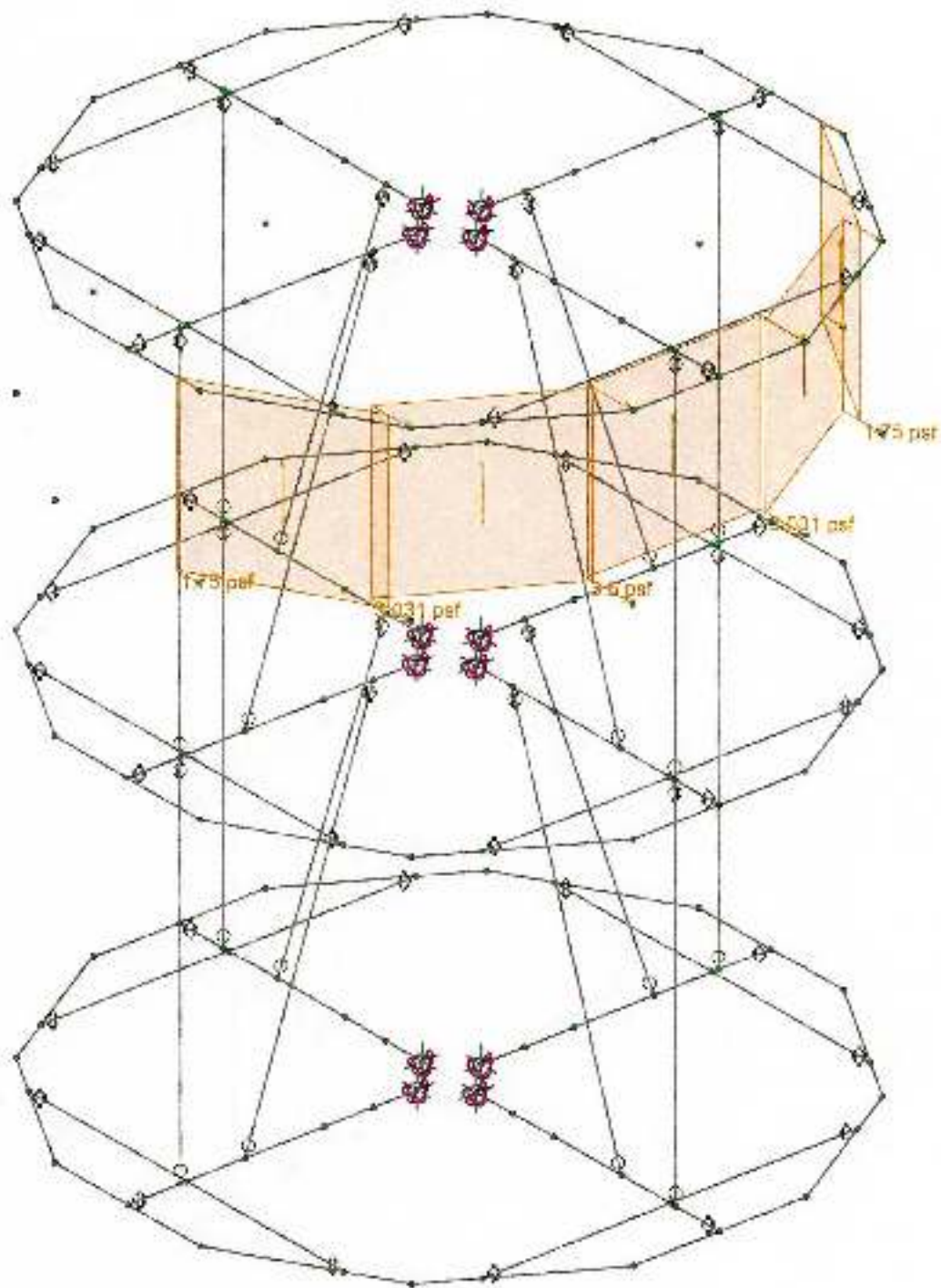
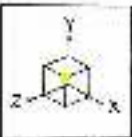


Loads: PL: 0, WL: 7 lbf



Vector SE

SK-10  
Oct 24, 2024 at 10:51 AM  
NV1-145 Soke Concealmen..



Loads: BLC 10, WLX Ice Inside

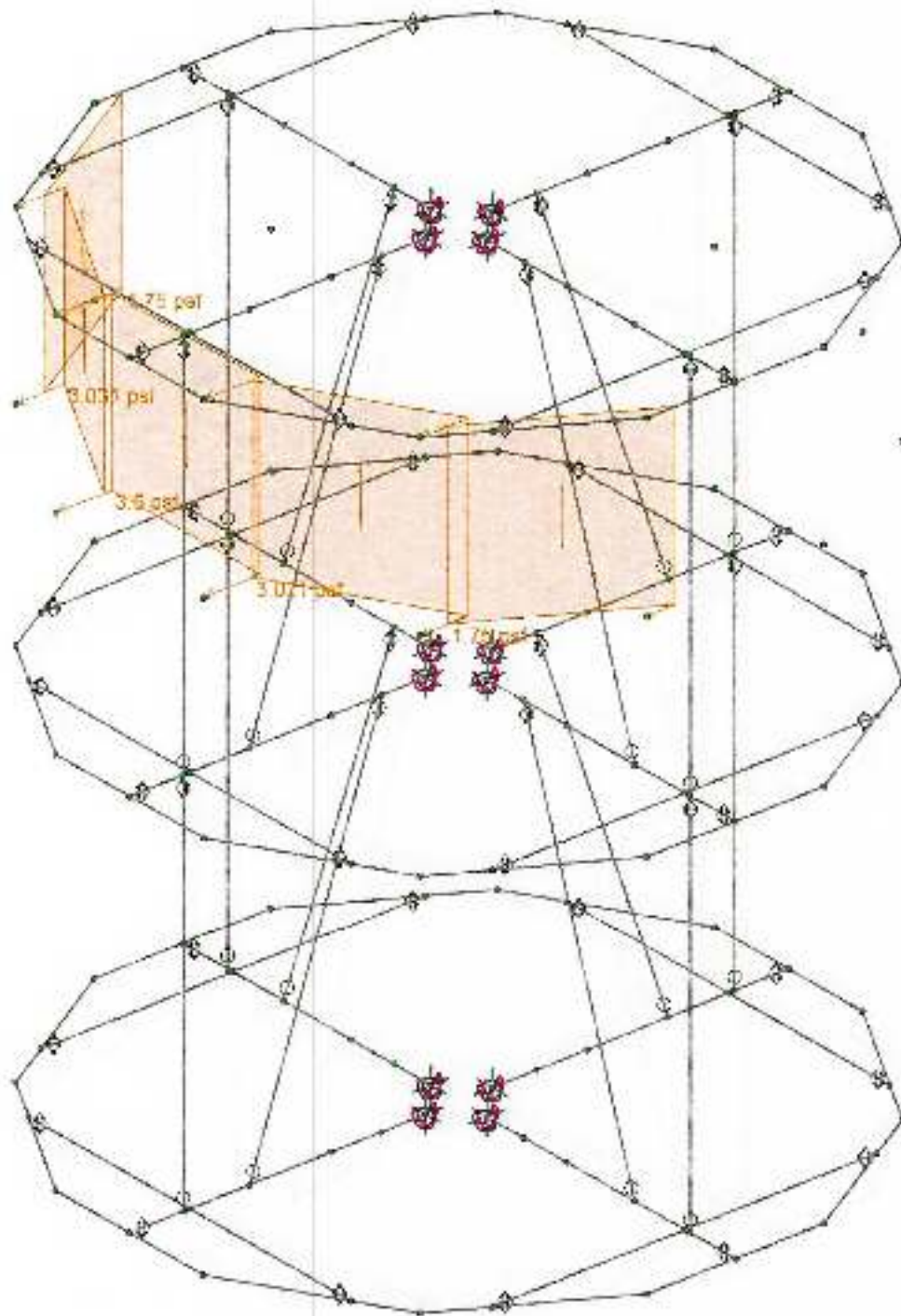
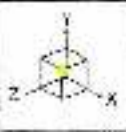


Vector SE

SK-11

Oct 24, 2024 at 10:54 AM

NM1-148 Spike Concealmen...



Loads: BLC 11, WLZ Ice Inside

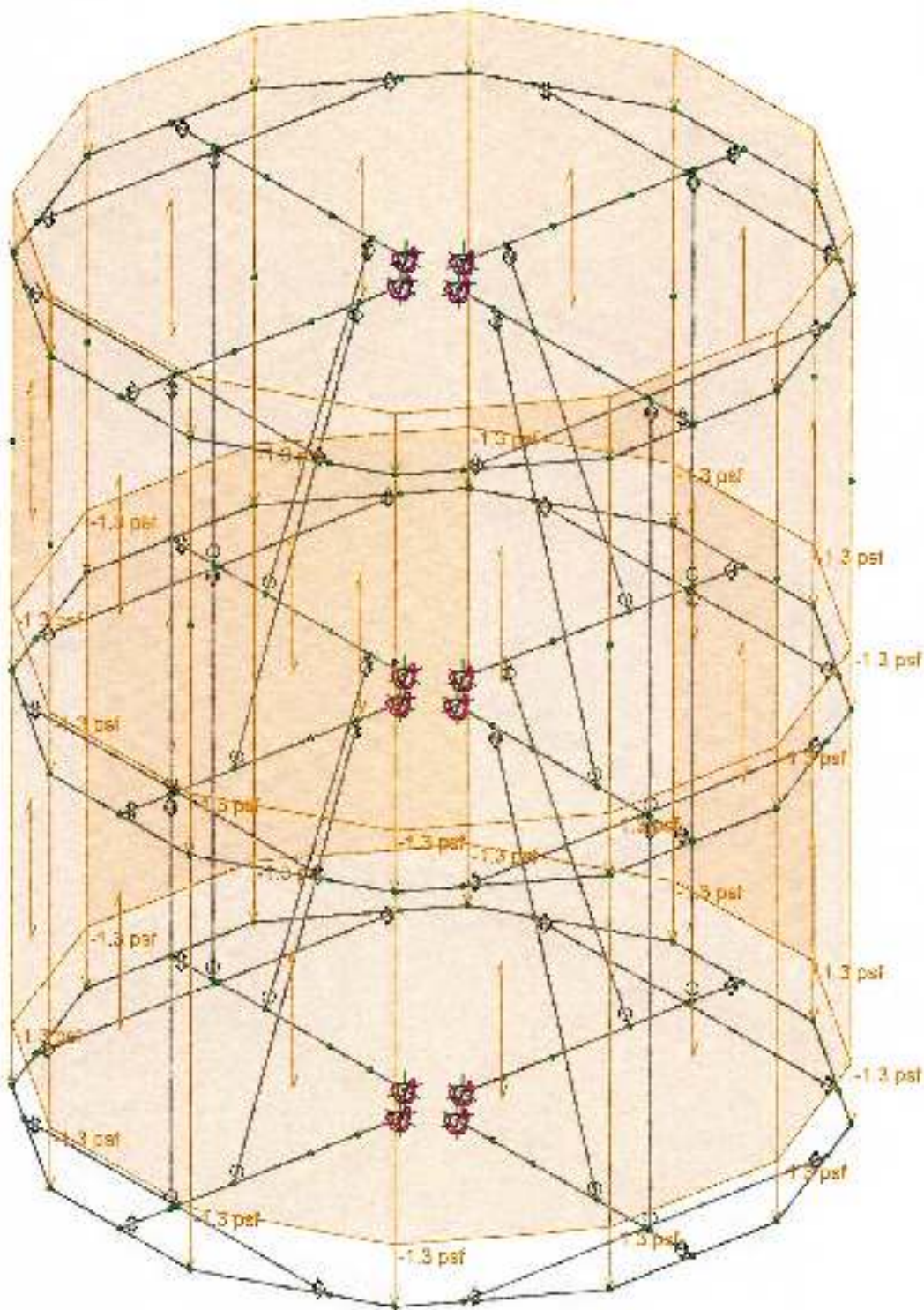
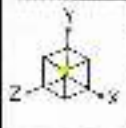


Vector SE

SK-12

Oct 24, 2021 at 10:51 AM

NM1-148 Spike Concessmen...



Loads: BLC 12, los Weight

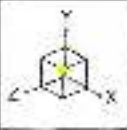


Vector SE

SK-13

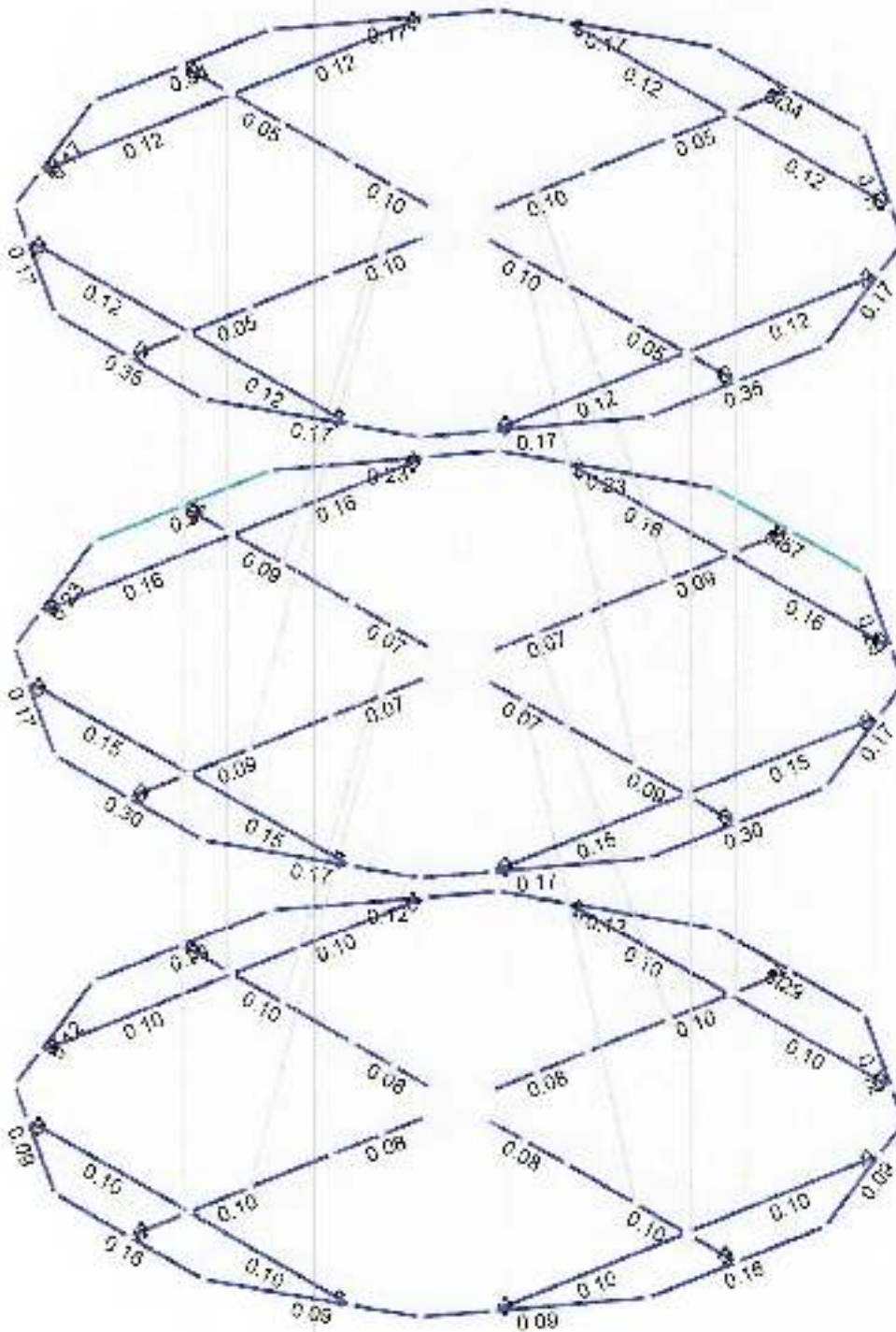
Oct 24, 2024 at 10:54 AM

NM1-148 Spike Concealment...



Code Check (Frv)

- No Calc
- > 1.0
- 90-1.0
- 75-90
- 50-75
- 0-.50



Member Code Checks Displayed (Envelope 1)

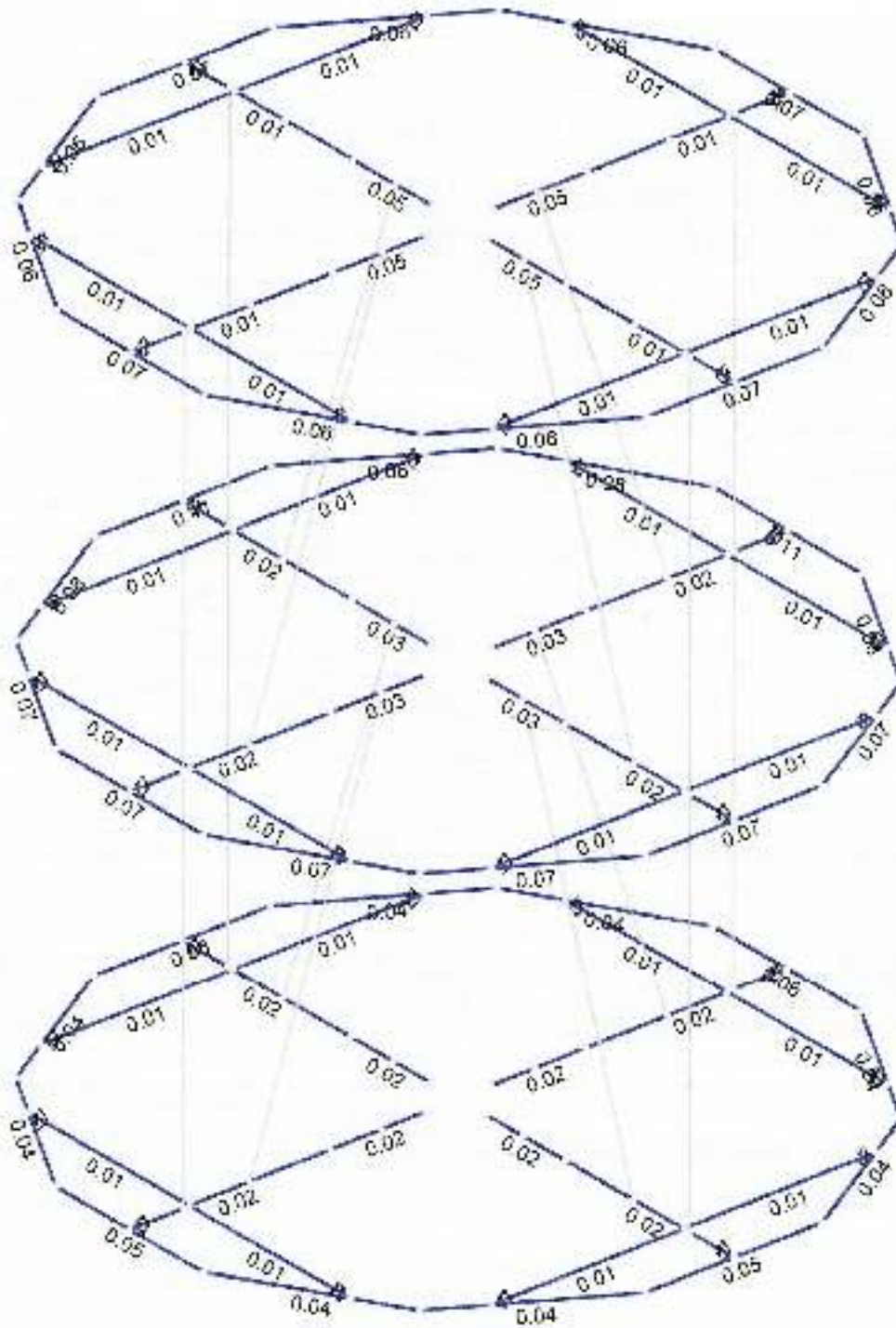
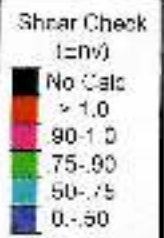
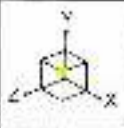


Vector SE

SK-14

Oct 24, 2024 at 10:54 AM

NM1-148 Spike Curves in en ..



Member Shear Checks Displayed (Enveloped)



Vector SE

SK-15

Oct. 24, 2024 at 10:55 AM

NM: 148 Spike Concealmen



Company : Vector SE  
 Designer :  
 Job Number :  
 Model Name :

8/1/2024  
 10/24/2024  
 10:55:17 AM  
 Checked By \_\_\_\_\_

**Model Settings**

Number of Reported Sections	5
Number of Internal Sections	100
Member Area Load Mesh Size (in <sup>2</sup> )	144
Consider Shear Deformation	Yes
Consider Torsional Warping	Yes
Approximate Mesh Size (in)	24
Transfer Forces Between Intersecting Wood Walls	Yes
Increase Wood Wall Nailing Capacity for Wind Loads	Yes
Include P-Delta for Walls	Yes
Optimize Masonry and Wood Walls	Yes
Maximum Number of Iterations	3
Single	No
Multiple (Optimum)	No
Maximum	Yes

Global Axis corresponding to vertical direction	Y
Convert Existing Data	Yes
Default Global Plane for z-axis	XZ
Plate Local Axis Orientation	Global

Hot Rolled Steel	AISC 15th (360-16) LRFD
Stiffness Adjustment	Yes (iterative)
National Annex	None
Connections	None
Cold Formed Steel	None
Stiffness Adjustment	Yes (iterative)
Wood	None
Temperature	< 100F
Concrete	None
Masonry	None
Aluminum	None
Structure Type	Building
Stiffness Adjustment	Yes (iterative)
Stainless	None
Stiffness Adjustment	Yes (iterative)

Compression Stress Block	Rectangular Stress Block
Analyze using Cracked Sections	Yes
Leave room for horizontal rebar splices (2"d bar spacing)	No
List forces which were ignored for design in the Detail Report	Yes

Column Min Steel	1
Column Max Steel	6
Rebar Material Spec	ASTM A615
Warn if beam-column framing arrangement is not understood	No
Number of Shear Regions	4
Region 2 & 3 Spacing Increase Increment (in)	4

Code	ASCE 7-16
Risk Category	I or II
Drift Cat	Other

**Hot Rolled Steel Properties**

	Label	E [ksi]	G [ksi]	Nt	Ham. Coeff [1n°F]	Density [kcf]	Yield [ksi]	Ry	Fu [ksi]	Rt
1	A36 Gr.36	29000	11154	0.3	0.65	0.49	36	58	58	1.2
2	A500 Gr.B RECT	29000	11154	0.3	0.65	0.527	45	54	54	1.3
3	A500 Gr.B RND	29000	11154	0.3	0.65	0.527	42	54	54	1.3
4	FRP	2800	450	0.3	0.65	0.11	10	12	30	1.1

**Hot Rolled Steel Section Sets**

	Label	Shape	Type	Design List	Material	Design Rule	Area [in²]	Iy [in⁴]	Izz [in⁴]	J [in⁶]
1	FRP Kicker Brace	11.4X4X6W4"CAP	MBrace	None	FRP	Typical	5.719	65.042	8.717	0.251
2	FRP Vertics. Brace	11.4X4X6W4"CAP	MBrace	None	FRP	Typical	5.719	65.042	8.717	0.251
3	STEEL Outrigger Weldment	HSS4X2X3	Beam	None	A500 Gr.B RECT	Typical	1.89	1.22	3.66	3.08
4	STEEL Radius Ring Assembly	9X4X3/16"	Beam	None	A36 Gr.36	Typical	2.409	11.423	2.887	0.070
5	STEEL Radius Ring Assembly Top	1.4X4X4	Beam	None	A36 Gr.36	Typical	1.93	3	3	0.044
6	STEEL Stand Off Arm	HSS5X5X3	Beam	None	A500 Gr.B REC	Typical	3.28	12.6	12.6	19.9
7	STEEL Stand Off Arm Liner	HSS4.5X4.5X5	Beam	None	A500 Gr.B RECT	Typical	5.48	15.3	15.3	25.7

**Load Combinations**

	Description	Solve	P-Delta	BLC	Factor	BLC	Factor	BLC	Factor
1	1.0D	Yes	Y	DL	1				
2	1.4D	Yes	Y	DL	1.4				
3	1.2D+1.6L	Yes	Y	DL	1.2	LL	1.6		
4	1.2D + 0.5LL + 1.0WLx	Yes	Y	DL	1.2	LL	0.5	WLX	1
5	1.2D + 0.5LL + 1.0WLz	Yes	Y	DL	1.2	LL	0.5	WLZ	1
6	1.2D + 0.5LL - 1.0WLx	Yes	Y	DL	1.2	LL	0.5	WLX	-1
7	1.2D + 0.5LL - 1.0WLz	Yes	Y	DL	1.2	LL	0.5	WLZ	-1
8	1.2D + 1.0WLx	Yes	Y	DL	1.2	WLX	1		
9	1.2D + 1.0WLz	Yes	Y	DL	1.2	WLZ	1		
10	1.2D - 1.0WLx	Yes	Y	DL	1.2	WLX	-1		
11	1.2D - 1.0WLz	Yes	Y	DL	1.2	WLZ	-1		
12	0.9D + 1.0WLx	Yes	Y	DL	0.9	WLX	1		
13	0.9D + 1.0WLz	Yes	Y	DL	0.9	WLZ	1		
14	0.9D - 1.0WLx	Yes	Y	DL	0.9	WLX	-1		
15	0.9D - 1.0WLz	Yes	Y	DL	0.9	WLZ	-1		
16	1.2D + 1.0Dx + 1.0Wix	Yes	Y	DL	1.2	OL1	1	OL2	1
17	1.2D + 1.0Dz + 1.0Wiz	Yes	Y	DL	1.2	OL1	1	OL3	1
18	1.2D + 1.0Dx - 1.0Wix	Yes	Y	DL	1.2	OL1	1	OL2	-1
19	1.2D + 1.0Dz - 1.0Wiz	Yes	Y	DL	1.2	OL1	1	OL3	-1

**Envelope Maximum Member Section Forces**

Member	Axial [lb]	Loc [ft]	Shear [lb]	Loc [ft]	LC Shear [lb]	Loc [ft]	LC Torque [lb-ft]	Loc [ft]	LCy-y Moment [lb-ft]	Loc [ft]	LCz-z Moment [lb-ft]	Loc [ft]
1 M98	max-1414.201	0	14	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
2	min-2362.771	10.5919	0	-11.722	10.5919	2	0	0	1	0	0	1
3 M94	max-1418.207	0	12	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
4	min-2361.772	10.5919	0	-11.722	10.5919	2	0	0	1	0	0	1
5 M93	max-1418.207	0	13	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
6	min-2361.772	10.5919	0	-11.722	10.5919	2	0	0	1	0	0	1
7 M95	max-1414.201	0	15	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
8	min-2362.771	10.5919	0	-11.722	10.5919	2	0	0	1	0	0	1
9 M49	max-1446.854	0	14	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
10	min-2394.567	10.5919	0	-11.722	10.5919	2	0	0	1	0	0	1
11 M47	max-1446.854	0	15	11.722	0	2	0	10.5919	0	10.5919	0	10.5919
12	min-2394.567	10.5919	0	-11.722	10.5919	2	0	0	1	0	0	1



**Envelope Maximum Member Section Forces (Continued)**

Member	Axial [lb]	Loc [']	Loc-y	Shear [lb]	Loc [']	Loc-z	Shear [lb]	Loc [']	Torque [lb-ft]	Loc [']	Loc-y	Moment [lb-ft]	Loc [']	Loc-z	Moment [lb-ft]	Loc [']
13 M46	max 1448.251	0	13	11.722	0	2	0	0	0.5913	0	0.5913	0	0	0	0	10.5819
14	min -2383.888	10.5913	-11.722	10.5913	2	0	0	0	1	0	0	1	0	0	1	10.5819
15 M45	max 1448.251	0	13	11.722	0	2	0	0	0.5913	0	0.5913	0	0	0	0	10.5819
16	min -2383.888	10.5913	-11.722	10.5913	2	0	0	0	1	0	0	1	0	0	1	10.5819
17 M89	max 905.661	0	13	0	10	19	0	10	19	0	10	19	0	10	19	0
18	min 501.605	10	13	0	0	1	0	0	1	0	0	1	0	0	1	0
19 M90	max 905.661	0	13	0	10	19	0	10	19	0	10	19	0	10	19	0
20	min 501.605	10	13	0	0	1	0	0	1	0	0	1	0	0	1	0
21 M81	max 906.079	0	17	0	10	19	0	10	19	0	10	19	0	10	19	0
22	min 499.864	10	15	0	0	1	0	0	1	0	0	1	0	0	1	0
23 M42	max 1083.508	0	18	0	10	19	0	10	19	0	10	19	0	10	19	0
24	min 640.67	10	12	0	0	1	0	0	1	0	0	1	0	0	1	0
25 M41	max 1083.508	0	18	0	10	19	0	10	19	0	10	19	0	10	19	0
26	min 640.67	10	12	0	0	1	0	0	1	0	0	1	0	0	1	0
27 M44	max 1083.507	0	16	0	10	19	0	10	19	0	10	19	0	10	19	0
28	min 640.956	10	14	0	0	1	0	0	1	0	0	1	0	0	1	0
29 M92	max 906.079	0	16	0	10	19	0	10	19	0	10	19	0	10	19	0
30	min 499.864	10	14	0	0	1	0	0	1	0	0	1	0	0	1	0
31 M43	max 1083.507	0	17	0	10	19	0	10	19	0	10	19	0	10	19	0
32	min 510.958	10	15	0	0	1	0	0	1	0	0	1	0	0	1	0
33 M31	max 1072.307	4.65810	406.526	1.50412	104.12	4.65818	19.793	1.45519	58.031	4.65819	492.438	4.61	10			
34	min -1053.54	4.65812	-407.959	1.50418	-46.96	1.50416	11.031	1.50413	-73.859	0	18	-186.197	4.61	12		
35 M77	max 471.748	4.65811	474.391	2.32911	130.859	2.32918	11.71	2.65917	267.953	2.32917	513.707	2.32913	19			
36	min -418.358	2.32915	-478.853	2.32917	-131.021	2.32917	-11.742	0	16	25.126	0	14	-625.535	2.32917		
37 M78	max 545.768	0	11	205.198	3.15411	30.017	3.15417	-6.659	3.15415	42.484	0	17	248.949	0.04911		
38	min -521.853	0	13	-201.878	3.15413	-52.515	0	19	-11.009	0	17	-41.086	4.65816	-241.279	0.06713	
39 M76	max 545.756	4.65811	201.859	1.50413	62.514	4.65816	11.053	4.65816	42.528	4.65816	248.914	4.61	11			
40	min -521.851	4.65815	-205.157	1.50417	-30.213	1.50418	8.507	0	14	-41.239	0	16	-241.247	4.65813		
41 M75	max 529.938	3.15415	127.066	4.65814	30.011	3.15417	-6.53	4.65814	42.579	0	16	179.503	0	18		
42	min -575.737	0	14	-130.845	3.20314	-52.508	0	19	-11.045	0	16	-41.241	4.65816	-171.773	0	14
43 M79	max 545.756	4.65810	201.859	1.50412	62.512	4.65816	11.01	4.65816	42.49	4.65816	248.914	4.61	13			
44	min -521.851	4.65812	-205.157	1.50416	-30.012	1.50416	6.959	1.50414	-41.086	0	17	-241.247	4.65812			
45 M36	max 1180.933	3.15410	256.237	4.65815	46.928	3.15418	-10.558	3.15414	69.514	0	16	353.366	0	19		
46	min -168.028	0	5	-256.914	3.20315	104.087	0	16	-9.546	0	16	-74.425	4.65817	-317.814	0	15
47 M35	max 1127.185	2.32919	410.513	2.28119	214.421	2.28119	17.487	4.65816	444.316	2.32919	592.859	2.32915	15			
48	min -1112.848	0	8	-110.625	2.32915	-216.745	2.32919	-17.455	0	17	37.464	4.65814	-603.146	2.32915		
49 M34	max 1151.231	4.65810	258.942	1.45610	104.05	4.65818	19.934	4.65817	69.437	4.65817	353.337	4.65819	10			
50	min -168.092	1.50413	-256.257	0	15	-46.902	1.50416	10.6	0	15	74.426	0	17	347.772	4.65815	
51 M33	max 1072.331	0	10	408	3.15410	46.968	3.15416	-10.558	4.65815	69.514	0	17	492.507	0.04510		
52	min -1059.597	0	12	-405.978	3.15412	-104.124	0	18	-19.946	0	17	-74.422	4.65817	-486.575	0.04512	
53 M32	max 925.705	4.65810	942.911	2.32912	214.037	2.28116	17.487	4.55917	443.891	2.32916	1235.293	2.32912	12			
54	min -912.475	2.32912	-950.439	2.32916	-216.362	2.32917	-17.574	0	18	37.464	4.65815	-1245.78	2.32916			
55 M30	max 1072.331	0	11	408	3.15411	46.968	3.15417	-11.03	3.15414	69.023	0	18	492.507	0.04811		
56	min -1058.581	0	13	-405.576	3.15413	-104.124	0	19	-19.792	3.20318	-73.86	4.65819	-486.575	0.04813		
57 M28	max 1127.185	2.32918	410.513	2.28118	215.826	2.32919	17.496	4.65816	444.316	2.32918	592.859	2.32914	18			
58	min -1112.848	0	14	-110.625	2.32914	-216.745	2.32918	-17.487	0	17	37.466	0	15	603.146	2.32914	
59 M28	max 1072.307	4.65811	405.526	1.50413	104.12	4.65819	19.948	4.55915	69.523	4.65815	492.438	4.61	11			
60	min -1058.54	4.65813	-407.959	1.50417	-46.96	1.50417	10.558	1.50414	-74.422	0	16	-486.494	4.61	13		
61 M29	max 925.705	4.65811	942.911	2.32913	215.826	2.32918	17.375	4.65818	443.891	2.32917	1235.293	2.32913	13			
62	min -912.475	2.32913	-950.439	2.32917	-216.362	2.32917	-17.467	0	15	37.466	0	14	-1246.78	2.32917		
63 M84	max 599.938	3.15410	127.066	4.65815	30.010	3.15418	-8.508	4.65814	42.622	0	16	179.503	0	19		
64	min -575.737	0	15	-130.845	3.20315	-52.517	0	15	-11.052	3.20315	-41.241	4.65817	-171.773	0	16	
65 M83	max 572.347	2.32919	208.828	2.28119	129.698	2.28118	11.742	4.65816	268.061	2.32919	292.337	2.32919	19			
66	min -549.933	0	15	208.537	2.32515	131.124	2.32918	-11.725	0	17	25.123	4.65814	-306.963	2.32915		
67 M82	max 599.964	4.65819	130.85	1.45519	62.506	4.65819	11.045	4.65817	42.583	4.65817	179.477	4.65819	19			

**Envelope Maximum Member Section Forces (Continued)**

Member	Axial [lb]	Loc [ft]	cy	Shear [lb]	Loc [ft]	cz	Shear [lb]	Loc [ft]	c	Torque [lb-ft]	Loc [ft]	cy-y	Moment [lb-ft]	Loc [ft]	cz-z	Moment [lb-ft]	Loc [ft]	c
68	min -575.759	1.50415	-127.073	0	15	-30.006	1.50416	8.531	0	15	-41.241	0	17	-171.752	4.65819			
69	M73 max 599.964	4.65818	130.65	1,458.8	62.514	4.65817	11.053	1,456.17	42.628	4.65817	179.477	4.65818						
70	min -575.759	1.50414	-127.073	0	14	-30.013	1.50419	8.507	0	15	-41.241	0	16	-171.752	4.65817			
71	M80 max 471.748	4.65810	474.391	2,281.10	129.595	2,281.16	11.742	4,659.17	267.953	2,329.16	613.707	2,329.12						
72	min -445.553	2.32912	-478.953	2,329.6	-131.021	2,329.16	-11.71	0	16	25.123	4.65819	-523.635	2,329.6					
73	M25 max 1181.031	4.65818	258.942	1,456.8	104.083	4,658.17	19.943	4,658.17	89.523	4,658.17	353.337	4,658.18						
74	min -1103.043	1.50414	-253.251	0	14	-46.82	1.50419	10.553	0	15	-74.428	0	16	-347.772	4.65814			
75	M74 max 572.347	2.32918	208.825	2,281.8	130.959	2,329.19	11.725	4,658.15	286.061	2,329.18	292.337	2,329.14						
76	min -548.693	0	14	-208.837	2,329.4	-131.124	2,329.18	-11.742	0	17	25.125	0	15	306.963	2,329.4			
77	M27 max 1180.933	3.15419	256.237	4,658.14	46.911	3,154.17	-10.599	3,154.14	59.429	0	16	353.368	0	16				
78	min -1166.028	0	14	-258.914	3,203.4	-104.064	0	19	19.932	0	16	-74.426	4,658.16	-347.314	0	14		
79	M51 max 545.786	0	10	205.188	3,154.10	30.018	3,154.19	8.506	3,154.15	42.622	0	17	248.943	0.04910				
80	min -621.559	0	12	-201.978	3,154.12	-62.317	0	17	-11.552	3,203.17	-41.239	4,658.17	-241.279	0.09713				
81	M1 max 1181.403	4.65818	69.213	4,658.18	306.015	1,504.12	16.22	1,458.15	320.076	4,658.18	263.337	4,658.12						
82	min -1091.595	4.65814	-17.536	1,504.19	-326.222	1,504.6	7.945	1,504.11	-294.18	4,658.14	-342.409	4,658.5						
83	M2 max 1045.488	2.32918	131.65	2,329.17	733.885	2,329.8	12.733	4,658.15	725.495	2,329.10	482.88	2,329.14						
84	min -970.539	0	14	131.779	2,329.18	-729.272	2,251.4	-12.732	0	15	599.266	2,329.12	-901.105	2,329.4				
85	M3 max 1161.396	0	8	17.543	3,154.18	329.237	3,154.10	-7.845	3,154.14	320.12	0	8	263.379	0	12			
86	min -1081.853	0	14	-69.215	0	15	-306.341	3,154.12	-16.219	0	16	-294.213	0	14	-342.437	0	5	
87	M4 max 1165.957	4.65811	69.194	4,658.18	297.906	1,504.15	16.226	1,458.18	316.266	4,658.11	259.369	4,658.15						
88	min -1066.184	4.65813	-17.519	1,504.17	-321.113	1,504.6	7.925	0	13	-290.375	4,658.13	-338.436	4,658.5					
89	M5 max 1053.661	2.32911	131.651	2,329.18	712.497	2,329.11	12.742	4,658.19	707.768	2,329.5	464.683	2,329.3						
90	min -978.646	0	13	-131.805	2,329.14	-758.227	2,281.7	-12.74	0	19	-581.497	2,329.15	583.085	2,329.7				
91	M7 max 1165.957	4.65810	69.194	4,658.18	297.906	1,504.14	16.226	1,458.19	316.266	4,658.10	259.369	4,658.4						
92	min -1066.184	4.65812	-17.519	1,504.15	-321.113	1,504.4	7.925	0	13	-290.375	4,658.12	-338.436	4,658.4					
93	M6 max 1053.661	2.32910	131.651	2,329.18	712.497	2,329.10	12.742	4,658.18	707.768	2,329.8	464.688	2,329.3						
94	min -978.646	0	12	-131.805	2,329.18	-758.227	2,281.6	-12.74	0	19	-581.497	2,329.14	583.085	2,329.5				
95	M9 max 1165.931	0	10	17.524	3,154.18	321.12	3,154.8	-7.825	3,154.12	316.303	0	10	259.408	0	14			
96	min -1066.178	0	12	-69.193	0	18	-287.326	3,154.14	-16.225	3,203.18	290.405	0	12	-338.456	0	4		
97	M11 max 1045.488	2.32919	131.651	2,329.18	733.885	2,329.9	12.733	4,658.17	725.485	2,329.11	482.88	2,329.5						
98	min -970.539	0	15	-131.779	2,329.19	-729.272	2,251.5	-12.732	0	17	599.266	2,329.13	-901.105	2,329.5				
99	M12 max 1181.396	0	9	17.543	3,154.19	329.237	3,154.11	-7.845	3,154.15	320.12	0	9	263.379	0	13			
100	min -1081.853	0	15	-69.215	0	17	-306.341	3,154.13	-16.219	3,203.17	-294.213	0	15	-342.437	0	7		
101	M6 max 1165.931	0	11	17.524	3,154.17	321.12	3,154.9	-7.825	3,154.13	316.303	0	11	259.408	0	15			
102	min -1066.178	0	13	-69.193	0	18	-287.326	3,154.15	-16.225	3,203.19	290.405	0	13	-338.456	0	5		
103	M10 max 1161.403	4.65819	69.213	4,658.17	306.015	1,504.13	16.22	1,458.17	320.076	4,658.5	263.337	4,658.3						
104	min -1091.595	4.65815	-17.535	1,504.19	-326.222	1,504.7	7.945	1,504.15	-294.18	4,658.15	-342.409	4,658.7						
105	S1 max 1442.969	2.5	15	1879.352	0	19	101.831	2.5	8	1.059	2.5	14	243.321	2.5	8	176.963	0	19
106	min -2229.018	0	5	-412.193	2.5	18	-101.910	1.172	-1.052	0	12	-243.285	2.5	8	2002.693	1.172	19	
107	M71 max 1633.182	2.5	9	-346.145	0	15	41.198	1.14810	0.071	2.5	12	98.775	2.5	10	1506.218	2.5	17	
108	min -632.469	0	15	-623.782	2.5	17	-41.17	0	4	-0.073	0	14	-98.779	2.5	4	-4.198	0	17
109	M70 max 1365.073	2.5	10	-347.767	0	12	41.198	1.14811	0.071	1.14813	98.775	2.5	11	1506.203	2.5	18		
110	min 26.367	1.17212	-623.387	2.5	18	-41.17	0	5	0.073	0	15	-98.779	2.5	5	-4.202	0	18	
111	M89 max 1365.073	2.5	11	-347.767	0	13	41.192	1.14818	0.068	2.5	14	98.681	2.5	9	1506.203	2.5	19	
112	min 26.367	1.17213	-623.387	2.5	19	-41.174	0	6	-0.076	0	12	-96.735	2.5	6	-4.202	0	19	
113	S2 max 1442.969	2.5	14	1879.352	0	18	101.818	2.5	11	1.057	1.14513	243.296	2.5	11	176.963	0	18	
114	min -2229.018	0	4	-412.193	2.5	18	-101.909	1.17215	-1.054	0	15	-243.287	2.5	13	-2002.693	1.172	13	
115	S3 max 1397.253	2.5	13	-879.85	0	17	101.818	2.5	10	1.057	2.5	12	243.206	2.5	10	176.943	0	17
116	min -2182.479	0	7	-412.517	2.5	17	101.820	1.17214	-1.054	0	14	-243.287	2.5	12	-2003.394	1.172	13	
117	S4 max 1397.253	2.5	12	-879.85	0	16	101.831	2.5	9	1.059	2.5	15	243.321	2.5	9	176.943	0	16
118	min -2182.479	0	5	-412.517	2.5	16	-101.815	1.17217	-1.052	0	13	-243.288	2.5	7	-2003.394	1.172	13	
119	M24 max 2646.43	2.5	8	1217.787	0	16	82.452	2.5	5	1.694	1.14619	197.043	2.5	13	86.87	0	16	
120	min -1999.465	0	14	-1055.776	2.5	16	-52.402	1.17217	-1.565	0	7	-197.259	2.5	15	-1317.708	1.172	13	
121	M23 max 2646.43	2.5	9	1217.787	0	17	82.452	2.5	10	1.555	1.14610	197.355	2.5	14	86.87	0	17	
122	min -1999.465	0	15	-1055.776	2.5	17	-52.4	1.17214	-1.705	0	4	-197.171	2.5	12	-1317.706	1.172	13	

Envelope Maximum Member Section Forces (Continued)

Member		Axial (lb)	Loc (ft)	Cy	Shear (lb)	Loc (ft)	Loz	Shear (lb)	Loc (ft)	Torque (lb-ft)	Loc (ft)	Loz-y Moment (lb-ft)	Loc (ft)	Loz-z Moment (lb-ft)	Loc (ft)					
123	M22	max	1515.753	2.5	10	217.055	0	18	82.452	2.5	11	-1.555	1.146	1	197.355	2.5	14	86.756	0	14
124		min	-869.005	0	2	-055.431	2.5	18	82.4	1.172	5	-1.705	0	5	-197.171	2.5	13	-1316.949	7	12
125	M21	max	1515.753	2.5	11	217.055	0	19	82.329	2.5	8	-1.694	1.146	8	197.043	2.5	12	86.756	0	12
126		min	-869.005	0	3	-055.431	2.5	10	-82.422	1.172	6	-1.565	0	6	-197.259	2.5	14	-1316.949	7	12
127	M72	max	1633.182	2.5	8	-346.145	0	14	41.152	1.146	9	0.058	2.5	15	98.581	2.5	9	1506.218	2.5	13
128		min	-538.458	0	4	-623.762	2.5	16	-47.174	0	7	-0.078	0	13	-98.725	2.5	7	-4.196	0	15
129	M17	max	1442.866	2.105	5	300.484	3.933	19	194.362	5.318	14	1.058	3.712	14	521.371	3.712	6	366.293	3.933	13
130		min	-1584.205	0	5	-723.906	3.878	19	-194.415	3.933	4	-1.062	0	17	-621.316	3.712	6	-1469.424	0	18
131	M18	max	1442.866	2.105	4	300.484	3.933	18	194.377	5.318	13	1.057	3.712	13	521.335	3.712	11	366.293	3.933	19
132		min	-1584.205	0	4	-723.906	3.878	18	-194.385	3.933	5	-1.064	0	16	-621.256	3.712	5	-1469.424	0	19
133	M19	max	1387.253	2.105	3	300.529	3.933	17	194.377	5.318	12	1.057	3.712	12	521.335	3.712	10	366.372	3.933	17
134		min	-1538.945	0	7	-723.857	3.878	17	-194.385	3.933	14	-1.064	0	14	-621.256	3.712	4	-1469.761	0	17
135	M85	max	1066.073	2.105	11	491.805	2.161	19	86.615	3.878	10	0.058	2.105	14	251.182	3.712	12	2893.152	2.151	19
136		min	-448.314	2.161	5	-678.074	2.105	19	-86.55	3.767	4	-0.076	0	12	-251.102	3.712	14	-23.451	5.318	17
137	M87	max	1633.182	2.105	9	492.654	2.161	17	86.611	3.878	8	0.071	3.712	12	251.24	3.712	14	2893.737	2.151	17
138		min	-1013.858	2.161	7	-678.338	2.105	17	-86.559	3.767	5	-0.073	2.161	14	-251.3	3.712	12	-23.44	5.318	19
139	M86	max	1066.073	2.105	10	491.805	2.161	18	86.611	3.878	9	0.071	3.712	13	251.24	3.712	15	2892.162	2.151	19
140		min	-448.314	2.161	4	-678.074	2.105	18	-86.595	3.767	7	-0.073	2.161	15	-251.3	3.712	13	-23.451	5.318	19
141	M20	max	1387.253	2.105	2	300.529	3.933	16	194.362	5.318	15	1.058	2.105	15	521.371	3.712	9	366.372	3.933	15
142		min	-1538.542	1.61	6	-723.887	3.878	16	-194.415	3.933	5	-1.062	2.161	13	-621.316	3.712	7	-1469.761	0	13
143	M37	max	1515.753	2.105	11	080.883	2.161	17	173.168	5.318	0	-1.554	2.105	6	502.544	3.712	8	2392.771	2.151	19
144		min	-980.963	2.161	5	-110.922	2.105	19	-172.842	3.933	4	-1.565	0	6	-502.325	3.712	6	-34.971	5.318	17
145	M39	max	2646.43	2.105	9	080.795	2.161	17	173.036	5.318	6	-1.555	3.712	0	502.61	3.712	10	2393.101	2.151	17
146		min	-2012.305	2.161	7	-111.216	2.105	17	-173.004	3.933	6	-1.705	2.161	4	-502.843	3.712	4	-34.924	5.318	15
147	M40	max	2646.43	2.105	8	080.795	2.161	16	173.168	5.318	11	-1.554	3.712	9	502.544	3.712	9	2393.101	2.151	16
148		min	-2012.308	2.161	5	-111.216	2.105	16	-172.842	3.933	5	-1.565	0	7	-502.325	3.712	7	-34.524	5.318	17
149	M88	max	1633.182	2.105	8	492.654	2.161	16	86.618	3.878	11	0.058	3.712	15	251.182	3.712	13	2893.737	2.151	16
150		min	-1013.858	2.161	5	-678.338	2.105	16	-86.55	3.767	5	-0.076	2.161	13	-251.102	3.712	15	-23.44	5.318	17
151	M38	max	1515.753	2.105	10	080.883	2.161	16	173.036	5.318	9	-1.555	2.105	11	502.61	3.712	11	2392.771	2.151	19
152		min	-980.963	2.161	4	-110.922	2.105	16	-173.004	3.933	7	-1.705	2.161	5	-502.843	3.712	5	-34.971	5.318	18
153	M97	max	920.746	5.072	3	57.795	5.072	5	-30.752	5.072	5	0	5.072	9	414.198	0	17	293.137	0	15
154		min	-924.265	0	7	-58.42	0	5	104.678	0	7	0	0	1	0	5.072	1	-296.309	0	5
155	M98	max	920.67	5.072	3	58.422	5.072	9	-30.15	5.072	5	0	5.072	9	414.194	0	17	296.323	0	9
156		min	-924.243	0	7	-57.8	0	5	104.878	0	7	0	0	1	0	5.072	1	-293.167	0	15
157	M99	max	1012.057	5.072	3	56.385	5.072	11	-62.726	5.072	4	0	5.072	9	722.458	0	16	255.986	0	11
158		min	-1013.222	0	7	-55.84	0	11	-165.594	0	6	0	0	1	0	5.072	1	-283.223	0	13
159	M100	max	1012.056	5.072	3	55.857	5.072	13	-62.95	5.072	4	0	5.072	9	722.058	0	16	293.279	0	13
160		min	-1018.245	0	7	55.593	0	7	165.574	0	6	0	0	1	0	5.072	1	-285.028	0	7
161	M101	max	502.04	5.072	3	28.455	5.072	11	-42.271	5.072	4	0	5.072	9	494.064	0	16	144.326	0	11
162		min	-514.158	0	7	-27.723	0	13	-120.552	0	6	0	0	1	0	5.072	1	-140.61	0	13
163	M102	max	502.045	5.072	3	27.726	5.072	13	-42.196	5.072	4	0	5.072	9	494.089	0	16	140.629	0	13
164		min	-514.18	0	7	-28.459	0	7	-120.552	0	6	0	0	1	0	5.072	1	-144.347	0	7
165	M103	max	920.67	5.072	2	58.422	5.072	8	-30.15	5.072	4	0	5.072	9	414.194	0	16	296.323	0	8
166		min	-924.243	0	6	-57.8	0	14	-104.676	0	6	0	0	1	0	5.072	1	-293.157	0	14
167	M104	max	1012.056	5.072	2	55.857	5.072	12	-62.723	5.072	5	0	5.072	9	722.451	0	17	293.279	0	12
168		min	-1018.245	0	6	55.593	0	6	165.592	0	7	0	0	1	0	5.072	1	-285.028	0	6
169	M105	max	502.045	5.072	2	27.726	5.072	12	-42.21	5.072	5	0	5.072	9	494.079	0	17	140.629	0	12
170		min	-514.18	0	6	-28.459	0	6	-120.552	0	7	0	0	1	0	5.072	1	-144.347	0	6
171	M106	max	502.04	5.072	2	28.455	5.072	10	-42.197	5.072	5	0	5.072	9	494.093	0	17	144.326	0	12
172		min	-514.158	0	6	-27.723	0	12	-120.57	0	7	0	0	1	0	5.072	1	-140.61	0	12
173	M107	max	1012.057	5.072	2	56.385	5.072	10	-62.952	5.072	5	0	5.072	9	722.065	0	17	255.986	0	12
174		min	-1018.222	0	6	-55.84	0	12	-165.577	0	7	0	0	1	0	5.072	1	-283.223	0	12
175	M108	max	920.746	5.072	2	57.795	5.072	14	-30.752	5.072	4	0	5.072	9	414.199	0	16	293.137	0	14
176		min	-924.265	0	6	-58.42	0	4	104.678	0	6	0	0	1	0	5.072	1	-296.309	0	4
177	M109	max	926.452	5.072	5	59.872	5.072	11	-29.782	5.072	3	0	5.072	9	414.615	0	18	303.670	0	11

**Envelope Maximum Member Section Forces (Continued)**

Member	Axial [lb]	Loc [ft]	LC	Shear [lb]	Loc [ft]	LC	Shear [lb]	Loc [ft]	LC	Torque [lb-ft]	Loc [ft]	LC	Loc-y Moment [lb-ft]	Loc [ft]	LC	Loc-z Moment [lb-ft]	Loc [ft]	LC
175	min -929.948	0	5	-59.254	0	3	-104.895	0	19	0	0	1	0	5.072	1	-300.543	0	13
179 M110	max 873.921	5.072	15	33.905	5.072	4	-61.921	5.072	15	0	5.072	19	723.815	0	17	171.969	0	14
180	min -881.253	0	5	-34.401	0	4	-165.881	0	17	0	0	1	0	5.072	1	-174.941	0	4
181 M111	max 433.152	5.072	15	16.757	5.072	4	-42.11	5.072	15	0	5.072	19	494.253	0	17	84.997	0	14
182	min -445.585	0	5	-17.501	0	4	-120.5	0	17	0	0	1	0	5.072	1	-88.764	0	4
183 M112	max 433.199	5.072	15	15.457	5.072	9	-42.112	5.072	15	0	5.072	19	494.257	0	17	76.599	0	9
184	min -445.523	0	5	-14.737	0	15	-120.502	0	17	0	0	1	0	5.072	1	-74.748	0	15
185 M113	max 874.015	5.072	15	30.38	5.072	9	-61.923	5.072	15	0	5.072	19	723.825	0	17	154.085	0	9
186	min -861.477	0	5	-29.883	0	15	-165.864	0	17	0	0	1	0	5.072	1	-157.567	0	15
187 M114	max 526.506	5.072	15	59.247	5.072	13	-29.763	5.072	15	0	5.072	19	414.818	0	19	300.504	0	13
188	min -929.964	0	5	-59.868	0	7	-104.901	0	19	0	0	1	0	5.072	1	-303.549	0	7
189 M115	max 926.452	5.072	14	59.872	5.072	10	-29.762	5.072	12	0	5.072	19	414.815	0	18	303.675	0	10
190	min -929.948	0	4	-59.254	0	12	-104.899	0	18	0	0	1	0	5.072	1	-300.543	0	12
191 M116	max 873.921	5.072	14	29.882	5.072	14	-61.921	5.072	14	0	5.072	19	723.818	0	16	151.566	0	14
192	min -881.293	0	4	-30.375	0	4	-165.881	0	16	0	0	1	0	5.072	1	-154.07	0	4
193 M117	max 433.152	5.072	14	14.737	5.072	14	-42.11	5.072	14	0	5.072	19	494.253	0	16	74.746	0	14
194	min -445.585	0	4	-15.458	0	4	-120.6	0	16	0	0	1	0	5.072	1	-78.403	0	4
195 M118	max 433.199	5.072	14	17.503	5.072	9	-42.112	5.072	14	0	5.072	19	494.257	0	16	68.778	0	9
196	min -445.523	0	4	-16.76	0	15	-120.502	0	16	0	0	1	0	5.072	1	-85.009	0	15
197 M119	max 874.015	5.072	14	34.501	5.072	9	-61.923	5.072	14	0	5.072	19	723.825	0	16	174.969	0	9
198	min -881.422	0	4	-33.912	0	15	-165.964	0	16	0	0	1	0	5.072	1	-172.001	0	15
199 M120	max 926.508	5.072	14	59.247	5.072	12	-29.763	5.072	12	0	5.072	19	414.818	0	18	300.504	0	12
200	min -929.964	0	4	-59.868	0	6	-104.901	0	19	0	0	1	0	5.072	1	-303.649	0	6

**Envelope Node Reactions**

Node Label	X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-ft]	LC	MY [lb-ft]	LC	MZ [lb-ft]	LC
1 R4	max 2182.479	10	1882.085	15	102.294	11	1.062	13	10.858	11	-110.414	14
2	min -970.27	12	1189.088	14	-102.281	5	-1.059	15	-10.876	5	-176.943	16
3 R1	max 102.294	10	1881.573	18	956.348	15	-110.711	13	10.858	10	1.559	14
4	min -102.281	4	1190.199	13	2329.019	5	-176.863	19	-10.876	4	-1.062	12
5 R3	max 102.3	10	1882.085	17	2182.479	11	176.943	17	10.853	8	1.064	14
6	min -102.263	4	1189.088	15	-910.27	13	110.414	15	-10.971	6	-1.057	12
7 R2	max 956.348	14	1881.573	19	102.3	11	1.057	13	10.863	9	-176.863	18
8	min -2229.018	4	1190.199	12	-102.283	5	-1.064	15	-10.871	7	110.711	12
9 N53	max 81.825	14	1216.824	19	674.296	11	-65.055	15	8.356	14	1.894	8
10	min -82.26	12	770.079	13	-869.028	13	86.769	19	-8.357	12	-1.555	6
11 N54	max 874.296	10	1216.824	18	81.872	15	1.555	11	8.386	9	86.769	18
12	min -869.005	12	770.079	12	-52.345	13	-1.705	5	-8.379	7	65.055	12
13 N55	max 81.872	14	1217.227	17	1999.455	15	86.87	17	8.386	8	1.705	8
14	min -82.345	12	767.955	15	-2003.773	5	54.846	15	-8.379	6	-1.555	6
15 N56	max 1999.455	14	1217.227	18	81.825	15	1.565	11	8.356	15	-54.846	14
16	min -2003.773	4	767.955	14	-82.29	13	-1.584	5	-8.357	15	-86.87	16
17 N101	max 40.896	14	-347.765	13	1066.073	11	4.202	19	4.179	10	0.068	14
18	min -41.074	12	-584.105	19	28.387	13	1.505	13	-4.187	4	-0.075	12
19 N102	max 1066.073	10	-347.765	12	40.919	15	0.071	13	4.19	13	-1.505	12
20	min 28.387	12	-584.105	18	-41.535	13	-0.073	15	-4.197	7	-4.202	18
21 N103	max 40.819	14	-346.152	15	538.469	15	-1.581	15	4.19	12	0.073	14
22	min -41.035	12	-584.526	17	-1533.182	5	-4.153	17	-4.191	6	-0.071	12
23 N104	max 538.469	14	-346.152	14	40.895	15	0.076	13	4.179	11	4.199	16
24	min -1633.782	4	-584.526	16	-41.014	13	-0.053	15	4.181	5	1.581	14
25 Totals:	max 7728.274	10	10057.249	19	7728.274	11						
26	min -7728.274	12	6452.807	14	-7728.274	13						



JOB NO.: U0142.2054.242

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PROJECT: NMC1-148 SPIKE

**ENCLOSURE CALCULATIONS**

FRP Member Design for Compression (RISA):

Label: FRP Kicker Brace

**INPUT:**

Unbraced Length, L [ft]: 10.6  
 Axial, C [lb]: 682  
 K: 1

**Notes:**

See RISA model member M48 for max axial force. Force  
 divided by 2 to account for double angles. Force multiplied by  
 0.8 to convert LRFD forces to ASD

Column: 4x4x3/8 FRP Angle

r [in]: 0.79  
 E [psi]: 2,800,000  
 A [in<sup>2</sup>]: 2.86

**OUTPUT:**

$f_c$  [psi]: 242 <  $F_u$  [psi]: 355 OK, 68%

**Select 4x4x3/8 FRP Angle FRP column****FRP Shear Connection w/ Steel Bolts:**

Label: Kicker to HSS typ.

Bearing stress of FRP member controls.

**INPUT:**

Design Force, P [lb]: 682  
 Steel Bolt Diameter, d, [in]: 1/2  
 # Bolts,  $n_b$ : 2  
 FRP Web Thickness,  $t_w$  [in]: 3/8  
 Double Shear: No  
 Bearing Stress: Longitudinal  
 Factor of Safety, FS: 4

**Notes:**

Design Force = axial in FRP Kicker Brace, typ.

**OUTPUT:**

$f_{b,y}$  [psi]: 1,844 <  $F_{b,y}$  [psi]: 7,500 OK, 25%

**Select (2) 1/2" diameter steel bolts**

See attached FRP material and section properties.



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PROJECT: NM01-146 SPIKE

FRP Member Design for Compression (RISA):

Label: FRP Vertical Brace

**INPUT:**

Unbraced Length, L [ft] 10.0  
 Axial C [lb] 318  
 K 1

**Notes:**

See RISA model member M42 for max axial force. Force divided by 2 to account for double angles. Force multiplied by 0.6 to convert LRFD forces to ASD

Column: 4x4x3/8 FRP Angle

r [in] 0.79  
 E [psi] 2,800,000  
 A [in<sup>2</sup>] 2.86

**OUTPUT:**

$f_c$  [psi] 11% <  $F_c$  [psi] 355 OK, 31%

**Select 4x4x3/8 FRP Angle FRP column**

FRP Shear Connection w/ Steel Bolts:

Label: Vertical Brace to HSS, typ.

Bearing stress of FRP member controls.

**INPUT:**

Design Force, P [lb] 318  
 Steel Bolt Diameter,  $d_b$  [in] 1/2  
 # Bolts,  $n_b$  2  
 FRP Web Thickness,  $t_w$  [in] 3/8  
 Double Shear: No  
 Bearing Stress: Lengthwise  
 Factor of Safety, FS 4

**Notes:**

Design Force = axial in FRP Vertical Brace, typ.

**OUTPUT:**

$f_{b1}$  [psi] 347 <  $F_{b1}$  [psi] 7,500 OK, 11%

**Select (2) 1/2" diameter steel bolts**

See attached FRP material and section properties.

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PROJECT: NM01-148 Spike

DESIGN APPROACH: LRFD

**BOLTED  
SHEAR CONNECTION**

Location: STEEL Stand Off Arm

Bolt Grade:	ASTM A325		
Bolt Diameter:	0.625	in	
Number of Bolts:	2		
Double Shear?	No		
Bolt Capacity:	24850	lbs	(AISC Equation J3-1)
Shear Load:	2546	lbs	
Check Bolt:	10.6%		

Result: **Select (2) 0.625 in. dia. ASTM A325 bolts.**

Note: See RISA model section set 'STEEL Stand Off Arm' load combination 4 for max Axial [lb]

**BOLT/PIN BEARING  
& MATERIAL TENSILE/SHEAR STRENGTH**

Location: STEEL Stand Off Arm

Bolt or Pin Diameter:	0.625	in		
Hole Diameter or Slot Width:	0.8875	in		
Number of Bolts or Pins:	2			
Plate Thickness:	0.375	in		
Plate Yield Strength (F <sub>y</sub> ):	38	ksi		
Plate Ultimate Strength (F <sub>u</sub> ):	58	ksi		
Bolt/Pin Parallel Edge Distance:	1	in		(measured from center of hole)
Bearing Capacity:	25692	lbs		
Perpendicular Edge Distance:	1	in		(measured from center of hole)
Effective Perp. Edge Distance:	1			
Tensile Rupture Capacity:	42820	lbs		(AISC Equation D5-1)
Shear Rupture Capacity:	37927	lbs		(AISC Equation D5-2)
Load:	2046	lbs		
Check Bearing:	10.3%			

Result: **Selected connection type is adequate.**

Note: See RISA model section set 'STEEL Stand Off Arm' load combination 4 for max Axial [lb]



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PROJECT: NM01-145 Spike

**BOLTED  
SHEAR CONNECTION**

Location: STEEL Outrigger Weldment

Bolt Grade:	ASTM A325	
Bolt Diameter:	0.625	in
Number of Bolts:	1	
Double Shear?	No	
Bolt Capacity:	12425	lbs (AISC Equation J3-1)
Shear Load:	1018	lbs
Check Bolt:	8.2%	

Result: **Select (1) 0.625 in. dia. ASTM A325 bolt.**

Note: See RISA model section set 'STEEL Outrigger Weldment' load combination 8 for max Axial [lb]

**BOLT/PIN BEARING  
& MATERIAL TENSILE/SHEAR STRENGTH**

Location: STEEL Outrigger Weldment

Bolt or Pin Diameter:	0.625	in	
Hole Diameter or Slot Width:	0.6875	in	
Number of Bolts or Pins:	1		
Plate Thickness:	0.375	in	
Plate Yield Strength ( $F_y$ ):	55	ksi	
Plate Ultimate Strength ( $F_u$ ):	58	ksi	
Bolt/Pin Parallel Edge Distance:	1	in	(measured from center of hole)
Bearing Capacity:	12846	lbs	
Perpendicular Edge Distance:	1	in	(measured from center of hole)
Effective Perp. Edge Distance:	1		
Tensile Rupture Capacity:	21410	lbs	(AISC Equation D5-1)
Shear Rupture Capacity:	18963	lbs	(AISC Equation D5-2)
Load:	1018	lbs	
Check Bearing:	7.9%		

Result: **Selected connection type is adequate.**

Note: See RISA model section set 'STEEL Outrigger Weldment' load combination 8 for max Axial [lb]



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**PROJECT:** NMC1-146 Spike**BOLTED  
SHEAR CONNECTION**

Location: STEEL Stand Off Arm Inner

Bolt Grade: ASTM A325

Bolt Diameter: 0.75 in

Number of Bolts: 3

Double Shear? No

Bolt Capacity: 53877 lbs (AISC Equation J3-1)

Shear Load: 1898 lbs

Check Bolt: 3.5%

**Result:** Select (3) 0.75 in. dia. ASTM A325 bolts.

**Note:** See RISA model section set 'STEEL Stand Off Arm Inner' load combination 6 for max Axial [lb]

**BOLT/PIN BEARING  
& MATERIAL TENSILE/SHEAR STRENGTH**

Location: STEEL Stand Off Arm Inner

Bolt or Pin Diameter: 0.75 in

Hole Diameter or Slot Width: 0.8125 in

Number of Bolts or Pins: 3

Plate Thickness: 0.375 in

Plate Yield Strength ( $F_y$ ): 36 ksiPlate Ultimate Strength ( $F_u$ ): 58 ksi

Bolt/Pin Parallel Edge Distance: 1 in

Bearing Capacity: 34638 lbs

Perpendicular Edge Distance: 1 in

Effective Perp. Edge Distance: 1

Tensile Rupture Capacity: 56113 lbs (AISC Equation D5-1)

Shear Rupture Capacity: 56890 lbs (AISC Equation D5-2)

Load: 1898 lbs

Check Bearing: 5.4%

**Result:** Selected connection type is adequate.

**Note:** See RISA model section set 'STEEL Stand Off Arm Inner' load combination 6 for max Axial [lb]

## Available AISC Checks:

Equation	Check?	Capacity
J3-6a	Yes	11623
J3-6b	No	
J5-8c	No	
J7-1	No	

(measured from center of hole)

(measured from center of hole)



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## Simulation of MONOPOLE MOUNT

Date: Thursday, October 24, 2024

Designer: JJB

Study name: Static 1

Analysis type: Static

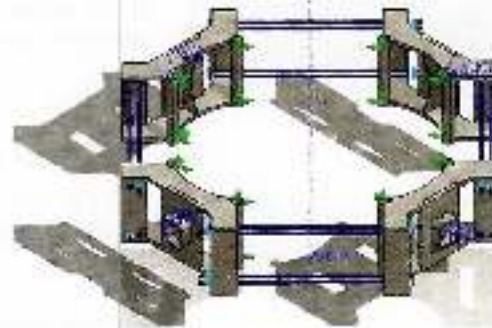
### Table of Contents

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Loads and Fixtures .....	11
Connector Definitions .....	15
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### Description

Four-sided Raycap Clamp





Model name: MONOPOLE MOUNT  
Current Configuration: Default

#### Solid Bodies

Document Name and Reference	Treated As	Volumetric Properties	Document Path/Date Modified
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024





Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup>	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt





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10/24/2024

		Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	Oct 23 17:20:18 2024
Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024



SOLIDWORKS

Assembled with SOLIDWORKS Simulation

Simulation of MONOPOLE MOUNT

4



Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
Boss-Extrude1	Solid Body	Mass:2.33967 lb Volume:8.2499 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.33808 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT SUPPORT.sldprt Oct 24 09:18:20 2024
Boss-Extrude1	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024
Mirror1	Solid Body	Mass:2.7207 lb Volume:9.59348 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:2.71886 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\2 x 0.145 - 6.sldprt Oct 24 13:00:27 2024
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Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024
Cut-Extrude1	Solid Body	Mass:6.53976 lb Volume:23.0598 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:6.53532 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\4 - 6.sldprt Oct 23 17:20:18 2024





Vector Structural Engineers, LLC  
651 W Galena Park Blvd., Suite 101  
Draper, UT 84020

JJB

10/24/2024

Boss-Extrude1	Solid Body	Mass:20.4191 lb Volume:72 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:20.4053 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT PLATE.sldprt Oct 23 17:42:47 2024
Cut-Extrude1	Solid Body	Mass:3.18636 lb Volume:11.2354 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:3.18419 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\MONOPOLE MOUNT STEEL TUBE.sldprt Oct 23 18:11:10 2024
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Mirror2	Solid Body	Mass:19.6216 lb Volume:69.1876 in <sup>3</sup> Density:0.283599 lb/in <sup>3</sup> Weight:19.6083 lbf	C:\Users\joshua.blom\Desktop\Raycap Clamp\W PLATE.sldprt Oct 24 09:10:00 2024





## Study Properties

Study name	Static 1
Analysis type	Static
Mesh type	Solid Mesh
Thermal Effect:	On
Thermal option	Include temperature loads
Zero strain temperature	77 Fahrenheit
Include fluid pressure effects from SOLIDWORKS Flow Simulation	Off
Solver type	FFEPlus
Inplane Effect:	Off
Soft Spring:	Off
Inertial Relief:	Off
Incompatible bonding options	Automatic
Large displacement	Off
Compute free body forces	Off
Friction	Off
Use Adaptive Method:	Off
Result folder	SOLIDWORKS document (C:\Users\joshua.blom\Desktop\Raycap Clamp\Results)

## Units

Unit system:	English (IPS)
Length/Displacement	in
Temperature	Fahrenheit
Angular velocity	Hertz
Pressure/Stress	ksi





## Material Properties

Model Reference	Properties	Components
	<p><b>Name:</b> ASTM A36 Steel  <b>Model type:</b> Linear Elastic Isotropic  <b>Default failure criterion:</b> Max von Mises Stress  <b>Yield strength:</b> 250 N/mm<sup>2</sup>  <b>Tensile strength:</b> 400 N/mm<sup>2</sup>  <b>Elastic modulus:</b> 200,000 N/mm<sup>2</sup>  <b>Poisson's ratio:</b> 0.26  <b>Mass density:</b> 7.85 g/cm<sup>3</sup>  <b>Shear modulus:</b> 79,300 N/mm<sup>2</sup></p>	<p>SolidBody  1(Mirror1)(Assem8^MONOPOL  E MOUNT-1/2 x 0.145 - 6-1),  SolidBody  1(Mirror1)(Assem8^MONOPOL  E MOUNT-1/2 x 0.145 - 6-2),  SolidBody 1(Cut-  Extrude1)(Assem8^MONOPOLE  MOUNT-1/4 - 6-1),  SolidBody 1(Cut-  Extrude1)(Assem8^MONOPOLE  MOUNT-1/4 - 6-2),  SolidBody 1(Boss-  Extrude1)(Assem8^MONOPOLE  MOUNT-1/MONOPOLE MOUNT  PLATE-1),  SolidBody 1(Cut-  Extrude1)(Assem8^MONOPOLE  MOUNT-1/MONOPOLE MOUNT  STEEL TUBE-1),  SolidBody 1(Boss-  Extrude1)(Assem8^MONOPOLE  MOUNT-1/MONOPOLE MOUNT  SUPPORT-1),  SolidBody 1(Boss-  Extrude1)(Assem8^MONOPOLE  MOUNT-1/W PLATE-2),  SolidBody  2(Mirror2)(Assem8^MONOPOL  E MOUNT-1/W PLATE-2),  SolidBody  1(Mirror1)(Assem8^MONOPOL  E MOUNT-10/2 x 0.145 - 6-1),  SolidBody  1(Mirror1)(Assem8^MONOPOL  E MOUNT-10/2 x 0.145 - 6-2),  SolidBody 1(Cut-  Extrude1)(Assem8^MONOPOLE  MOUNT-10/4 - 6-1),  SolidBody 1(Cut-  Extrude1)(Assem8^MONOPOLE  MOUNT-10/4 - 6-2),  SolidBody 1(Boss-  Extrude1)(Assem8^MONOPOLE</p>





		<p>       MOUNT-10/MONPOLE        MOUNT PLATE-1),        SolidBody 1(Cut-        Extrude1)(Assem8 MONOPOLE        MOUNT-10/MONPOLE        MOUNT STEEL TUBE-1),        SolidBody 1(Boss-        Extrude1)(Assem8 MONOPOLE        MOUNT-10/MONPOLE        MOUNT SUPPORT-1),        SolidBody 1(Boss-        Extrude1)(Assem8 MONOPOLE        MOUNT-10/W PLATE-2),        SolidBody        2(Mirror2)(Assem8 MONOPOLE        MOUNT-10/W PLATE-2),        SolidBody        1(Mirror1)(Assem8 MONOPOLE        MOUNT-11/2 x 0.145 - 6-1),        SolidBody        1(Mirror1)(Assem8 MONOPOLE        MOUNT-11/2 x 0.145 - 6-2),        SolidBody 1(Cut-        Extrude1)(Assem8 MONOPOLE        MOUNT-11/4 - 6-1),        SolidBody 1(Cut-        Extrude1)(Assem8 MONOPOLE        MOUNT-11/4 - 6-2),        SolidBody 1(Boss-        Extrude1)(Assem8 MONOPOLE        MOUNT-11/MONPOLE        MOUNT PLATE-1),        SolidBody 1(Cut-        Extrude1)(Assem8 MONOPOLE        MOUNT-11/MONPOLE        MOUNT STEEL TUBE-1),        SolidBody 1(Boss-        Extrude1)(Assem8 MONOPOLE        MOUNT-11/MONPOLE        MOUNT SUPPORT-1),        SolidBody 1(Boss-        Extrude1)(Assem8 MONOPOLE        MOUNT-11/W PLATE-2),        SolidBody        2(Mirror2)(Assem8 MONOPOLE        MOUNT-11/W PLATE-2),        SolidBody        1(Mirror1)(Assem8 MONOPOLE        MOUNT-8/2 x 0.145 - 6-1),     </p>
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JJB  
10/24/2024

		<p>SolidBody 1(Mirror1)(Assem8^MONOPOLE MOUNT-8/2 x 0.145 - 6-2), SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-8/4 - 6-1), SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-8/4 - 6-2), SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-8/MONOPOLE MOUNT PLATE-1), SolidBody 1(Cut-Extrude1)(Assem8^MONOPOLE MOUNT-8/MONOPOLE MOUNT STEEL TUBE-1), SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-8/MONOPOLE MOUNT SUPPORT-1), SolidBody 1(Boss-Extrude1)(Assem8^MONOPOLE MOUNT-8/W PLATE-2), SolidBody 2(Mirror2)(Assem8^MONOPOLE MOUNT-8/W PLATE-2)</p>
Curve Data:N/A		



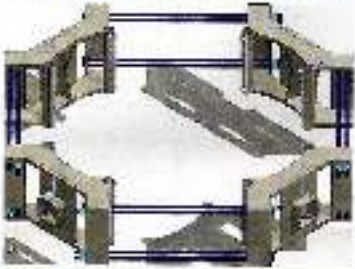
SOLIDWORKS



Rendered with SOLIDWORKS simulation

Simulation of MONOPOLE MOUNT





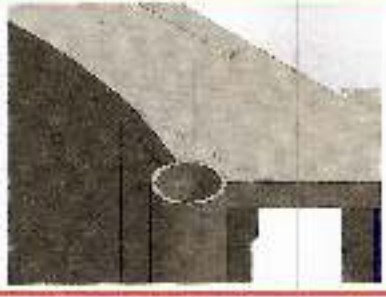

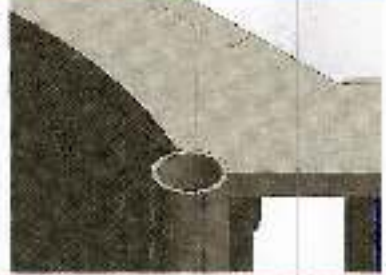
## Loads and Fixtures

Fixture name	Fixture Image	Fixture Details		
Reference Geometry-2		<p>Entities: 8 edge(s) Reference: Face-1 x Type: Use reference geometry Translation: 0, 0 rad., 0 Units: in</p>		
<b>Resultant Forces</b>				
Components	X	Y	Z	Resultant
Reaction force(lbf)	0.729984	-7,184.11	0.138231	7,184.11
Reaction Moment(lbf.In)	0	0	0	0

Load name	Load Image	Load Details
Gravity-1		<p>Reference: Top Plane Values: 0 0 -386.22 Units: in/s^2</p>
Force-1		<p>Entities: 1 face(s) Type: Apply normal force Value: -2,229 .lbf</p>

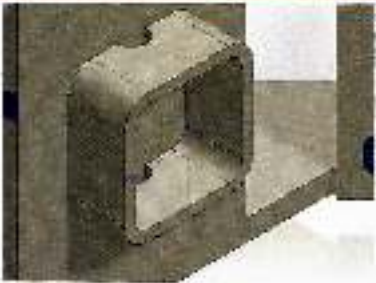
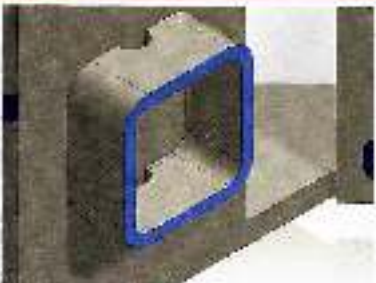
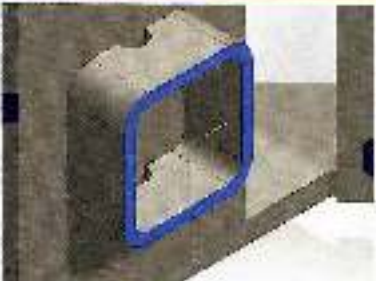





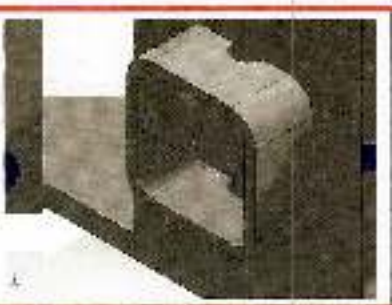
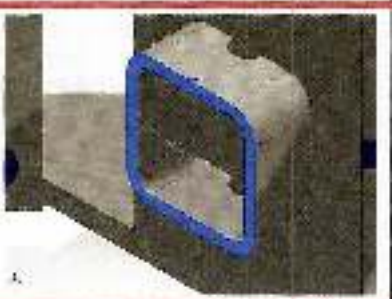
Force-2		<p>Entities: 1 face(s) Reference: Axis2 Type: Apply force Values: ---, ---, -1,879.9 lbf</p>
Torque-1		<p>Entities: 1 face(s) Reference: Axis6 Type: Apply torque Value: 18,074.6 lbf.in</p>
Copy[ 1 ] Force-1		<p>Entities: 1 face(s) Type: Apply normal force Value: -2,229 lbf</p>
Copy[ 1 ] Force-2		<p>Entities: 1 face(s) Reference: Axis17 Type: Apply force Values: ---, ---, 1,879.9 lbf</p>
Copy[ 1 ] Torque-1		<p>Entities: 1 face(s) Reference: Axis18 Type: Apply torque Value: 18,074.6 lbf.in</p>

25



<p>Copy[ 1 ] Force-1[1]</p>		<p>Entities: 1 face(s) Type: Apply normal force Value: -2,229 lbf</p>
<p>Copy[ 1 ] Force-2[1]</p>		<p>Entities: 1 face(s) Reference: Axis19 Type: Apply force Values: ---, ---, 1,879.9 lbf</p>
<p>Copy[ 1 ] Torque-1[1]</p>		<p>Entities: 1 face(s) Reference: Axis20 Type: Apply torque Value: 18,074.6 lbf.in</p>
<p>Copy[ 1 ] Force-1[13][1]</p>		<p>Entities: 1 face(s) Type: Apply normal force Value: -2,229 lbf</p>

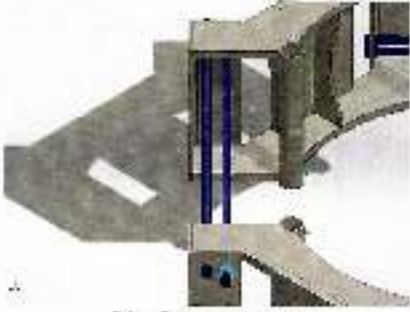
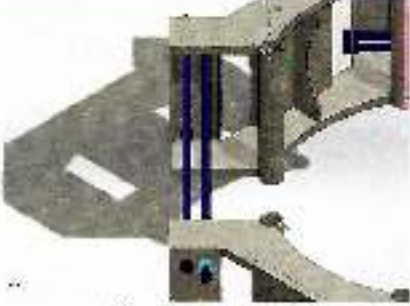


<p>Copy[ 1 ] Force-2[1][1]</p>		<p>Entities: 1 face(s) Reference: Axis16 Type: Apply force Values: ---, ---, -1,879.9 lbf</p>
<p>Copy[ 1 ] Torque-1[1][1]</p>		<p>Entities: 1 face(s) Reference: Axis15 Type: Apply torque Value: 18,074.6 lbf.in</p>



## Connector Definitions

### Pin/Bolt/Bearing Connector

Model Reference	Connector Details	Strength Details		
 <p>Pin Connector-1</p>	Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0	No Data		
<b>Connector Forces Joint 1</b>				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	299.43	0	299.43	423.46
Shear Force (lbf)	0.29259	0.15461	-0.29257	0.44171
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	95.95	137.48	-95.95	193.17
<b>Connector Forces Joint 2</b>				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-299.43	-0	-299.43	-423.46
Shear Force (lbf)	-0.29259	-0.15461	0.29257	0.44171
Torque (lbf.in)	4.2204e-06	0	4.2204e-06	5.9685e-06
Bending moment (lbf.in)	-99.197	-125.19	99.197	188.02
 <p>Pin Connector-2</p>	Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0	No Data		





Connector Forces Joint 1				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	167.08	-0	167.08	-236.29
Shear Force (lbf)	-0.14211	-0.044949	0.14209	0.20592
Torque (lbf.in)	-2.2336e-08	0	-2.2336e-08	3.1589e-08
Bending moment (lbf.in)	50.597	-57.461	-50.597	91.771

Connector Forces Joint 2				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-167.08	0	-167.08	236.29
Shear Force (lbf)	0.14211	0.044949	-0.14209	0.20592
Torque (lbf.in)	6.4084e-08	-0	6.4084e-08	-9.0628e-08
Bending moment (lbf.in)	-51.588	63.724	51.588	96.868



Pin Connector-3

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

Connector Forces Joint 1				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	148.6	-0	148.6	-210.15
Shear Force (lbf)	0.34643	-0.28745	-0.34642	0.56802
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	-60.912	46.294	60.912	97.794

Connector Forces Joint 2				
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-148.6	0	-148.6	210.15
Shear Force (lbf)	-0.34643	0.28745	0.34642	0.56802
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	54.792	-61.043	-54.792	98.644

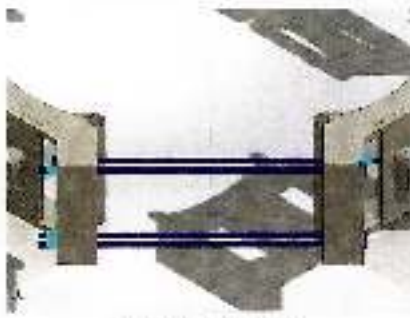




	<p>Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection: Rigid Type: Units: English (IPS) Rotational stiffness value: 0</p>	No Data																									
Pin Connector-4																											
Connector Forces Joint 1																											
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Shear Force (lbf)	-0.13743	0.077944	0.13743	0.2094																							
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Connector Forces Joint 2																											
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	<p>Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection: Rigid Type: Units: English (IPS) Rotational stiffness value: 0</p>	No Data																									
Pin Connector-5																											
Connector Forces Joint 1																											
<table border="1"> <thead> <tr> <th>Type</th> <th>X-Component</th> <th>Y-Component</th> <th>Z-Component</th> <th>Resultant</th> </tr> </thead> <tbody> <tr> <td>Axial Force (lbf)</td> <td>296.1</td> <td>0</td> <td>-296.1</td> <td>418.75</td> </tr> <tr> <td>Shear Force (lbf)</td> <td>0.17629</td> <td>-0.14127</td> <td>0.17627</td> <td>0.28655</td> </tr> <tr> <td>Torque (lbf.in)</td> <td>0</td> <td>0</td> <td>-0</td> <td>0</td> </tr> <tr> <td>Bending moment (lbf.in)</td> <td>-100.37</td> <td>124.44</td> <td>-100.37</td> <td>188.77</td> </tr> </tbody> </table>	Type	X-Component	Y-Component	Z-Component	Resultant	Axial Force (lbf)	296.1	0	-296.1	418.75	Shear Force (lbf)	0.17629	-0.14127	0.17627	0.28655	Torque (lbf.in)	0	0	-0	0	Bending moment (lbf.in)	-100.37	124.44	-100.37	188.77		
Type	X-Component	Y-Component	Z-Component	Resultant																							
Axial Force (lbf)	296.1	0	-296.1	418.75																							
Shear Force (lbf)	0.17629	-0.14127	0.17627	0.28655																							
Torque (lbf.in)	0	0	-0	0																							
Bending moment (lbf.in)	-100.37	124.44	-100.37	188.77																							
Connector Forces Joint 2																											



Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-796.1	-0	296.1	-418.75
Shear Force (lbf)	-0.17629	0.14127	-0.17627	0.28655
Torque (lbf.in)	0	0	-0	0
Bending moment (lbf.in)	97.468	-131.69	97.468	190.64



Pin Connector-6

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

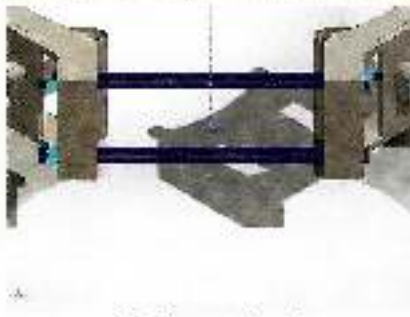
No Data

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	177.69	-0	-177.69	-251.29
Shear Force (lbf)	-0.041436	0.011963	-0.041423	0.059799
Torque (lbf.in)	3.2385e-07	-0	-3.2385e-07	-4.5799e-07
Bending moment (lbf.in)	-57.751	-60.293	-57.751	101.52

**Connector Forces Joint 2**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-177.69	0	177.69	251.29
Shear Force (lbf)	0.041436	-0.011963	0.041423	0.059799
Torque (lbf.in)	-3.0908e-07	0	3.0908e-07	4.3711e-07
Bending moment (lbf.in)	57.401	57.866	57.401	99.69



Pin Connector-7

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
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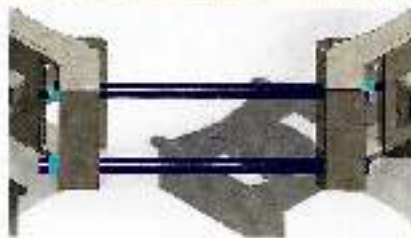




Axial Force (lbf)	-138.99	-0	138.99	-196.57
Shear Force (lbf)	-0.073459	0.13005	-0.073473	0.16646
Torque (lbf.in)	-2.034e-06	0	2.034e-06	-2.8765e-06
Bending moment (lbf.in)	-51.875	-49.745	-51.875	88.64

#### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	138.99	0	-138.99	196.57
Shear Force (lbf)	0.073459	-0.13005	0.073473	0.16646
Torque (lbf.in)	1.913e-06	0	-1.913e-06	2.7054e-06
Bending moment (lbf.in)	54.745	52.992	54.745	93.82



Pin Connector-8

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection: Rigid  
Type:  
Units: English (IPS)  
Rotational stiffness value: 0

No Data

#### Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	12.477	0	-12.477	17.645
Shear Force (lbf)	-0.055332	-0.039551	-0.055333	0.08768
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	-21.054	-17.502	-21.054	34.538

#### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-12.477	0	12.477	-17.645
Shear Force (lbf)	0.055332	0.039551	0.055333	0.08768
Torque (lbf.in)	1.0551e-06	0	-1.0551e-06	1.4921e-06
Bending moment (lbf.in)	20.211	19.861	20.211	34.806





	<p>                 Entities: 2 face(s)                  Type: Pin                  With retaining ring (No translation): Yes                  With key (No rotation): No                  Connection Type: Rigid                  Units: English (IPS)                  Rotational stiffness value: 0             </p>	<p>No Data</p>
--	---	----------------

Pin Connector-9

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-289.93	0	-289.93	410.03
Shear Force (lbf)	0.31207	-0.4776	-0.31209	0.6503
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	-97.56	122.94	97.56	184.8

**Connector Forces Joint 2**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	289.93	-0	289.93	-410.03
Shear Force (lbf)	-0.31207	0.4776	0.31209	0.6503
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	87.434	-136.17	-87.434	184.94

	<p>                 Entities: 2 face(s)                  Type: Pin                  With retaining ring (No translation): Yes                  With key (No rotation): No                  Connection Type: Rigid                  Units: English (IPS)                  Rotational stiffness value: 0             </p>	<p>No Data</p>
--	---	----------------

Pin Connector-10

**Connector Forces Joint 1**

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	195.92	-0	195.92	-277.07
Shear Force (lbf)	0.23139	-0.1846	-0.23138	0.37571
Torque (lbf.in)	-0	0	-0	0
Bending moment (lbf.in)	63.693	65.094	-63.693	111.13

**Connector Forces Joint 2**





Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-195.92	0	-195.92	277.07
Shear Force (lbf)	-0.23139	0.1846	0.23138	0.37571
Torque (lbf.in)	2.1102e-06	-0	2.1102e-06	-2.9842e-06
Bending moment (lbf.in)	-67.595	-74.877	67.595	121.43



Pin Connector-11

Entities: 2 face(s)  
 Type: Pin  
 With retaining ring (No translation): Yes  
 With key (No rotation): No  
 Connection: Rigid  
 Type:  
 Units: English (IPS)  
 Rotational stiffness value: 0

No Data

Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-140.61	-0	-140.61	-198.85
Shear Force (lbf)	0.40394	0.44276	-0.40395	0.72276
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	51.57	57.884	-51.57	93.11

Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	140.61	0	140.61	198.85
Shear Force (lbf)	-0.40394	-0.44276	0.40395	0.72276
Torque (lbf.in)	0	0	0	0
Bending moment (lbf.in)	-61.01	-40.66	61.01	95.382



Pin Connector-12

Entities: 2 face(s)  
 Type: Pin  
 With retaining ring (No translation): Yes  
 With key (No rotation): No  
 Connection: Rigid  
 Type:  
 Units: English (IPS)  
 Rotational stiffness value: 0

No Data

Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
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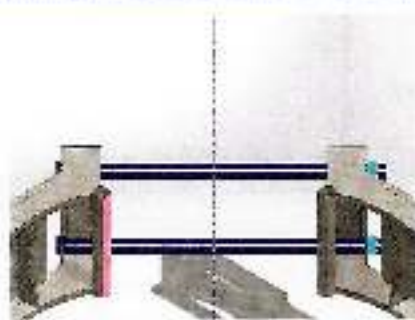




Axial Force (lbf)	21.421	0	21.421	30.293
Shear Force (lbf)	0.19279	0.31392	-0.19279	0.41578
Torque (lbf.in)	-9.8166e-09	-0	-9.8166e-09	-1.3883e-08
Bending moment (lbf.in)	12.75	24.596	-12.75	30.497

#### Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-21.421	-0	-21.421	-30.293
Shear Force (lbf)	-0.19279	-0.31392	0.19279	0.41578
Torque (lbf.in)	-2.3525e-07	-0	-2.3525e-07	-3.327e-07
Bending moment (lbf.in)	-19.452	-16.364	19.452	32.008



Pin Connector-13

Entities: 2 face(s)  
Type: Pin  
With retaining ring (No translation): Yes  
With key (No rotation): No  
Connection Type: Rigid  
Units: English (IPS)  
Rotational stiffness value: 0

No Data


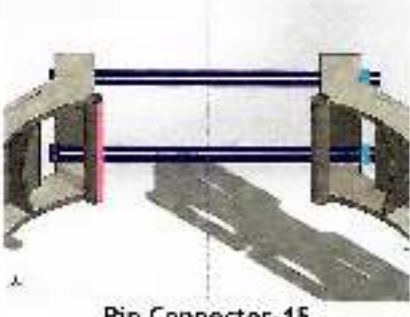
#### Connector Forces Joint 1

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-4.5667	0	4.5667	6.4583
Shear Force (lbf)	0.29607	1.3987	0.29607	1.46
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-17.015	14.157	-17.015	27.919

#### Connector Forces Joint 2

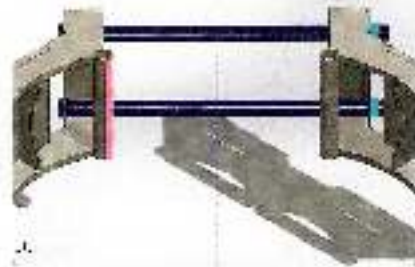
Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	4.5667	-0	-4.5667	-6.4583
Shear Force (lbf)	-0.29607	-1.3987	-0.29607	1.46
Torque (lbf.in)	-5.2755e-07	0	5.2755e-07	7.4606e-07
Bending moment (lbf.in)	-12.839	-1.5182	-12.839	18.22



 <p>Pin Connector-14</p>	<p>Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0</p>	<p>No Data</p>																											
<p><b>Connector Forces Joint 1</b></p>																													
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Type	X-Component	Y-Component	Z-Component	Resultant																									
Axial Force (lbf)	11.271	-0	-11.271	-15.94																									
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Torque (lbf.in)	-0	0	0	0																									
Bending moment (lbf.in)	-18.251	7.4271	-18.251	26.858																									
<p><b>Connector Forces Joint 2</b></p>																													
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Type	X-Component	Y-Component	Z-Component	Resultant																									
Axial Force (lbf)	-11.271	0	11.271	15.94																									
Shear Force (lbf)	-0.2995	-1.7639	-0.2995	1.814																									
Torque (lbf.in)	-0	0	0	0																									
Bending moment (lbf.in)	-19.398	5.3579	-19.398	27.951																									
 <p>Pin Connector-15</p>	<p>Entities: 2 face(s) Type: Pin With retaining ring (No translation): Yes With key (No rotation): No Connection Type: Rigid Units: English (IPS) Rotational stiffness value: 0</p>	<p>No Data</p>																											
<p><b>Connector Forces Joint 1</b></p>																													
<table border="1"> <thead> <tr> <th>Type</th> <th>X-Component</th> <th>Y-Component</th> <th>Z-Component</th> <th>Resultant</th> </tr> </thead> <tbody> <tr> <td>Axial Force (lbf)</td> <td>4.7067</td> <td>-0</td> <td>-4.7067</td> <td>-6.6563</td> </tr> <tr> <td>Shear Force (lbf)</td> <td>-0.36657</td> <td>1.48</td> <td>-0.36657</td> <td>1.5682</td> </tr> <tr> <td>Torque (lbf.in)</td> <td>-2.8054e-07</td> <td>0</td> <td>2.8054e-07</td> <td>3.9674e-07</td> </tr> <tr> <td>Bending moment (lbf.in)</td> <td>-18.377</td> <td>-16.867</td> <td>-18.377</td> <td>30.983</td> </tr> </tbody> </table>	Type	X-Component	Y-Component	Z-Component	Resultant	Axial Force (lbf)	4.7067	-0	-4.7067	-6.6563	Shear Force (lbf)	-0.36657	1.48	-0.36657	1.5682	Torque (lbf.in)	-2.8054e-07	0	2.8054e-07	3.9674e-07	Bending moment (lbf.in)	-18.377	-16.867	-18.377	30.983				
Type	X-Component	Y-Component	Z-Component	Resultant																									
Axial Force (lbf)	4.7067	-0	-4.7067	-6.6563																									
Shear Force (lbf)	-0.36657	1.48	-0.36657	1.5682																									
Torque (lbf.in)	-2.8054e-07	0	2.8054e-07	3.9674e-07																									
Bending moment (lbf.in)	-18.377	-16.867	-18.377	30.983																									
<p><b>Connector Forces Joint 2</b></p>																													



Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-4.7067	0	4.7067	6.6563
Shear Force (lbf)	0.36657	-1.48	0.36657	1.5682
Torque (lbf.in)	2.9124e-08	-0	-2.9124e-08	-4.1187e-08
Bending moment (lbf.in)	-13.208	1.221	-13.208	18.719



Pin Connector-16

Entities: 2 face(s)  
 Type: Pin  
 With retaining ring (No translation): Yes  
 With key (No rotation): No  
 Connection Type: Rigid  
 Units: English (IPS)  
 Rotational stiffness value: 0

No Data

## Connector Forces Joint 1

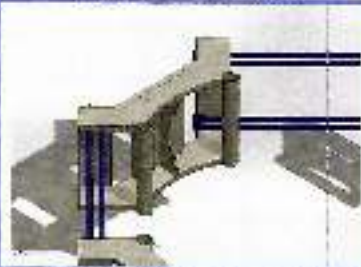

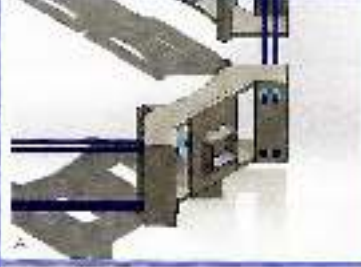

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	-11.411	0	11.411	16.138
Shear Force (lbf)	-0.22899	1.8998	-0.22899	1.9272
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-21.217	-4.4156	-21.217	30.329

## Connector Forces Joint 2

Type	X-Component	Y-Component	Z-Component	Resultant
Axial Force (lbf)	11.411	-0	-11.411	-16.138
Shear Force (lbf)	0.22899	-1.8998	0.22899	1.9272
Torque (lbf.in)	-0	0	0	0
Bending moment (lbf.in)	-19.333	-5.3556	-19.333	27.861



## Interaction Information

Interaction	Interaction Image	Interaction Properties
Component Contact-9		<b>Type:</b> Bonded <b>Components:</b> 5 component(s), 2 Solid Body (s) <b>Options:</b> Continuous mesh
Component Interaction-12		<b>Type:</b> Bonded <b>Components:</b> 8 component(s) <b>Options:</b> Independent mesh
Component Interaction-13		<b>Type:</b> Bonded <b>Components:</b> 8 component(s) <b>Options:</b> Independent mesh
Component Interaction-14		<b>Type:</b> Bonded <b>Components:</b> 8 component(s) <b>Options:</b> Independent mesh





### Mesh information

Mesh type	Solid Mesh
Mesher Used:	Curvature-based mesh
Jacobian points for High quality mesh	16 Points
Maximum element size	2 in
Minimum element size	0.4 in
Mesh Quality	High
Remesh failed parts independently	Off

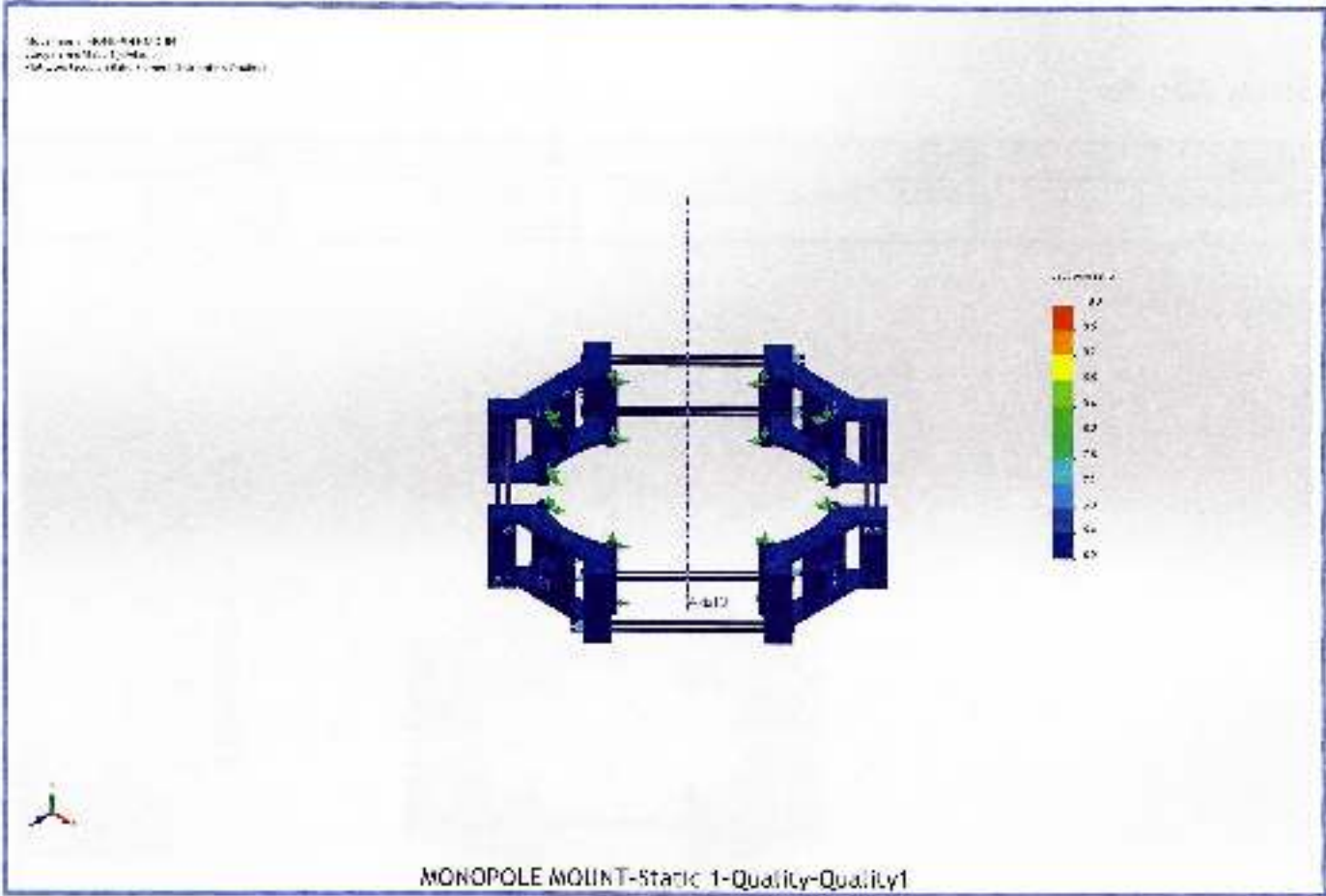
### Mesh Information - Details

Total Nodes	74378
Total Elements	35555
Maximum Aspect Ratio	53.291
% of elements with Aspect Ratio < 3	49.7
Percentage of elements with Aspect Ratio > 10	3.55
Percentage of distorted elements	0
Time to complete mesh(hh:mm:ss):	00:00:05
Computer name:	VSE096

### Mesh Quality Plots

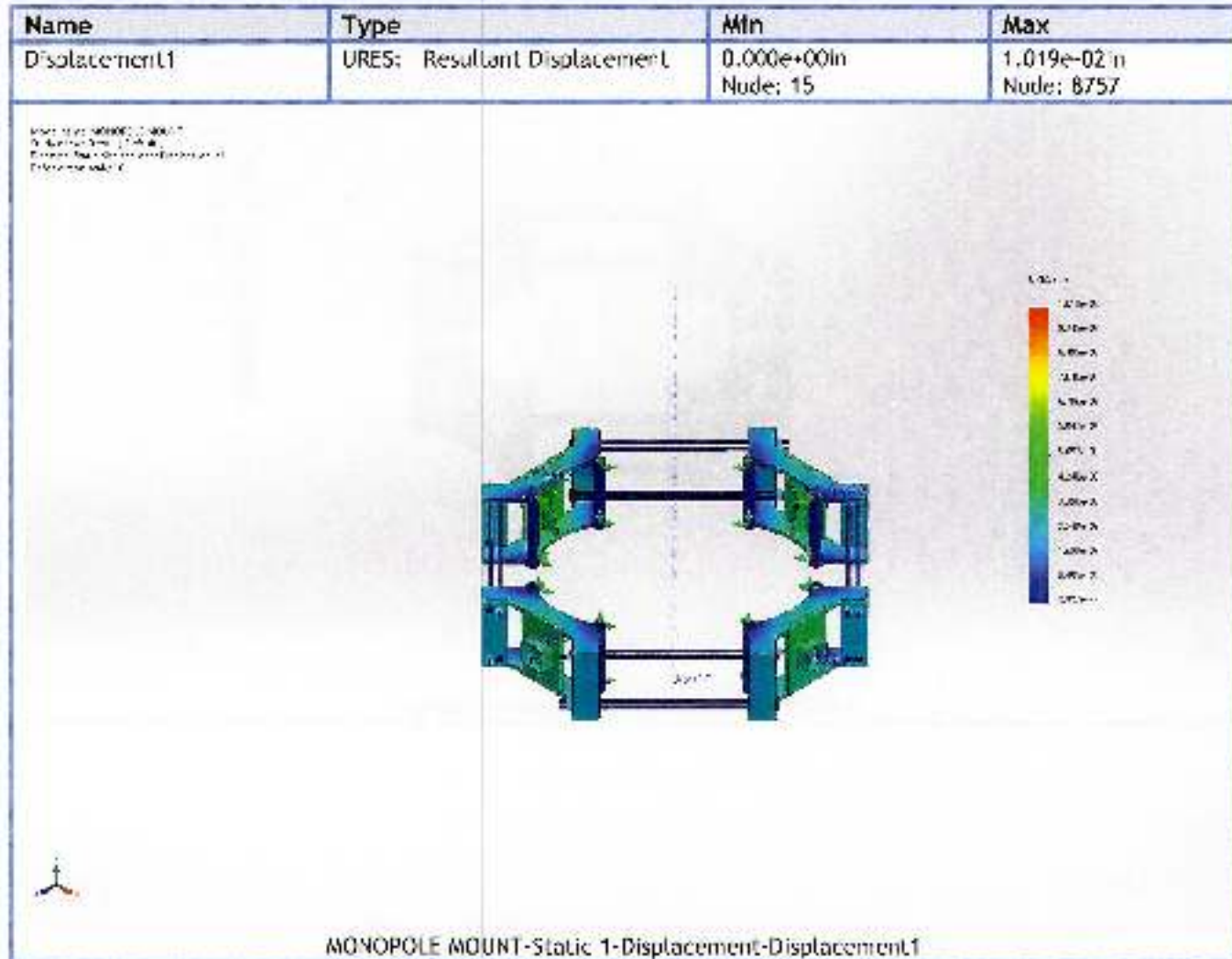
Name	Type	Min	Max
Quality1	Jacobian ratio	1.0 Element: 2023	28.9 Element: 20129





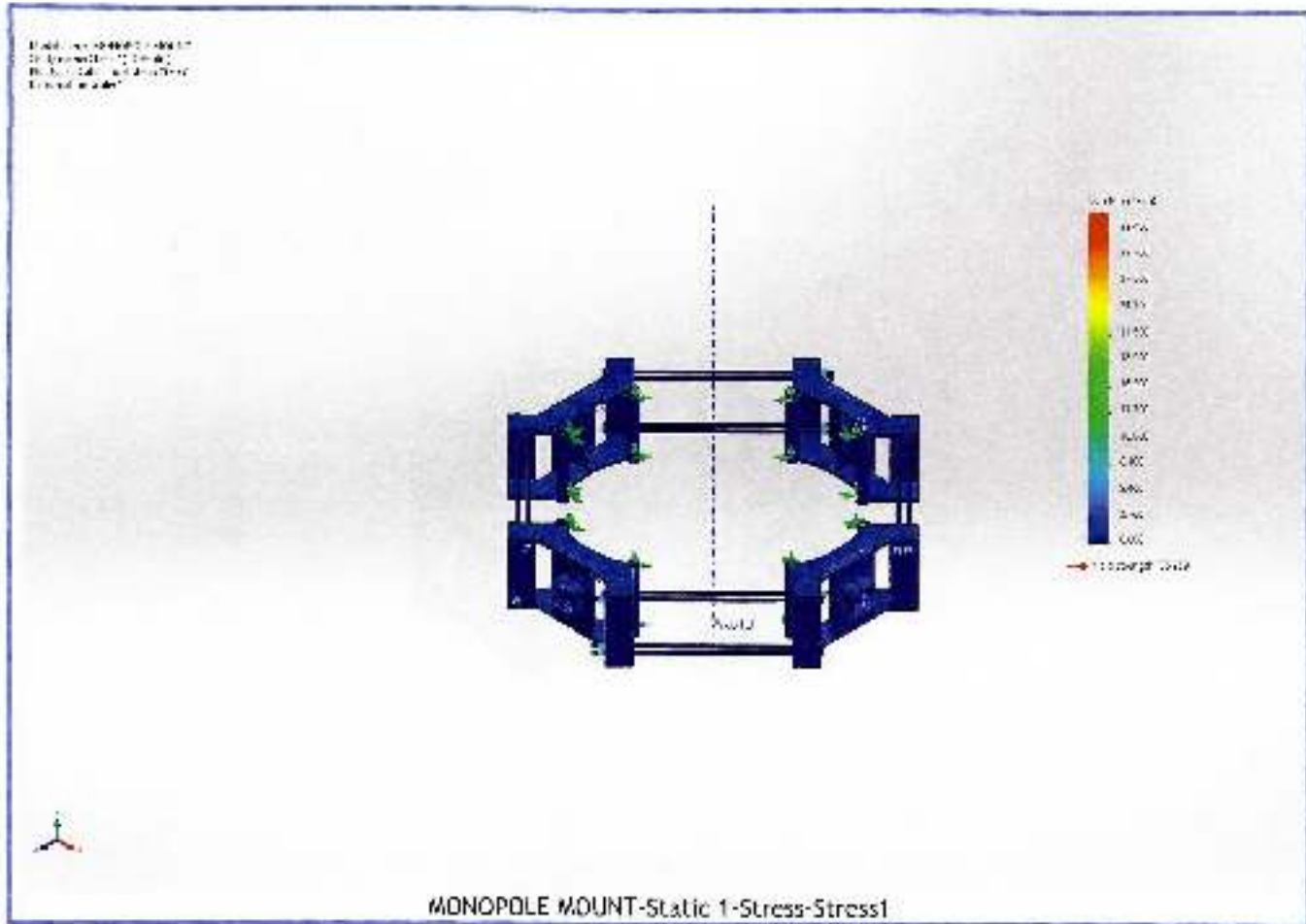


## Study Results



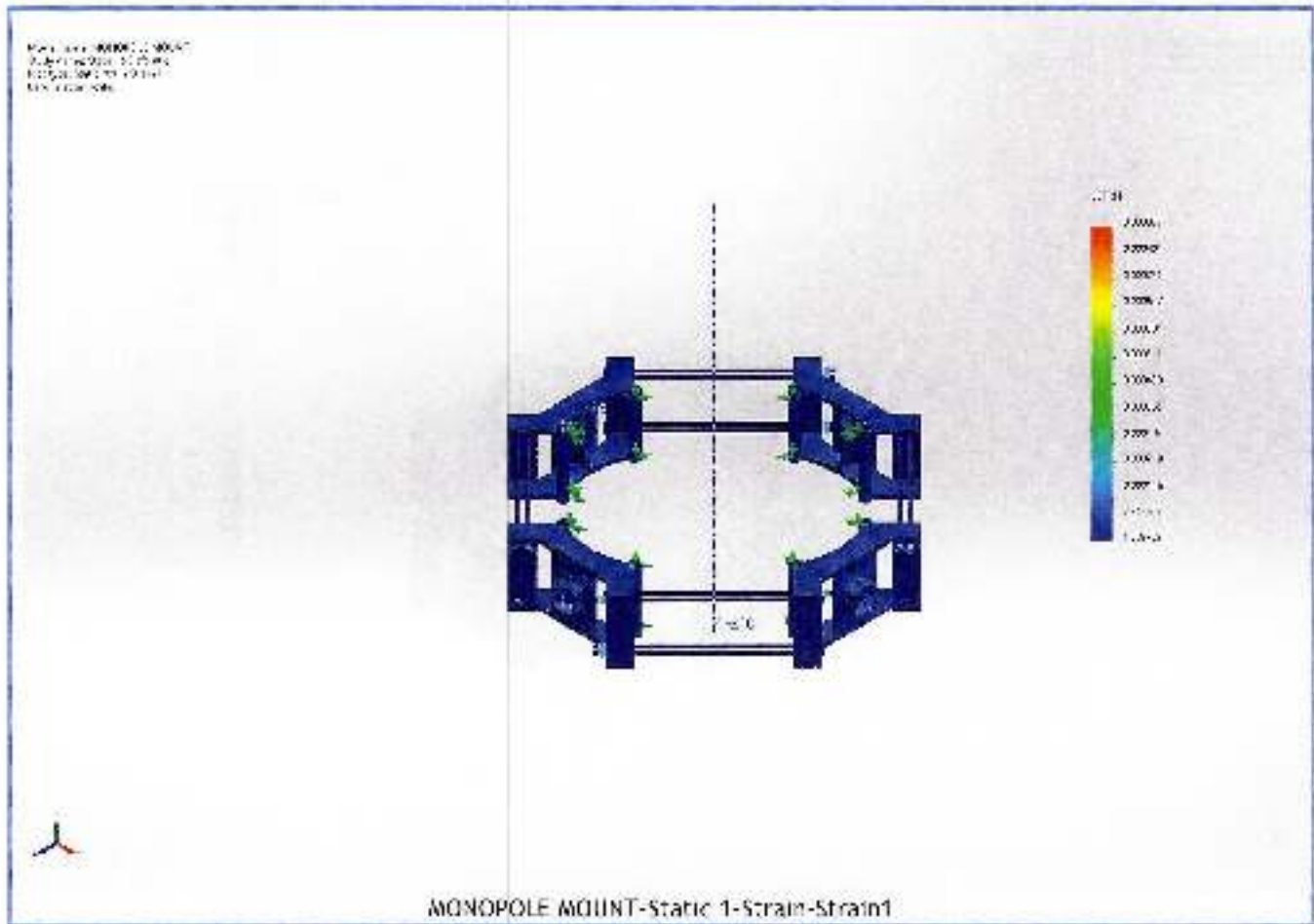
Name	Type	Min	Max
Stress1	VON: von Mises Stress	0.000ksi Node: 18526	30.273ksi Node: 479





Name	Type	Min	Max
Strain1	ESTRN: Equivalent Strain	1.38e-09 Node: 18526	0.000877 Node: 479





Name	Type	Min	Max
Stress2	VON: von Mises Stress	0.000ksi Node: 18526	30.273ksi Node: 479

